



Modeling and verifying ice supersaturated regions in the ARPEGE model for persistent contrail forecast

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Abstract. Contrails formed by aircraft in ice supersaturated regions (ISSR) can persist and spread for several hours, evolving into cirrus which have a net positive effect on global warming. Reducing this contribution could be achieved through on-purpose flight planning, in particular by avoiding ice supersaturated regions. In this context, a modification to the cloud scheme of the ARPEGE operational numerical weather prediction (NWP) model is proposed to enable the representation of ISSRs at cruise altitude. This modification does not require any major algorithmic changes or additional computational effort, and the methodology is transferable to similar parameterizations, commonly used in global circulation models.

Humidity forecasts are evaluated using in situ aircraft humidity observations and compared with operational forecasts from ARPEGE and the Integrated Forecast System (IFS). A sensitivity study on neighborhood tolerance and humidity thresholding is carried out, enabling a comprehensive comparison between NWP forecasts. It is shown that the modified cloud scheme allows for supersaturation, significantly improving the representation of humidity with respect to ice, with ISSR discrimination skills close to IFS (hit rate $\sim 80\%$ and false alarm ratio $\sim 30\%$ when a neighborhood tolerance of 150 km, i.e. 10 min of flight, is applied). The spatial correspondence between observations and the modified ARPEGE model is illustrated by a commercial flight case study. The modelization of ice supersaturation in ARPEGE can therefore be used for further contrail climate impact applications, together with the associated evaluation methodology, which contributes to the definition of a shared framework for ISSR verification.

1 Introduction

Contrails, also known as condensation trails, are high-altitude ice clouds that form when water vapor from fuel combustion is released by jet engines. When temperatures are low enough and exceed the so-called Schmidt-Appelman criterion (Schumann, 1996), engine emissions lead to the formation of straight cirrus clouds, which are often clearly visible behind aircraft. When triggered in ice supersaturated regions commonly denoted ISSRs (i.e. relative humidity w.r.t ice $RH_{ice} > 100\%$), the trail can spread to form a large cirrus cloud, which can persist for several hours and is clearly visible by satellite (Minnis et al., 1998; Gierens and Vázquez-Navarro, 2018).



According to various studies (Lee et al., 2009, 2021), and in view of increasing civil air traffic, these induced cirrus clouds are likely to contribute significantly and positively to global warming. The effective radiative forcing (ERF) associated to persistent contrail could be of the same order of magnitude as ERF issued from CO₂ emissions of aviation industry, even if large uncertainties remain, stemming from various sources, such as our incomplete understanding of contrail cirrus life cycle and radiative properties (Schumann and Heymsfield, 2017).

The impact of persistent contrails on global warming might be mitigated by optimizing pre-tactical flight paths or by tactical avoidance of regions where meteorological conditions are likely to be favorable to persistent contrails (Sausen et al., 2023). Studies by Teoh et al. (2020) suggested that only 2 % of flights could contribute to 80 % of the estimated contrail ERF by using algorithmic climate change function (van Manen and Grewe, 2019). Other studies by Matthes et al. (2020) involving climate-optimization simulations found that the aviation-induced climate impact can be reduced in the range of 50 % at the expense of 1-2 % additional operational costs. The potential mitigation options at pre-tactical and tactical time scale to reduce climate impacts require operational weather forecasts, preferably at continental or global scale. These models must be reliable to predict where contrails may form and persist, which requires sufficient quality on temperature and relative humidity estimates in the upper troposphere and lower stratosphere (UTLS) region.

Most global circulation models (GCM) do not properly represent humidity in these regions because the parametrization of cirrus cloud formation implements saturation adjustment. One of the first operational parametrizations of supersaturation w.r.t ice in a global NWP model was proposed by Tompkins et al. (2007) and implemented in the Integrated Forecast System (IFS) of the European Center for Medium-Range Weather Forecasts (ECMWF). Ice supersaturation is parametrized within the cloud scheme by modifying the amount of water vapor in the clear-sky portion of the grid-box according to temperature conditions. However, this scheme is associated with a prognostic cloud fraction description which is non-easily transferable to many other global circulation models where cloud fraction is diagnosed. In general, obtaining a reliable description of the ISSR remains a challenge (e.g. Gierens et al., 2020) and very recent works are being done on modified micro-physical schemes to allow or enhance the description of ISSR (e.g. Sperber and Gierens, 2023; Borella et al., 2024; Seifert, 2024; Thompson et al., 2024), making this topic a very active field of research. In the global NWP ARPEGE model of the French national weather service Météo-France (Bouyssel et al., 2022), cloud fraction is diagnosed and the current saturation adjustment scheme converts instantaneously any excess of water vapor above ice saturation into ice, which leads to the result that ISSR cannot be represented.

The growing interest for ISSR forecasting for operational mitigation strategies should also trigger appropriate verification methods of NWP models. Most verification studies (e.g. Tompkins et al., 2007; Reutter et al., 2020; Gierens et al., 2020; Sperber and Gierens, 2023) compared the distribution of temperature and relative humidity to in situ measurements acquired from the In-service Aircraft for a Global Observing System database (IAGOS - previously named MOZAIC - Marenco et al., 1998; Petzold et al., 2015). The authors acknowledged that IAGOS offers a relevant reference for characterizing humidity in the UTLS, especially for contrail applications, and used these observations to exhibit main biases on ISSR in NWP models. Pointwise or neighborhood-based binary metrics have also been applied (e.g. Tompkins et al., 2007; Thompson et al., 2024; Wolf et al., 2025) to evaluate ISSR forecasts discrimination capabilities and compare forecasts against each other. Indeed,



it is both important to discriminate between the capacity to detect ISSR and also to avoid false alarms, due to the trade-off of additional CO₂ emissions when avoiding an ISSR. These verification methods deserve to be completed to accurately describe NWP model capabilities. ISSR occurrences are known to be a rather rare phenomenon in the atmosphere with patchy structures (Spichtinger and Leschner, 2016) embedded in thin layers close to the cold and humid tropopause (Petzold et al., 2020), which requires dedicated metrics including spatialization. For this purpose, the use of available information along IAGOS aircraft flight paths in the verification process seems valuable and adapted to aviation applications. In addition, recent studies suggested that unreliable forecasts may still have skills to discriminate ISSRs, provided that post-processing calibration or adapted threshold on relative humidity are applied (Teoh et al., 2022; Wolf et al., 2025). This leads to consider a range of different thresholds for ISSR verification for a complete evaluation and comparison of NWP models capabilities. In the end, a shared framework for the verification of ISSR should be defined, which is an important cornerstone of any strategy for avoiding areas conducive to the triggering of persistent warming contrails.

The proposed study addresses two major questions related to forecasting high-tropospheric humidity and ISSR. The first issue is the development of supersaturation in a global NWP model, the ARPEGE global NWP model of Météo-France, by modifying its cloud scheme. The second aspect addresses the verification of ISSR forecasts using IAGOS humidity observations.

The article is structured as follows. Section 2 is dedicated to the modified Smith cloud scheme (Smith, 1990) used in ARPEGE for allowance of supersaturation with respect to ice. Section 3 is dedicated to the presentation of observational and forecast datasets used for calibration and verification, and the interpolation methodology. The calibration procedure of the modified cloud scheme is presented in Sect. 4. The verification methodology and associated statistical results are presented and applied in Sect. 5, including a case study. The methodologies and the results presented in this paper are discussed in Sect. 6. Conclusions and perspectives of this work are given in Sect. 7. All the calculations related to the modification of the ARPEGE cloud scheme are given in the Appendix.

2 Modified cloud scheme for the ARPEGE model to allow ice supersaturation

The microphysical scheme used in ARPEGE was first developed by Lopez (2002). It mainly follows the approach proposed in Fowler et al. (1996), but with a reduced complexity. It is based on a prognostic representation of four condensed water species (cloud droplets, ice crystals, rain, snow) for large scale and shallow convective clouds, and on a diagnostic representation for deep convective clouds. A statistical cloud scheme using a symmetrical triangular probability density function (Smith, 1990) provides cloudiness and mean cloud water condensate within a grid-box for large scale clouds, assuming that cloud condensation and evaporation are instantaneous and reversible. The width of the probability density function is defined by a critical relative humidity threshold that decreases with model level height and horizontal resolution. Partitioning between liquid and ice contents is temperature-dependent, so that the mixed phase lies between 273.15 K and 250 K (more details can be found in Roehrig et al., 2020). Cloud formation initiates when saturation is locally exceeded within the grid-box, which is an actual limitation of the ARPEGE cloud scheme as it removes any supersaturation. This hypothesis, validated in the liquid



phase, is known to be erroneous in the ice phase, as supersaturation relative to ice is commonly measured by in situ or remote sensing instruments (e.g. Krämer et al., 2009; Heymsfield et al., 2017). Here, we propose a simple extension of the Smith cloud scheme implemented in the ARPEGE model to allow ice supersaturation at cruise levels.

2.1 Parametrization of supersaturation w.r.t. ice

95 The parametrization of supersaturation w.r.t ice in the UTLS is based on the assumption that ice crystals are formed in most cases by the homogeneous nucleation process when the temperature is lower than 235 K. We introduce a saturation ratio coefficient k which is a function of the average temperature in the grid-box \bar{T} and represents the ratio of saturation to be reached to have homogeneous nucleation processes activated in the grid-box. For temperatures colder than 235 K, the saturation ratio coefficient is set such as

$$100 \quad k = C_{\text{calib}} \cdot f(\bar{T}), \quad f(T) = 2.583 - T/207.8 \text{ K} \quad (1)$$

where $f(T)$ represents the homogeneous nucleation threshold as a function of T (see e.g. Koop et al., 2000; Kärcher and Lohmann, 2002; Tompkins et al., 2007; Sperber and Gierens, 2023), and C_{calib} is a calibration coefficient used for the tuning of the model. From 235 K, a linear return is made back to $k = 1$ at 250 K ($k = 1$ for $\bar{T} \geq 250$ K). This implies that the range of temperature where supersaturation is allowed in our study is set for temperatures colder than 250 K collocating with the
 105 pure ice phase limit within ARPEGE microphysical scheme, this range being compatible with persistent contrail applications. In higher temperature conditions where mixed-phase or pure liquid conditions can exist, the ARPEGE cloud scheme is not directly impacted by the modification.

The second step is to write the local thermodynamic adjustment equation to include the saturation ratio coefficient in the classical scheme. The following assumptions are used:

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- when ice supersaturation conditions are allowed (i.e. $k > 1$), condensate can exist within a grid-box for any point where the saturation ratio k is locally exceeded.
 - once the supersaturation threshold is locally exceeded, local adjustment is instantly obtained back to saturation.

Local equations of the cloud scheme are then given by the following set of equations:

$$q_c^+ = \begin{cases} q_t - q_{\text{sat}}(T, p) & q_t > k \cdot q_{\text{sat}}(T, p), \\ 0 & q_t \leq k \cdot q_{\text{sat}}(T, p), \end{cases} \quad (2)$$

115 where q_c^+ is the local condensed content after adjustment, q_t is the total specific humidity before adjustment, that is the sum of the vapor and the condensate ($q_v + q_c$), and $q_{\text{sat}}(T, p)$ is the saturation specific humidity w.r.t liquid water or ice before adjustment at temperature T and pressure p . The symbol "+" denotes that the variable is being diagnosed from the prognostic variables, which means that the value is obtained after adjustment. Figure 1 provides a graphical representation of Eq. (2). With the modification of the scheme, the total specific humidity (in blue) must exceed the values of $k \cdot q_{\text{sat}}$ (in purple) for a cloud to



120 form, while in the operational version, a cloud would form once q_{sat} (in green) is exceeded. Consequently, areas classified as cloudy in the operational scheme may be supersaturated with the new scheme.

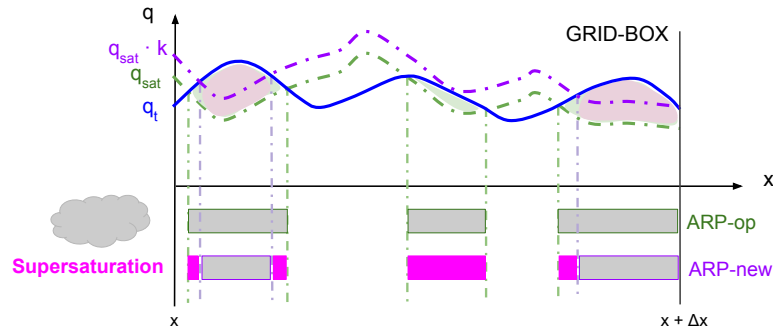


Figure 1. Illustration of the variability of q_t and q_{sat} inside a NWP model grid-box. In the current ARPEGE model (denoted ARP-op in green), thermodynamical adjustment is done back to saturation when $q_t > q_{sat}$. In the modified ARPEGE model (denoted ARP-new in purple), thermodynamical adjustment is done back to saturation when $q_t > k \cdot q_{sat}$, which allows supersaturation.

2.2 Calculation of the mean condensed content and the mean cloud cover

The difference between the modified and the original ARPEGE scheme relies in the introduction of variable k in Eq. (2) to define the nucleation threshold, and the following consists in reworking the original cloud scheme equations with $k > 1$. To calculate the mean condensed content and the mean cloud cover in the grid-box, a statistical description of the distance to supersaturation $q_t - k q_{sat}$ in the grid-box is used. We introduce the notation \bar{x} (resp. x') to represent the grid-box mean value (resp. the local perturbation) of a variable x . Following the cloud distribution concepts developed by Sommeria and Deardorff (1977) and Mellor (1977), and assuming that pressure fluctuations are negligible in the grid-box (Bougeault, 1981), the local difference between q_t and $k q_{sat}(T, p)$ can be expressed by

$$130 \quad q_t - k q_{sat}(T, p) = Q_{c,k} + s, \quad (3)$$

where $Q_{c,k}$ characterizes the average distance to supersaturation ($k > 1$) resp. saturation ($k = 1$) in the grid-box, such as

$$Q_{c,k} = a_{L,k} [\bar{q}_t - k \bar{q}_{sat}(\bar{T}_L, \bar{p})], \quad (4)$$

and s represents the local deviation around the value of $Q_{c,k}$ and can be described by

$$s = a_{L,k} [q'_t - k b_L T'_L], \quad (5)$$

135 with L being the latent heat of condensation, c_p the specific heat capacity of air at constant pressure, and $T_L = T - (L/c_p) \cdot q_c$ the liquid water temperature which is conserved through the condensation process. The factors $a_{L,k}$ and b_L account for changes



in q_{sat} due to latent heating and are given by

$$a_{L,k} = (1 + kb_L L/c_p)^{-1}, \quad (6)$$

$$b_L = \varepsilon L \bar{q}_{sat} (\bar{T}_L, \bar{p}) / R \bar{T}_L^2, \quad (7)$$

140 where R is the dry air specific gas constant and ε is the ratio of dry air constant and vapor constant.

The local deviation s is statistically modeled by a centered G -distribution with a standard deviation $\sigma_{s,k}$ such as $s \sim G_{[0,\sigma_{s,k}]}$. This implies that $q_t - k q_{sat}$ follows a G -distribution with a mean equal to $Q_{c,k}$ and a standard deviation $\sigma_{s,k}$ which gives

$$q_t - k q_{sat} \sim G_{[Q_{c,k},\sigma_{s,k}]}. \quad (8)$$

Note that to keep the framework simple, we have assumed that the nature of the probability distribution is independent of the value of k . This translates into the fact that the $q_t - k q_{sat}$ distributions for different values of k differ from each other by an offset and a scaling factor.

The mean cloud fraction after adjustment C^+ is given by the integration of $q_t - k q_{sat}$ distribution $G_{[Q_{c,k},\sigma_{s,k}]}$ for positive values only, which corresponds to the cloudy part of the grid-box. It can be expressed as the integral of the normalized centered probability distribution $G_{[0,1]}(t)$ (see calculations in Appendix A)

$$150 \quad C^+ = \int_{-Q_{c,k}/\sigma_{s,k}}^{+\infty} G_{[0,1]}(t) dt. \quad (9)$$

The mean cloud water content after adjustment \bar{q}_c^+ is given by integrating the local content $q_t - q_{sat}$ only on the grid-box cloudy part. In order to get a workable expression, it is assumed that local positive values of $q_t - k q_{sat}$ coincide with the highest $q_t - q_{sat}$ values (see calculations in Appendix A), which gives:

$$\bar{q}_c^+ = \sigma_{s,1} \int_{-Q_{c,k}/\sigma_{s,k}}^{+\infty} G_{[0,1]}(t) \left(t + \frac{Q_{c,1}}{\sigma_{s,1}} \right) dt. \quad (10)$$

155 It is important to note that steps from Eq. (2) to Eq. (10) do not depend on the probability distribution that is chosen, hence the methodology can be applied to cloud schemes based on the same type of statistical distribution concepts.

2.3 Application to the ARPEGE cloud scheme

The Smith (1990) cloud scheme used in ARPEGE assumes a symmetric triangular probability function for the setting of the s distribution. Applying this methodology in our context, the probability density function is represented by a symmetric triangular distribution with a finite support, its lower and upper limits spanning from $-\sqrt{6}\sigma_{s,k}$ to $\sqrt{6}\sigma_{s,k}$, as represented in Fig. 2. The cloud fraction is non-zero when $-Q_{c,k} < \sqrt{6}\sigma_{s,k}$ indicating the presence of condensed water when the critical point corresponding to $-Q_{c,k} = \sqrt{6}\sigma_{s,k}$ is obtained. This equality can be used to define the critical relative humidity threshold $\bar{U}_{c,k} = \bar{q}_v / \bar{q}_{sat}(\bar{T}, \bar{p})$. Evaluating $Q_{c,k}$ at this critical point where $\bar{q}_t = \bar{q}_v$ and $\bar{T}_L = \bar{T}$ leads to

$$\sigma_{s,k} = \frac{a_{L,k}}{\sqrt{6}} \bar{q}_{sat}(k - \bar{U}_{c,k}). \quad (11)$$



165 This expression exhibits a direct relation between the width of the distribution $\sigma_{s,k}$ and the critical relative humidity $\bar{U}_{c,k}$. This allows the cloud scheme closure by the definition of a critical relative humidity threshold, as the s distribution is fully determined by its standard deviation. Defining $\alpha_k = Q_{c,k}/\sigma_{s,k}\sqrt{6}$, the integration of Eq. (9) and (10) gives an explicit algorithm (see Algorithm 1) for the computation of C^+ and \bar{q}_c^+ (see appendix A for calculations). Setting $k \equiv 1$ returns to original Smith cloud scheme.

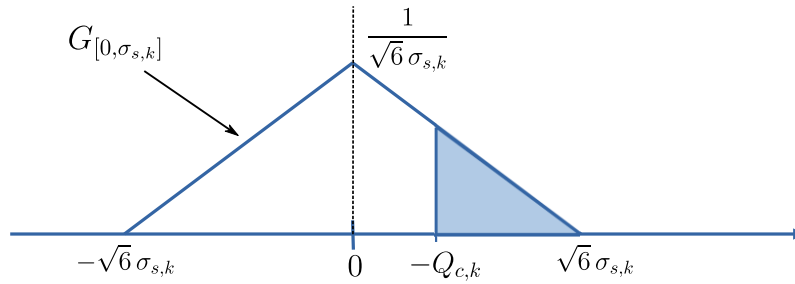


Figure 2. Probability density function G applied for the statistical representation of variability inside the grid-box in the modified Smith cloud scheme. Shaded area measures the cloud fraction as it corresponds to the integration of the cloudy part of the grid-box (i.e. $q_t - k q_{sat} > 0$).

Algorithm 1 Modified Smith Cloud Scheme

If $\alpha_k \leq -1$ then

$$C^+ = 0 \quad \text{and} \quad \bar{q}_c^+ = 0 \tag{12a}$$

If $-1 < \alpha_k \leq 0$ then

$$C^+ = \frac{1}{2}(1 + \alpha_k)^2 \quad \text{and} \quad \bar{q}_c^+ = \frac{\sigma_{s,1}}{\sqrt{6}}(1 + \alpha_k)^3 + \sigma_{s,1}\sqrt{6}\frac{(1 + \alpha_k)^2}{2}(\alpha_1 - \alpha_k) \tag{12b}$$

If $0 < \alpha_k \leq 1$ then

$$C^+ = 1 - \frac{1}{2}(1 - \alpha_k)^2 \quad \text{and} \quad \bar{q}_c^+ = \sigma_{s,1}\alpha_1\sqrt{6} + \frac{\sigma_{s,1}}{\sqrt{6}}(1 - \alpha_k)^3 - \sigma_{s,1}\sqrt{6}\frac{(1 - \alpha_k)^2}{2}(\alpha_1 - \alpha_k) \tag{12c}$$

If $\alpha_k > 1$ then

$$C^+ = 1 \quad \text{and} \quad \bar{q}_c^+ = \sigma_{s,1}\alpha_1\sqrt{6} \tag{12d}$$

170 The final closure of the system of equations can be given by an arbitrary definition of $U_{c,k}$ for all values of k . However, some simple limiting cases in the s formulation given in Eq. (5) can be exhibited and allows to restrict the closure to the choice of $U_{c,1}$:

Closure 1 - If predominance of humidity variability term over temperature variability term is assumed in the s formula i.e.

$q'_t \gg kb_L T'_L$, then $\sigma_{s,k}/\sigma_{s,1}$ is equal to $a_{L,k}/a_{L,1}$ and closure is given by:

$$175 \quad \bar{U}_{c,k} = \bar{U}_{c,1} + k - 1 \tag{13}$$



Closure 2 - If temperature variability term is assumed to be predominant in the s formula i.e. $kb_L T'_L \gg T'_L$, then $\sigma_{s,k}/\sigma_{s,1}$ equals $k a_{L,k}/a_{L,1}$ and closure is given by:

$$\bar{U}_{c,k} = k \bar{U}_{c,1}. \quad (14)$$

180 3 Historical dataset

This study aims to compare forecasts issued from several NWP models: ARPEGE with the modified cloud scheme, non-modified ARPEGE, and IFS model from ECMWF, to in situ measurements of UTLS humidity. The observational dataset is issued from instrumental data from the In-service Aircraft for a Global Observing System (IAGOS; <https://www.iagos.org>). The study period extends from the 1st July 2022 to the 30th June 2023 within the aerial boundary of 80° W–40° E and 185 30°–75° N, covering the space of North Atlantic and Europe that is one of the world’s densest air traffic regions. The vertical domain extends from FL250 to FL450, encompassing regions favorable to the triggering of persistent contrails. The datasets are randomly split into two parts, such that half of the flights are used to calibrate the modified ARPEGE cloud scheme, while the other half is used for the verification of NWP model forecasts (see Fig. 3).

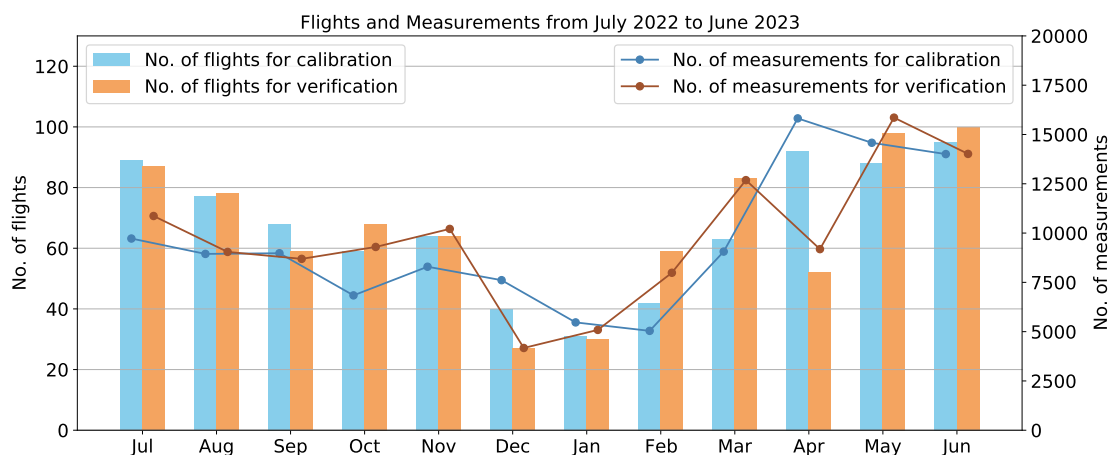


Figure 3. IAGOS equipped flights and measurements from July 2022 to June 2023. The dataset is divided in two subsets: flights dedicated to the calibration of the new cloud scheme (blue) and flights dedicated to the verification (orange).

3.1 NWP data

190 The operational version of the ARPEGE model runs 4 times a day with a stretched native grid of 5 km above Europe and 25 km over Oceania and with a 105 level vertical grid. In the following we will denote "ARP-new" the ARPEGE model with the modified cloud scheme, and "ARP-op" the version of the model with the operational (non-modified) cloud scheme. We also



perform the verification of RH_{ice} provided by the high resolution (HRES) configuration of the IFS model operated by ECMWF (ECMWF-documentation, 2025, cy48r1). It has a mean native resolution of approximately 9 km worldwide and 137 vertical
195 levels. ARP-op and IFS forecasts start from their own respective operational analysis. The ARP-new forecast starts from the analysis of ARP-op.

For all NWP models, runs of 00Z and 12Z are used, and hourly time steps from T+6 to T+17 are considered for output lead terms. Each output is interpolated on a regular 0.25° lat/lon horizontal grid. The vertical output grid is composed of 21 vertical
200 Standard Atmosphere (ICAO, 1993).

3.2 IAGOS

IAGOS is a European non-profit association involving research organizations, universities and weather services from Germany, France and the U.K, which provides in situ commercial aircraft observations in relation with air quality and climate change (e.g. Bundke et al., 2015; Filges et al., 2015; Nédélec et al., 2015; Petzold et al., 2015). Ambient air temperature and relative
205 humidity measurements are one of the main IAGOS-core data products. They are measured by a platinum resistance sensor (Pt100) and a capacitive sensor (Humicap-H, Vaisala, Finland), respectively, which are combined into the so-called ICH sensor (IAGOS Capacitive Hygrometer (Neis et al., 2015)). The accuracy of the instruments used for RH measurements is considered approximately 5 % with typical 1-3 min instrument response time ($\approx 15 - 50$ km of flight if a cruising speed of 250 m/s is considered) (e.g. Petzold et al., 2020). Aircrafts equipped with IAGOS sensors operate at a cruising altitude between 9 and 13
210 km, providing a comprehensive in situ dataset of UTLS humidity on a global scale, although northern extra-tropical and, in particular, Europe and Northern Atlantic flight paths are more frequently sampled.

The IAGOS observational dataset and NWP models have very different resolutions. Indeed, the horizontal outputs of the model data is 0.25° (20–25 km at mid-latitudes), while the output frequency of the observations is 4 s along the flight track, resulting in a spatial resolution of approximately 1 km between adjacent observed points, considering regular cruise speeds. In
215 order to have comparable resolutions for the needs of calibration and verification, the IAGOS dataset is smoothed and under-sampled. A temporal interval of 100 s with a centered mean-filter window is applied to obtain an under-sampled resolution of ~ 25 km. Nearest point interpolation in time and space dimensions is then used to assign each observation to the NWP outputs in closest proximity.

4 Calibration of the modified cloud scheme

220 In this section, we present the calibration process for the modified cloud scheme. The calibration is based on adjusting the saturation ratio coefficient k through the calibration coefficient C_{calib} (see Fig. 4). It is also necessary to define a critical humidity threshold for any value of k in order to obtain a closed system of equations. Two formulations given by closure 1 and 2 in equations (13) and (14) are tested (see Sect. 2.3). Both options are set in the basis of the critical humidity threshold $U_{c,1}$ that is used in ARP-op ($U_{c,1} \simeq 50\%$ in the study domain).

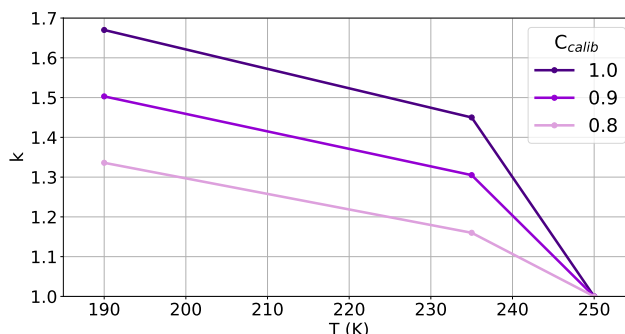


Figure 4. Saturation ratio coefficient k as a function of temperature for different values of C_{calib} .

225 The RH_{ice} results given by ARP-new forecasts are compared to IAGOS in situ measurements in the UTLS, for closure 1 (Fig. 5a) and 2 (Fig. 5b). For both closures, the frequency histogram plot with the associated frequency bias on $RH_{ice} > 100\%$ events is analyzed as a function of different C_{calib} values: 1.0, 0.9 and 0.8.

The results in Fig. 5 show that supersaturation with respect to ice is achieved with both closures. With closure 1, slightly higher supersaturation values are reached, however, histogram curves show a more pronounced divergence from IAGOS for the different values of C_{calib} . In contrast, closure 2 approaches the observations more closely for all RH_{ice} values. We conclude that in our study the closure 2 is better suited to the IAGOS observations and will therefore analyze its results in greater detail.

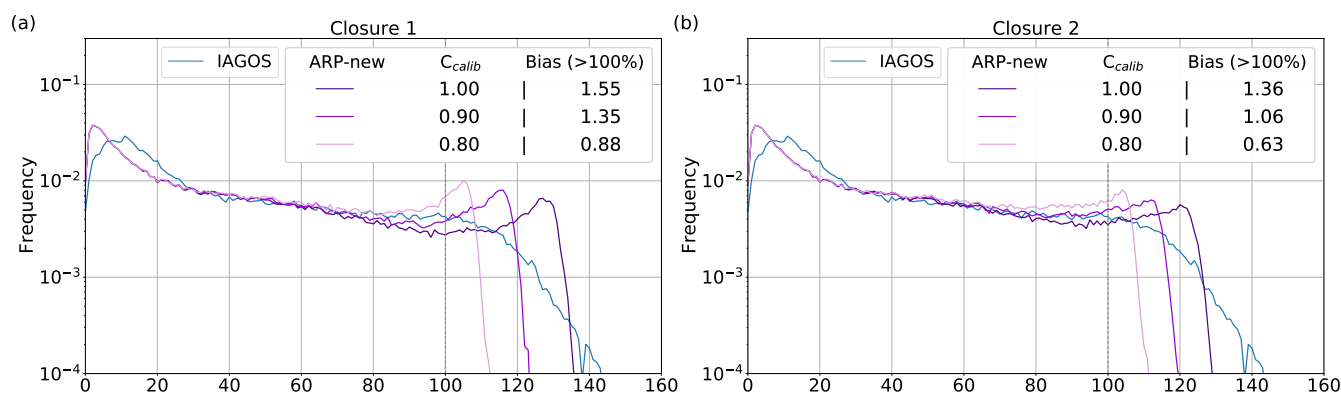


Figure 5. Frequency histograms of RH_{ice} (1 % bins) with the associated frequency bias on $RH_{ice} > 100\%$. Results are shown for under-sampled IAGOS observational dataset and ARP-new for different C_{calib} values ranging from 0.8 to 1.0. In panel (a), ARP-new is defined with closure 1 and in panel (b), with closure 2. Calibration dataset from the 1st July 2022 to the 30th June 2023 within the aerial boundary of 80° W–40° E and 30–75° N, covering North Atlantic and Europe.

In the RH_{ice} histogram shown in Fig. 5b, the ARP-new results demonstrate a high degree of alignment with observations for RH_{ice} values between 80 % to 100 %, especially for $C_{calib} = 0.90$. For supersaturated values ranging from 100 % to 110 %, RH_{ice} values are slightly over-forecast. At a certain point, ARP-new is unable to predict higher supersaturation values. When



235 $C_{calib} = 0.90$ is set, there is a sudden halt around 115 %, meaning that RH_{ice} values above 115 % are not forecast. This limit can be extended to higher values as C_{calib} increases but leads to an over-forecast of ISSR events as shown by the frequency bias results.

The evaluation of the results leads us to select the following calibration set for ARP-new: $C_{calib} = 0.90$ with closure 2. In addition to demonstrating a relative humidity frequency distribution that closely aligns with the observations, this combination
240 has the best bias on RH_{ice} events > 100 % and manages to predict higher supersaturated values than $C_{calib} = 0.80$, without under-predicting, unlike $C_{calib} = 1.00$, the sub-saturated values.

5 Verification

This section is dedicated to the verification of RH_{ice} forecast and, more particularly, ISSR events by the calibrated ARP-new model (closure 2 and $C_{calib} = 0.90$). The results are compared to the ARP-op model and the IFS model. We pay particular
245 attention to the use of appropriate and easy-to-interpret metrics in the context of persistent contrail avoidance. Indeed, ISSR occurrences are known to be a rather rare phenomenon in the atmosphere (~10 % of the IAGOS dataset in this study) requiring metrics adapted to such imbalanced datasets. Moreover, ISSRs can often have small dimensions compared to the synoptic scale or be organized in heterogeneous patterns (Spichtinger and Leschner, 2016; Gierens and Vázquez-Navarro, 2018), requiring metrics involving a neighborhood approach also referred as "spatial metrics". In addition, the choice of appropriate RH_{ice}
250 decision thresholds for contrail avoidance application is an on-going question (e.g. Dietmüller et al., 2023), demonstrating the need for sensitivity analysis. Then, after a first general analysis of the results on the continuous RH_{ice} variable in Sect. 5.1, we propose the introduction of spatial verification metrics using the available trajectory information in Sect. 5.2, thus allowing a better assessment of ISSR forecast quality in terms of spatial scale. A methodology for a comprehensive evaluation of the discrimination capabilities of ISSR events with different degrees of intensity is also introduced by performing a sensitivity
255 analysis on RH_{ice} thresholds in Sect. 5.3.

5.1 Verification of RH_{ice} continuous variable

The RH_{ice} histogram with the associated frequency bias for $RH_{ice} > 100$ % and the Mean Absolute Error (MAE) for different observed humidity categories are calculated for the verification dataset and for three models: ARP-new, ARP-op and IFS. Figure 6 (top) shows that ARP-new permits supersaturation, exhibiting a close alignment with the observed RH_{ice} histogram,
260 although it does not allow supersaturation exceeding 115 %, as underlined in the calibration study (Sect. 4). The frequency bias of ARP-new for RH_{ice} events greater than 100 % is neutral. ARP-new offers enhanced reliability in comparison to ARP-op, which shows a peak at 100 %, standing out from the rest of the curve and followed by a precipitous drop beyond 100 %, indicating that supersaturation is not forecast. Moreover, ARP-new gets to remove the over-representation of the 70–100 % RH_{ice} categories of ARP-op. Concerning IFS, as shown in previous studies (e.g. Gierens et al., 2020; Sperber and Gierens,
265 2023), the results show a pronounced peak at 100 % and an under-estimation for higher RH_{ice} values evidenced by the frequency



bias (0.81) on RH_{ice} events greater than 100 %. IFS has a significant shortcoming when confronted with values exceeding 110 %.

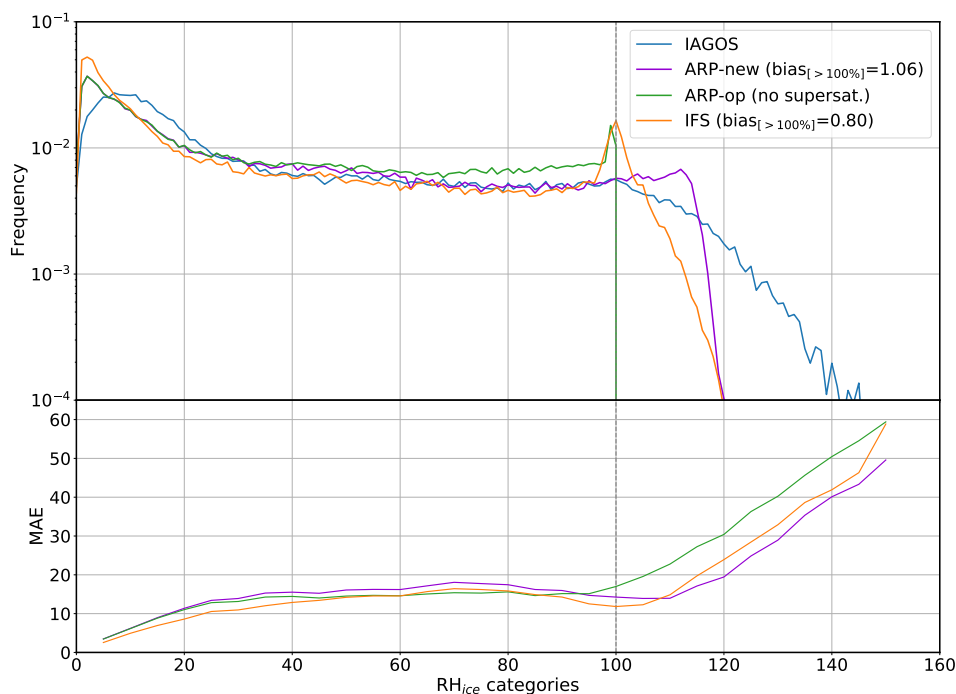


Figure 6. Frequency histogram of RH_{ice} (1 % bins) with the associated frequency bias on $RH_{ice} > 100$ % [top] and Mean Absolute Error (MAE) computed for different categories of observed humidity (5 % bins) [bottom]. Results are shown for IAGOS observational dataset (blue), ARP-new (purple), ARP-op (green) and IFS (orange). Verification dataset from the 1st July 2022 to the 30th June 2023 within the aerial boundary of 80° W– 40° E and 30 – 75° N, covering North Atlantic and Europe.

While the histogram gives a general idea of the distribution of the data, the MAE analyzes each observed RH_{ice} point and its corresponding forecast as to how close they are in value and provides an average of the pointwise model’s accuracy. Therefore, the conclusions of both are complementary. In Fig. 6 (bottom), ARP-new shows lower MAE values than ARP-op for RH_{ice} categories above 95 %, while in lower categories the MAE is just slightly higher. This suggests that most of the values removed from the over-representation of the 70-100 % categories in ARP-op, have been correctly adjusted to represent supersaturated values in ARP-new. For categories ranging from 95 to 105 %, the IFS model shows the lowest MAE values across all models, however, exhibiting a steady increase for categories above 105 %. In fact, categories around 100 % are significantly over-forecast by IFS, ensuring a lower amount of error for this specific categories of observations. In return, there is a strong MAE increase for under-predicted categories over 105 %. A similar trend is observed in ARP-new, however, for higher RH_{ice} , around 115 %, i.e. precisely when the histogram reveals a shortcoming. As a result, ARP-new exhibits the lowest MAE for higher supersaturated values.



5.2 ISSR verification with a trajectory-neighborhood approach

280 5.2.1 Methodology

This section introduces a trajectory-neighborhood verification approach for the evaluation of ISSR and presents resulting scores. In traditional verification methods or point-by-point metrics, perfect scores require near-perfect spatial and temporal matching with observations. However, it is not realistic to expect grid-scale accuracy in well-resolved NWP models due to the presence of small-scale variability (Schwartz, 2017). In fact, even if the model accurately forecasts the size and structure of an existing ISSR, it may be penalized if the predicted ISSR is slightly displaced in space and/or time. This is known as a "double penalty" (Gilleland et al., 2009; Bouttier and Marchal, 2024), as it would be regarded as both a miss and a false alarm, resulting in a less favorable score than if the model had not even predicted the existence of the ISSR. It is therefore useful to implement an effective neighborhood tolerance approach in order to deal with double penalty and capture relevant estimations of the quality of the forecast. From another perspective, neighborhood methods can also be used to identify the spatial scale at which a forecast becomes skillful or to determine the scale at which a desired model skill is achieved.

In this paper, we propose a trajectory-based neighborhood approach that compares predicted values and observations with a neighborhood tolerance oriented upstream and downstream of the flight trajectory. A symmetric approach, illustrated in Fig. 7, is taken to redefine traditional pointwise metrics used for binary event verification such as the hit rate (HR) and the false alarm ratio (FAR) scores (JWGFR, 2017).

- 295 – Hit rate (HR) with neighborhood tolerance: if an ISSR is observed in the flight trajectory, the associated forecast is classified as a true positive if the ISSR is forecast at any point within a distance 'd' upstream or downstream in the flight trajectory. The hit rate in a 'd' neighborhood can then be calculated as the ratio between the number of hits and the total number of ISSR observations. The hit rate is also called *Probability Of Detection (POD)* or *Recall* in literature.
- False alarm ratio (FAR) with neighborhood tolerance: symmetrically, if an ISSR is forecast in the flight trajectory but not observed within a distance 'd' upstream or downstream from the forecast, then it is scored as a false alarm. The FAR is defined as the ratio between the number of false alarms and the total number of ISSR forecasts, and is related to the precision score by $\text{Precision} = 1 - \text{FAR}$.

The mathematical expression of HR and FAR with neighborhood tolerance is given by

$$\text{HR} = \frac{\sum_i \max_{k \in \mathcal{N}_{d,i}} F_k \cdot O_i}{\sum_i O_i}, \quad \text{FAR} = \frac{\sum_i \max_{k \in \mathcal{N}_{d,i}} O_k \cdot F_i}{\sum_i F_i}, \quad (15)$$

305 where F_i and O_i are equal to 1 when an ISSR forecast (resp. observation) occurs at i^{th} record of the trajectory, and where $\mathcal{N}_{d,i}$ represents trajectory-neighborhood records downstream and upstream of the i^{th} record within a distance d and at constant flight level (i.e. tolerance of $\pm 1000\text{ft}$).

Hit rate and FAR are two metrics which characterize the discrimination skills of the forecast system on the positive event in a very intuitive way: the hit rate measures the capability of the forecast system to detect observed ISSRs while FAR represents



310 the predicted ISSR events which actually did not occur. These two complementary metrics often show an inverse relationship, where improving one of them worsens the other and can be combined in a single metric which is commonly used for imbalanced datasets where the emphasis is on the positive event: the F_β -score (e.g. Christen et al., 2023; Bouttier and Marchal, 2024). This score is given by the weighted harmonic mean of hit rate and precision score, such that

$$F_\beta\text{-score} = \frac{1 + \beta^2}{\beta^2 \text{HR}^{-1} + (1 - \text{FAR})^{-1}}, \quad \left(F_1\text{-score} = \frac{2}{\text{HR}^{-1} + (1 - \text{FAR})^{-1}} \right), \quad (16)$$

315 where $\beta > 1$ gives more weight to detection compared to precision and inversely if $\beta < 1$. In the case of rare events with high impact, the emphasis is often on the hit rate. However, in the case of ISSRs, it is important to ensure precision. By avoiding areas that are not actually supersaturated, aviation contribution to global warming could increase with respect to the baseline trajectory by supplementary CO₂ emissions, thus achieving the opposite effect to what was intended. In this paper, a neutral value of $\beta = 1$ is chosen and we leave to future studies the possibility of considering other values of this parameter in
 320 conjunction with optimization work involving climate metrics.

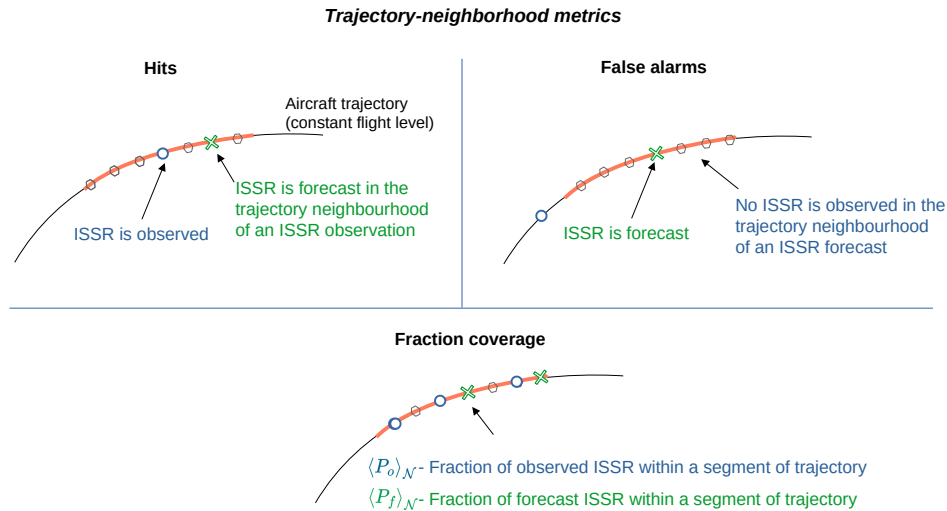


Figure 7. Definition of hits, false alarms and fraction coverage methodology on ISSR events with a trajectory-neighborhood approach.

In addition to the F_β score, a trajectory-neighborhood Fraction Skill Score (FSS) is implemented. This widely used method compares the forecast and observed ISSR fractional coverage within a defined spatial neighborhood (Ebert, 2009; JWGFGR, 2017). It is defined in our context by

$$\text{FSS} = 1 - \frac{\sum_i \left(\langle P_f \rangle_{\mathcal{N}_{d,i}} - \langle P_o \rangle_{\mathcal{N}_{d,i}} \right)^2}{\sum_i \langle P_f \rangle_{\mathcal{N}_{d,i}}^2 + \sum_i \langle P_o \rangle_{\mathcal{N}_{d,i}}^2}, \quad (17)$$



325 where $\langle P_f \rangle_{\mathcal{N}_{d,i}}$ and $\langle P_o \rangle_{\mathcal{N}_{d,i}}$ are the fraction of ISSR forecasts (resp. observations) in the neighborhood $\mathcal{N}_{d,i}$ (see illustration in Fig. 7). The score is a skill metric inspired by the Brier score, which evaluates the difference between observed and predicted ISSR event fractions, considered as probabilities.

5.2.2 Results

330 The results of ISSR verification with trajectory-based approach are given in Fig. 8, where the outcomes of HR, FAR, F_1 -score and FSS are shown for varying neighborhood values ranging from the nearest to 240 km, with 30 km increments. The 95 % confidence intervals are calculated by using the bootstrap technique to account for sampling uncertainty (e.g. Bradley et al., 2008).

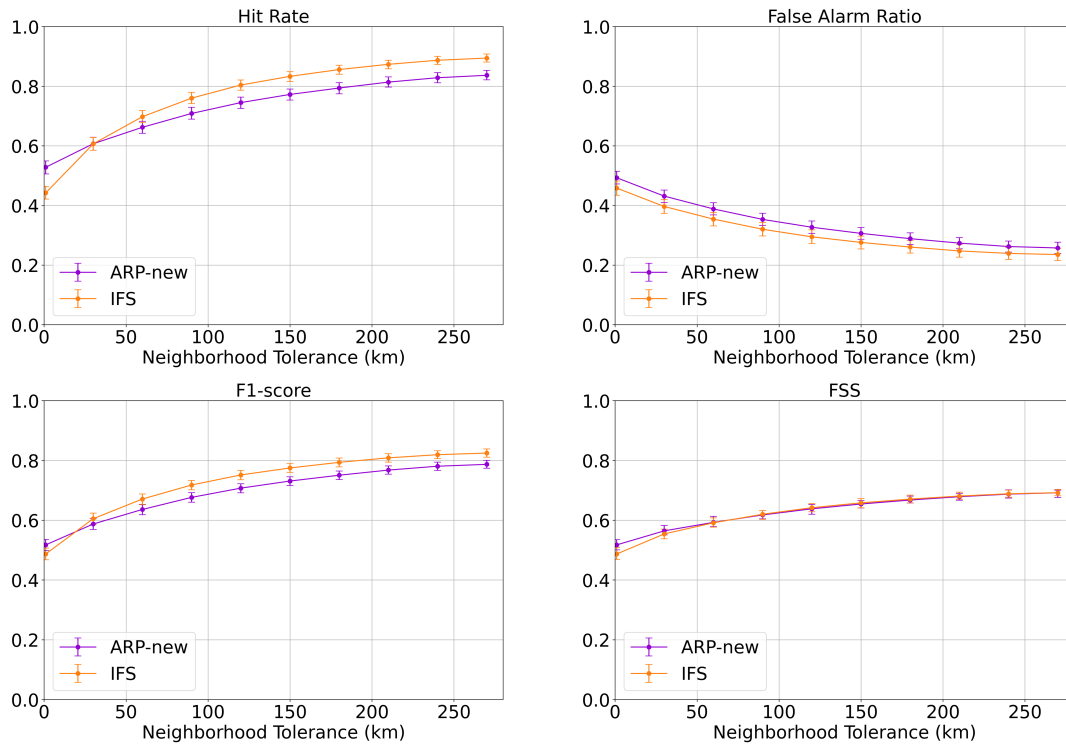


Figure 8. HR, FAR, F_1 -score and FSS score on ISSR events ($RH_{ice} > 100\%$) forecasts depending on increasing neighborhood spatial tolerance, for ARP-new (purple) and for IFS (orange) with 95 % confidence intervals. Neighborhood distances range from the nearest to 270 km, with 30 km increments. Verification dataset from the 1st July 2022 to the 30th June 2023 within the aerial boundary of 80° W– 40° E and 30 – 75° N, covering North Atlantic and Europe.

The results show that the scores have a high sensitivity to the neighborhood tolerance. With a neighborhood tolerance of 150 km which represents approximately 10 minutes of flight, ARP-new has a HR of around 77 % and a FAR of 31 %, compared with 53 % and 49 % respectively for the nearest grid-point. These values indicate that when an ISSR was observed, an ISSR

335



was forecast in a 150 km neighborhood in 77 % of the cases, and symmetrically that when an ISSR was forecast, an event could be observed in 69 % of the cases. If higher neighborhood tolerances are applied, the HR can reach values higher than 80 % with a FAR lower than 30 %, showing a rather good spatial agreement between observations and forecasts of ISSRs events.

A comparison of the discrimination capabilities of ARP-new and IFS shows that both NWP models have close skills. When
340 no neighborhood tolerance is taken into account, ARP-new has a higher HR but also a higher FAR than IFS. This translates into close F_1 and FSS scores for both models, with a slight advantage for ARP-new. Increasing the neighborhood tolerance improves all scores for both models, but IFS shows a better HR, FAR and F_1 -score than ARP-new, while the FSS scores still overlap. Some care has to be taken when comparing HR, FAR and F_1 -score with neighborhoods. Indeed, because of its general underestimation of ISSR (frequency bias ~ 0.8), IFS will have a tendency to have low FARs and low HRs when the nearest
345 point is considered. When the neighborhood tolerance is increased, the HR becomes less sensitive to this dry bias, since a single positive forecast in the neighborhood is enough to obtain a hit. This explains why, when the neighborhood tolerance is increased, IFS shows a greater increase in the HR, and consequently, in the F_1 -score compared to ARP-new which has a neutral bias. Although the FSS score is less easy to interpret, it appears to be more robust for global performance comparison purposes as it does not artificially offset biases.

350 5.3 Sensitivity analysis on RH_{ice} decision threshold

In Sect. 5.2, the RH_{ice} threshold has been set at 100 % in order to identify ISSRs in both forecasts and observations. However, there is a high interest in studying the sensitivity of scores on ISSR threshold definition for both forecast and observations:

- Regarding forecasts, varying the RH_{ice} threshold provides an overview of the NWP model performance range and should be considered for a complete evaluation of NWP model discriminatory skills. Since models are not perfectly calibrated
355 to observations, there may be forecast threshold values that offer better scores than the 100 % threshold regarding the end-user needs (see e.g. Dietmüller et al. (2023) who used a threshold lower than 100 % for ISSR detection in ERA5 models, and Teoh et al. (2022) and Wolf et al. (2025) who used post-processing recalibration of the RH_{ice} parameter).
- Regarding observations, evaluating the forecast of highly ice supersaturated regions (i.e. $RH_{ice} \simeq 110 \%$, 120% , ...) is also needed, as literature has shown that the lifetime persistence of contrails is influenced by the level of the supersaturation in the ISSR (Schumann et al., 2012). For slightly subsaturated regions (i.e. $RH_{ice} \simeq 90 \%$, 95%), there is also an
360 interest as it has been shown that saturation rates just below ice saturation could be sufficient to allow the existence of persistent contrails (Li et al., 2023).

In order to perform this sensitivity study, a robust approach in the context of imbalanced datasets is to use a graphical tool called the Precision-Recall curve (Saito and Rehmsmeier, 2015). The Precision-Recall curve is drawn by calculating the recall
365 (i.e. hit rate) and precision (i.e. 1-FAR) scores at several RH_{ice} thresholds for the forecast. In general terms, the curve closest to the top/right corner corresponds to the best discrimination capabilities, where precision and hit rate (recall) are optimal, i.e., equal to 1. This graphical tool is roughly equivalent to the widely used Receive Operation Characteristic (ROC) curve, but the Precision-Recall curve is better used in the context of rare events (Saito and Rehmsmeier, 2015; Bouttier and Marchal, 2024).



In Fig. 9, we show the Precision-Recall curves computed with no neighborhood tolerance. We represent four distinct plots, each corresponding to a different RH_{ice} threshold for the observations: 95 %, 100 %, 105 % and 115 %. We include ARP-op in this plot because, although it does not permit supersaturation, it may be capable of detecting ISSRs with a threshold of less than 100 %. For each curve, we calculate the Average Precision (AP), which is defined as the area under the Precision-Recall curve. The AP offers a concise overview of the Precision-Recall curve, facilitating direct comparisons between models and their scores across varying RH_{ice} ranges. Moreover, we represent the diagonal line where neutral frequency bias is obtained.

The results obtained with the observation threshold of 100 % (Fig. 9b) indicate that all three models have close APs, with an advantage for IFS. In addition, IFS exhibits the highest precision and recall scores close to the diagonal where neutral frequency bias is obtained. A comparison of the APs obtained with the 95 % threshold (Fig. 9a) reveals an improvement for all models with IFS being significantly better in the diagonal region. At higher humidity ranges, with the threshold of 105 % and 115 % (Fig. 9c and d), the APs are significantly lower for all the models, with ARP-new and ARP-op now performing the best. When comparing APs obtained for relative humidity above 100 % versus 115 %, a decrease of approximately 60 % in scores is revealed for all models.

The comparison of ARP-new model with ARP-op model shows that both models have a similar ability to discriminate ISSRs. For example, forecast threshold of 90 % in the non-modified ARPEGE corresponds to broadly the same HR and precision values as a threshold of 100 % with the modified cloud scheme. We conclude that the modified scheme strongly enhanced the reliability of the ARPEGE forecast of ISSR (as shown by Fig. 6), while being neutral on its inherent discrimination skills.

A comparison of the monotony of the Precision-Recall curves reveals that ARP-new and ARP-op exhibit divergent behavior compared to IFS. The ARPEGE curves are quasi monotonic, indicating that an increase in the decision threshold of the forecast is accompanied by an increase in precision. In contrast, IFS does not follow the same behavior. From a certain threshold close to 98 %, an increase in the decision threshold results in a decline in both precision and recall. This penalizes the global AP score for IFS, while it exhibits its maximum potential of ISSR discrimination for thresholds close to 98 %.

In addition to providing an overview of the performance of each model, the Precision-Recall curves can also be used to adjust the decision threshold in line with specific preferences regarding non-detections and false alarms. For example, should a pointwise HR of 0.6 be requested, we can ascertain the RH_{ice} threshold that should be selected in each model to discriminate ISSRs and the pointwise precision that will be achieved. If we fix the observation threshold at 100 % and aim for a HR of 0.6, we will have to choose $RH_{ice} = 97$ % as the threshold for the ARP-new forecast, giving a precision of 0.49. Similarly, we would have to choose a threshold of 87 % for ARP-op, with a precision of 0.47, and 97 % for IFS, with 0.55 precision.

Finally, it should be noted that the Precision-Recall curve can also be calculated with a neighborhood tolerance, following the methodology presented in Sect. 5.2.1 to calculate the HR and FAR.

5.4 Case study

In this section, we investigate a transatlantic IAGOS flight from 23 September 2022 between Frankfurt (Germany) and Washington D.C. (USA). A comparison is made between the observed and forecast ISSRs using IAGOS measurements and NWP

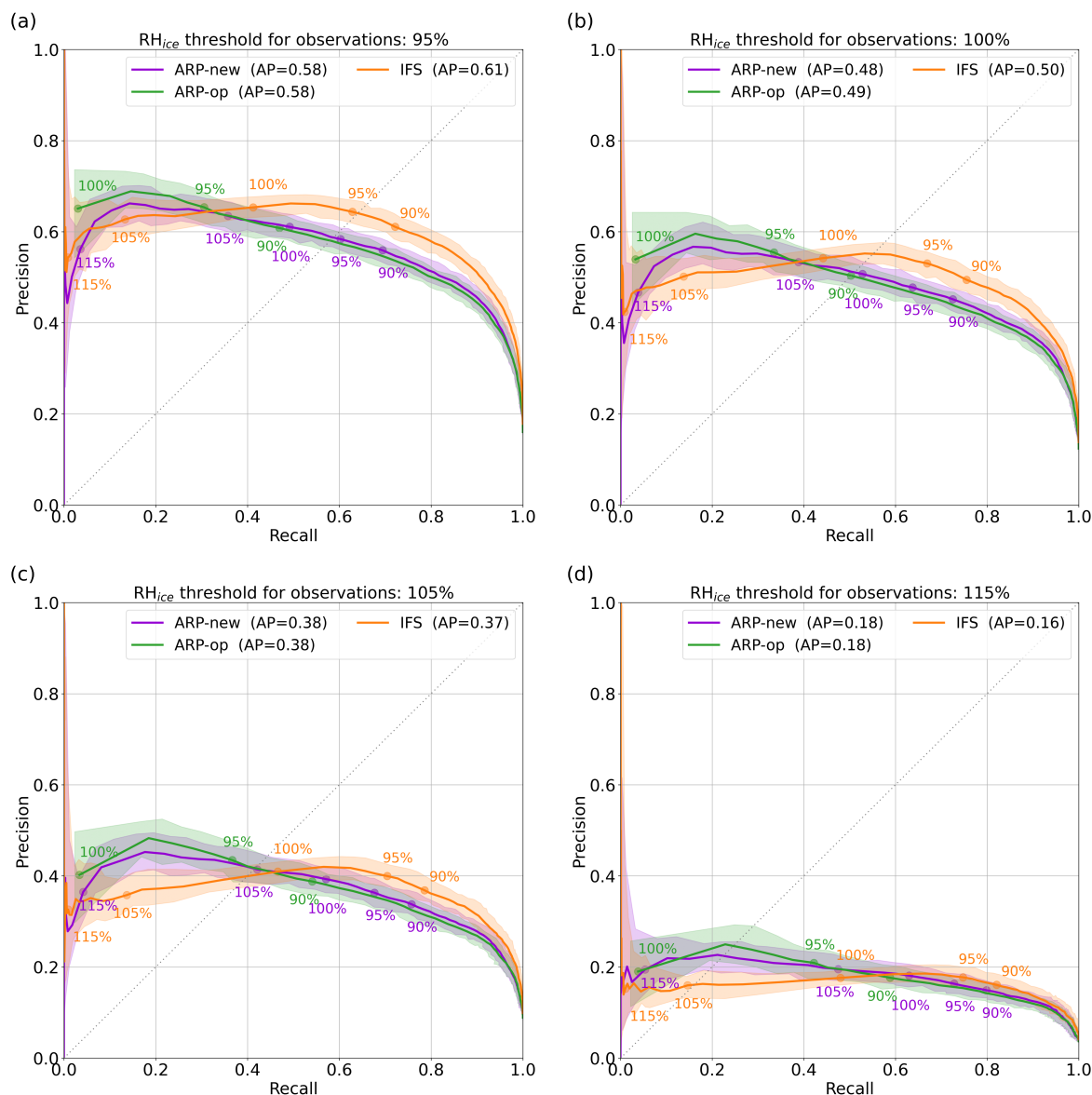


Figure 9. Precision-Recall curves representing discrimination skills of ARP-new (purple), ARP-op (green) and IFS (orange) for different RH_{ice} thresholds for observations: (a) 95 %, (b) 100 %, (c) 105 % and (d) 115 %. All the curves have been calculated without neighborhood tolerance. Intervals of 95 % confidence are shown with shaded areas. The points on the curves corresponding to the forecast thresholds are indicated accordingly: 95 %, 100 %, 105 % and 115 %. The legend includes the Average Precision score (AP) for each curve. The diagonal represents the neutral bias line. Verification dataset from the 1st July 2022 to the 30th June 2023 within the aerial boundary of 80° W–40° E and 30–75° N, covering North Atlantic and Europe.



data from both ARP-new, ARP-op and IFS. Figure 10 shows RH_{ice} along the IAGOS flight path. Take-off and landing are not included in this graph, as flight levels below FL250 are not of interest for this study.

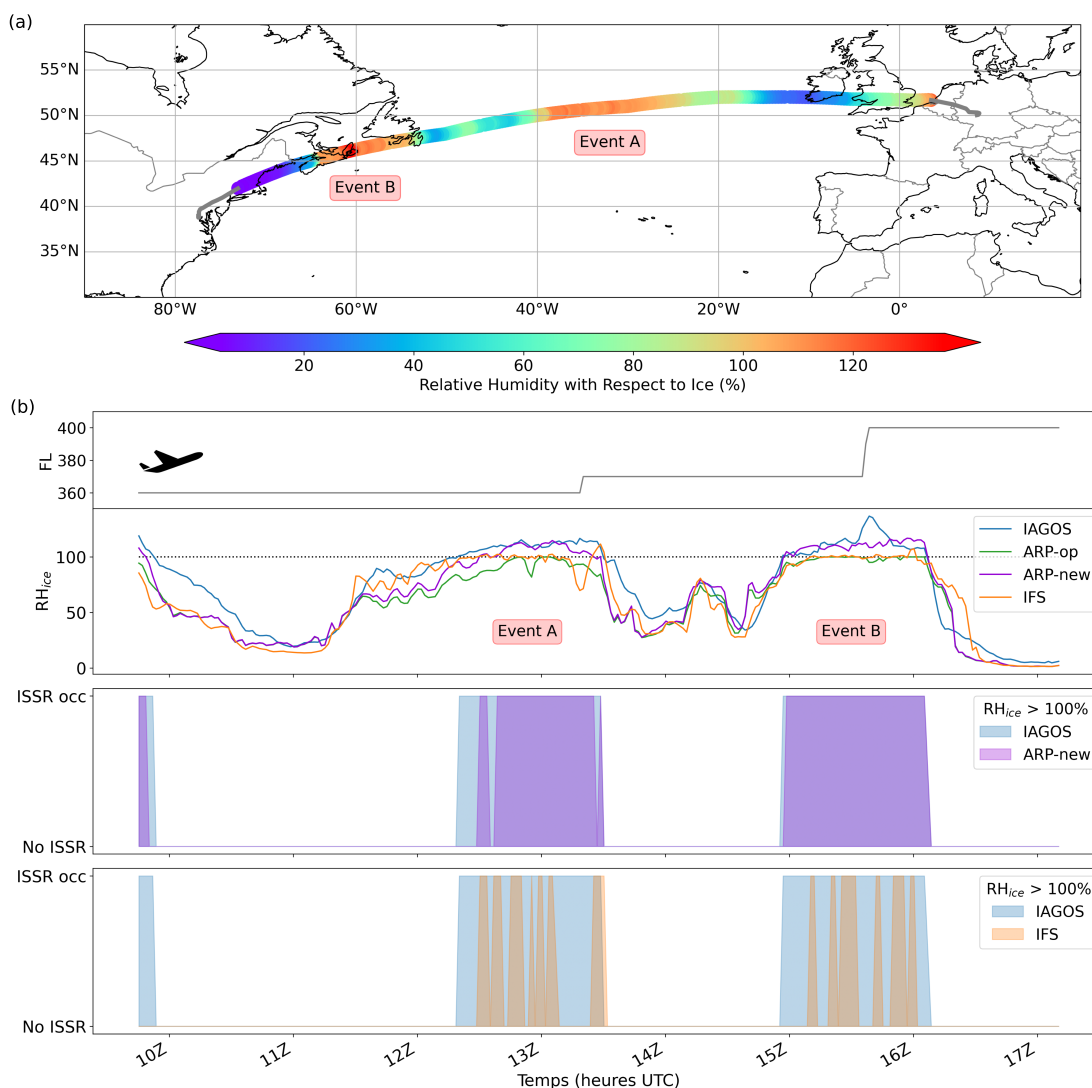


Figure 10. Case study of a transatlantic IAGOS flight, departing Frankfurt (FRA), Germany, on 23 September 2022 at 09:07 UTC and landing in Washington (IAD), USA, at 18:03 UTC. Panel (a) presents the flight trajectory with the observed RH_{ice} values. Two main ISSR events are identified denoted *A* and *B*. In panel (b), the times series shows the temporal evolution of RH_{ice} during the flight trajectory as measured by the IAGOS sensor (blue) and as forecast by NWP models - run 00Z. We represent ARP-new (purple), ARP-op (green) and IFS (orange). The three bottom series highlight observed ISSR occurrences (blue shading) with predicted ones for ARP-new (purple shading) and IFS (orange shading).



There are two distinct areas where the values are greater than 100 %, shown in orange and red (Fig. 10a). The first is over the Atlantic Ocean (region *A*), and the second is the vicinity of Newfoundland, Canada (region *B*). In Fig. 10b, the time series show the temporal evolution of RH_{ice} , with ISSR events highlighted in bottom plots to facilitate comparison between observations and forecasts. In this case, the ARP-new model has a very good agreement with the occurrence of ISSR events in regions *A* and *B*, particularly in region *B*. In the region *A*, RH_{ice} reveals that the ARP-new curve is slightly below the ISSR threshold while the observations start being supersaturated, yet leading to 'miss' events when, in fact, the global view of the episode is well predicted. This demonstrates the value of the neighborhood approach as a means of correctly interpreting scores. ARP-op, as it does not predict RH_{ice} values higher than 100 %, does not detect the ISSRs. However, it follows closely the time evolution of observations, even though it remains below the observations for $RH_{ice} > 100$ %. With regard to IFS, while the plot comparing the ISSRs indicates that it did not fully predict the episode, the relative humidity evolution reveals a pattern very closely aligned with the observations, but with a deficiency in reaching higher supersaturated values, confirming the IFS under-prediction of high values of RH_{ice} , as shown in Fig. 6. In the case of IFS, introducing a neighborhood tolerance in the verification process allows to counterbalance this under-representation of ISSR and exhibit the potential of detection capabilities of this model.

Figure 11 provides a zoomed spatial view of regions *A* and *B*. ISSR observed events in the flight trajectory are compared to ARP-new forecast at corresponding flight levels, and the presence of multiple persistent contrails is shown on the Cirrus Reflectance Product from Suomi NPP/VIIRS at times close to the flight path. This example highlights the good agreement between observations and forecast and confirms the potential of what could be made using NWP model forecasts to predict environments favorable to persistent contrail triggering.

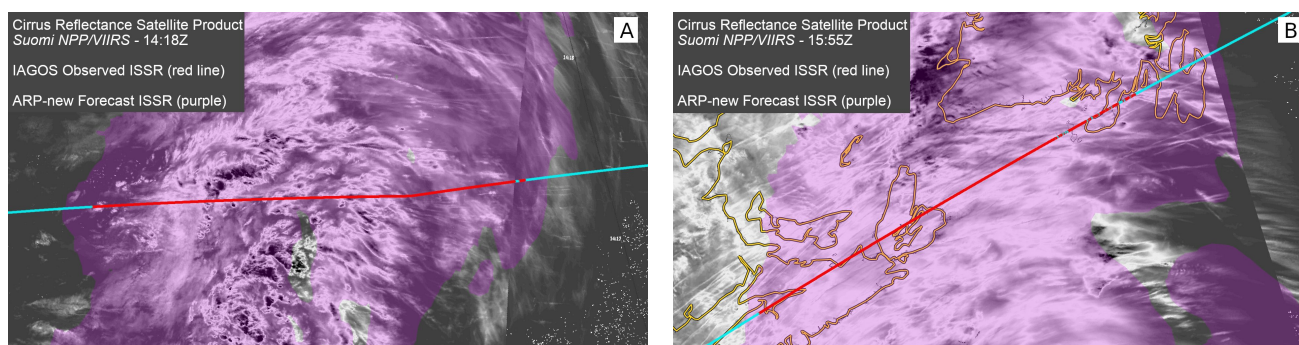


Figure 11. Cirrus Reflectance satellite imagery provided by NASA Worldview (<https://worldview.earthdata.nasa.gov>) from Suomi NPP/VIIRS identifying persistent contrails regions *A* (left) and *B* (right) on 23 September 2022 from the case study shown in Fig.10. IAGOS flight path is shown (cyan dots) exhibiting observed ISSR events (red dots). Forecast of ISSR by ARP-new model run-00Z at lead terms T+13 (left) T+16 (right) is given in spatio-temporal vicinity of the flight trajectory.



6 Discussion

Discussion on three key areas is proposed in the following. First, we analyze the modifications and assumptions we have made
425 on the cloud scheme and microphysics of the ARPEGE model. Second, we explore the definition of appropriate verification
methodologies to provide a comprehensive picture of a model's skill in the context of ISSR avoidance. Finally, we discuss
the results obtained on the performance of NWP models for ISSR discrimination and the implications for contrail avoidance
applications.

6.1 Cloud scheme and microphysics

430 A modified ARPEGE cloud scheme which allows supersaturation w.r.t ice is presented in this work. Some of the concepts
developed by Tompkins et al. (2007) in the framework of the IFS cloud scheme are used and adapted to be applied in the
original Smith cloud scheme implemented in ARPEGE. This allows to obtain local supersaturation w.r.t ice in the clear-sky
part of the grid-box, instead of assuming local ice saturation adjustment at any point. An important point is that much of the
methodology leading to the new parametrization is independent of the choice of the statistical distribution for the description
435 of local humidity and temperature variations inside the grid-box. This allows similar developments for NWP models using the
same type of statistical concepts for cloud representation. This is the case, for example, of the ICE3 micro-physical scheme
implemented in the French regional NWP model AROME (Seity et al., 2011, 2012), which uses a Gaussian distribution for the
representation of clouds and could benefit from these developments. Another important point is that this modification can be
implemented without any major modification to the operational ARPEGE cloud scheme, and does not imply supplementary
440 computational effort.

In the new scheme, some assumptions are made regarding the introduction of supersaturation in ARPEGE cloud scheme,
most of them having already been discussed in Tompkins et al. (2007); Sperber and Gierens (2023). For example, in the modi-
fied scheme, in-cloud adjustment to ice saturation is assumed instantaneous. However, it has been shown that RH_{ice} decreases
with a relaxation time that can exceed several time steps, to finally reach few percent above saturation, thus allowing local in-
445 cloud supersaturation w.r.t ice. Sperber and Gierens (2023) proposed a cooling-cloud formation-phase relaxation process as an
alternative to instantly adjusting to the equilibrium value. This modification requires the addition of new prognostic variables
describing the history of in-cloud supersaturation, which adds further complexity, but could result in a better description of
 RH_{ice} distribution for the highest values. Regarding cirrus cloud formation, homogeneous nucleation is considered dominant
compared to heterogeneous nucleation at the altitudes and temperatures of interest for the contrail application. It can be jus-
450 tified by the presence of relatively pristine environments with few ice nucleating particles (see e.g. Gierens, 2003; Tompkins
et al., 2007; Sperber and Gierens, 2023). Thus, a threshold with temperature dependence issued from Koop et al. (2000) is used
to represent the maximum local value of supersaturation which can be obtained before homogeneous nucleation processes
are activated. Sperber and Gierens (2023) highlight that for slow updrafts the amount of generated ice crystals could however
become large enough to reduce the supersaturation limit. This could lead to incorporate the vertical velocity in the expression
455 of this coefficient. In a general way we acknowledge that cloud formation processes, and then supersaturation w.r.t ice will



be better represented in NWP models involving more detailed physical processes, including aerosols, with 2-moment schemes that better represent the physics of nucleation and crystal growth in a complex background (Vié et al., 2016; Thompson et al., 2024; Seifert, 2024). However, the balance of computational costs and improved forecast benefits needs to be carefully assessed before implementing such a complex scheme into an operational system.

460 Finally, we decided to focus this study on the Europe and North Atlantic domain due to the high density of aircraft in this area, which provides a large number of available observations (Teoh et al., 2024). However, we believe that this work could be extended to tropical regions. In this case, it might be calibrated accordingly, given that tropical climates differ from mid-latitude regions and the occurrence of ISSRs depends on factors such as dominant deep convection (Spichtinger and Leschner, 2016). The final steps towards operationalizing the modified scheme are to verify the impact on the general parameters of the global
465 NWP model (temperature, wind, etc.) and to adjust all the parameterizations accordingly. Indeed, modifying the cloud scheme, and in particular the representation of cirrus clouds, has a feedback effect on the radiation balance, which plays a decisive role in the model's outcomes.

6.2 Verification methodology

In this work, particular attention has been paid to the definition of appropriate verification metrics. In addition to traditional
470 verification methods on humidity variable (e.g. Frequency histograms, Mean Absolute Error), the statistical results emphasize the importance of adopting a neighborhood approach when evaluating the capacity of a model to discriminate ISSRs. Introducing a neighborhood tolerance allows to link the quality of the forecast to a spatial scale, as well as addressing several scoring issues (e.g. double penalty, observation uncertainty, interpolation on gridded data). The trajectory-neighborhood method is intuitive, simple to implement and results can be interpreted in the frame of a flight trajectory. However, it does not include
475 forecast information on the adjacent vertical levels, nor of points to the right or left of the flight trajectory. Consequently, the method compromises between maintaining symmetry in dealing with forecasts and observations and ensuring straightforward interpretation with the flight trajectory, while disregarding the potential to consider forecasts of ISSRs that may be offset to one side of the flight trajectory.

The verification metrics HR, FAR and F_{β} -score with the use of a neighborhood tolerance, give easily interpretable informa-
480 tion on spatial scales at which a certain degree of correspondence between observed and forecast events is achieved, but this methodology can hide biases and should be completed by its estimation to have a complete overview of the performances of the forecasts. The FSS score is less directly interpretable, but provides a summary of all the factors that can assess NWP model quality (including true negatives in the verification). The Recall-Precision plot has shown to be a valuable tool to measure the sensitivity of different NWP models to RH_{ice} decision threshold, and provide a full NWP model inter-comparison outcome.
485 Further verification metrics could also be explored by methods based on neighborhood-populating contingency tables (e.g. Gilleland et al., 2009; Schwartz, 2017; Stein and Stoop, 2019), each method having their qualities and drawbacks regarding for example inconsistent event definitions or keeping symmetry between hit and false alarm calculations. Other advanced spatial verification techniques, such as object-based methods (Wolff et al., 2014) could provide further information on NWP model



quality, for example by targeting most significant ISSR features. However, implementing this kind of methodology can present
490 some challenges regarding mathematical data processing to obtain geometrically coherent ISSR features.

In future works, complementary observational dataset could be useful for further verification of the NWP models. For
instance, radiosonde observations could provide information on the vertical profile of humidity and temperature (e.g. Bland
et al., 2021; Thompson et al., 2024). Also, contrails tracked using satellite imagery, ground-based cameras and lidars (Vazquez-
Navarro et al., 2010; Kulik, 2019; Chevallier et al., 2023), along with flight and ground-based contrail observations (Curat and
495 Péchaud, 2023, COOP Program) represent an additional data source. However, verification is less direct, as both contrail
formation (Schmidt-Appleman) and its persistence (ISSR) must be considered together.

6.3 Performances of NWP models for ISSR discrimination and potential use for contrail avoidance application

This study shows that ARP-new has an enhanced agreement with RH_{ice} observations from IAGOS measurements in the UTLS
when compared to ARP-op. Results of Sect. 5.1 show that it corrects the dry bias of RH_{ice} above 70 % and overcomes the limit
500 at 100 % that the operational model exhibits. However, it over-predicts slightly occurrences of RH_{ice} in the range of 105 % to
115 % and under-predicts values above 115 %. As a confirmation of previous studies, IFS exhibits also a capability to produce
supersaturation w.r.t ice, but with an overestimation of values very close to 100 %, a general underestimation of ISSRs, and a
shortcoming in representing values above 105 %.

In terms of model performance to detect ISSR events, ARP-new and IFS models show close skills as shown by the FSS score
505 verification in Sect. 5.2.2. For ARP-new, HR and FAR results indicate that when ISSR was observed in IAGOS, an ISSR was
forecast in a 150 km upstream or downstream the trajectory (i.e. 10 min of flight) in ~ 80 % of the cases. Symmetrically when an
ISSR was forecast, ISSR event could be observed in ~ 70 % of the cases. This indicates a rather good spatial correspondence
between forecasts and observations. For IFS, the scores are even better but must be tempered because of the IFS dry bias
which is artificially corrected when neighborhood tolerance is applied. These statistical results are well illustrated by the case
510 study presented in Sect. 5.4. On this case, the correspondence between forecast and observation patterns is exhibited for both
ARPEGE and IFS models on RH_{ice} spatio-temporal evolution. On the one hand, ARP-new corresponds closely to observations
in the ISSR zones. On the other hand, ARP-op and, to a lesser extent, IFS show underestimation of the highest RH_{ice} values in
accordance with their statistical dry bias on ISSR.

The sensitivity study driven on the RH_{ice} threshold provides additional information. In particular, it allows a comparison on
515 NWP model skills for detecting ISSR events, relaxing the constraint on the choice of RH_{ice} decision thresholds in the forecast.
This comparison shows that ARP-new outperforms IFS in predicting the highest supersaturated events and that, conversely,
IFS outperforms ARP-new when slight undersaturation thresholds are considered. In addition, the range of HR and FAR pairs
that can be obtained by each model with adjusted thresholds is measured. It shows that even without allowing supersaturation,
the ARP-op has also skill for discriminating ISSRs, similar to ARP-new if decision thresholds lower than 100 % are applied,
520 which is a major conclusion of this work. This suggests that post-processing recalibration of RH_{ice} outputs can be a workable
strategy to use non-allowing supersaturation NWP forecast such as ARP-op. Finally, the study shows that IFS and ARP-new
recall-precision curves have a shortcoming on precision when decision thresholds greater than a certain amount (98 % for IFS,



resp. 110 % for ARP-new) are applied in the forecast. Indeed, while higher thresholds should lead to greater success ratio of ISSR forecasts, the results show a stagnation of precision beyond these thresholds. This is particularly true for IFS leading to
525 the conclusion that applying thresholds greater than 98 % to detect ISSR is de facto sub-optimal. We believe that this behavior should be further analyzed to understand its cause, probably related to the saturation adjustment process.

It is important to note that the comparison between different NWP models which is conducted in this study is not able to separate the specific contribution of the cloud and microphysical schemes in ARPEGE or IFS regarding ISSR forecast. In a schematic view, the quality of a NWP model for predicting supersaturation w.r.t ice is the result of the quality in representing
530 several processes across various scales, among them: at the largest scales, the global circulation, which induces the positioning of high water content areas in the right geographical location, and at a lower scale the microphysical processes that allows to estimate the right amount of supersaturation reached in these areas. Comparing separately cloud schemes within the same NWP model could be done in dedicated research work but will represent a certain amount of implementation and calibration work. A first, lighter approach, which could be used to minimize the impact of global circulation on scores, would be to base
535 forecasts on the same analysis at initial time.

Moving forward to end-user verification metrics is sketched out in this work by proposing the use of spatial metrics in the verification to take into account the spatial scales of the operational context. This may involve the inclusion of a margin of uncertainty when planning avoidance strategies. For instance, according to Fig. 8, including a 150 km margin to avoid an
540 ISSR forecast helps guarantee that ~ 80 % of the ISSRs that actually occurred will be avoided, and that ~ 70 % of the flight paths will be appropriately rerouted, otherwise an ISSR would have been crossed. The introduction of the F_{β} -score is also a user-oriented approach as it allows to give differential weight in scoring to detection or precision capabilities of the forecast. Indeed, precision has a great importance in a contrail avoidance operation where supplementary CO₂ emissions are emitted.

Assessment of quality regarding contrail application requires a further step beyond this study, involving traffic and use of climate metrics with associated CO₂ and non-CO₂ contributions. Some additional degrees of freedom in the use of NWP
545 models in the operational context can also be obtained which opens optimization possibilities. For example, the sensitivity study on RH_{ice} decision threshold presented in this work can be used as a base for future optimization work which would tune this threshold according to climate impact metrics and operational constraints. In the same vein, the use of a multi-model approach or/and ensemble forecasts could also prove very useful for this type of trade-off problem by tuning a probability threshold on persistent contrails occurrence conditions.

550 7 Conclusions

This article presents improvements in the cloud scheme of the global ARPEGE NWP model to allow the representation of supersaturation w.r.t ice in the UTLS. This study goes hand to hand with a verification methodology that explores NWP model skills in forecasting RH_{ice}, within the context of persistent contrail mitigation applications. Forecasts of ARPEGE with the modified cloud scheme, are compared to the non-modified (operational) ARPEGE and the IFS model from ECMWF which



555 already implements a supersaturation parametrization. The models are evaluated against aircraft in situ measurements of UTLS humidity from the IAGOS program. Here are the main conclusions of the study:

- The modified cloud scheme allows supersaturation and bias correction for humidity, showing close alignment with the RH_{ice} distribution of in situ aircraft measurements. This modification does not require any major algorithmic changes or additional computational effort. In addition, the methodology used provides a framework that can be applied to similar statistical cloud schemes.
560
- Discrimination capabilities when forecasting ISSRs with the modified ARPEGE at lead terms between 6 and 18 hours show a hit rate of $\sim 80\%$ and a false alarm ratio of $\sim 30\%$ when a neighborhood tolerance of 150 km i.e. 10 min of flight is applied. These results show a good spatial agreement between forecast and observations.
- When compared to the IFS forecast, the modified ARPEGE model exhibits a potential improvement in the representation of RH_{ice} distribution around and beyond saturation. Regarding ISSR discrimination skills, the modified ARPEGE exhibits broadly similar capabilities to those of IFS, better for IFS when slightly subsaturated events are considered, and better for modified ARPEGE when high supersaturated events are considered. In both cases, the models have shortcomings in representing the highest values of RH_{ice} ($>105\text{-}110\%$ for IFS, $>115\%$ for ARPEGE).
565
- Scores show that the operational ARPEGE, even without supersaturation physics, can also be used to discriminate ISSRs provided that a RH_{ice} decision threshold lower than 100% is applied. For IFS, using a RH_{ice} threshold of 100% to detect ISSR is shown to be sub-optimal and lower thresholds (98%) seem to be more appropriate. This suggests that post-processing recalibration of RH_{ice} outputs could be a viable solution when using NWP forecasts with non-allowing supersaturation schemes or more generally biased humidity outputs. However, it implies supplementary complexity for end-users. A model like the modified ARPEGE could allow for direct implementation without the need for adjustments, enabling flight trajectory optimization testing without additional effort.
570
575
- With regard to ISSR verification methodologies, the benefits of using spatial metrics are demonstrated. Indeed, in addition to solving traditional scoring issues like double penalty, spatial metrics are useful to relate the forecast skills at different spatial scales to the end-user application: here the avoidance margin applied to ISSR forecasts when rerouting flight paths. Sensitivity study is also conducted on humidity decision thresholds in order to comprehensively assess performance and make meaningful comparisons between discrimination skills of NWP models.
580

In the short term, the main perspectives will be to make the modified scheme operational, which involves: coupling the assimilation, analyzing the impact on the ARPEGE general circulation on a global scale, and readjusting the parameter set according to the results, if necessary. Additional checks may also be carried out using complementary observations (e.g. radiosondes) to study the performance of the models in capturing the vertical extent of ISSRs, which can be essential for avoidance strategies.
585 As part of CICONIA SESAR Joint Undertaking (2023), with end-user partners, work on cost/loss metrics linking NWP model ISSR discrimination capabilities to traffic and climate metrics with associated CO_2 and non- CO_2 contributions is underway to explore the feasibility of avoidance scenarios.



Appendix A: Modified Smith cloud scheme calculations

A1 General expressions of cloud fraction and mean water content

590 The mean cloud fraction is given by the integration of $q_t - kq_{sat}$ distribution $G_{[Q_{c,k}, \sigma_{s,k}]}$ for positive values only, which corresponds the cloudy part of the grid-box:

$$C^+ = \int_0^{+\infty} G_{[Q_{c,k}, \sigma_{s,k}]}(q) dq. \quad (A1)$$

Introducing $t = (q - Q_{c,k})/\sigma_{s,k}$ scaling gives:

$$C^+ = \int_{-Q_{c,k}/\sigma_{s,k}}^{+\infty} G_{[0,1]}(t) dt, \quad (A2)$$

595 where $G_{[0,1]}$ is the centred and reduced probability distribution.

In a similar way, the mean condensate content after adjustment \bar{q}_c^+ is given by the expectation formula using the $q_t - q_{sat}$ distribution. The integration is proceeded on the cloudy part of the grid-box. In order to get a workable expression, it is assumed that $q_t - kq_{sat} > 0$ coincides with the highest values of $q_t - q_{sat}$. This allows to calculate \bar{q}_c^+ such that

$$\bar{q}_c^+ = \int_{q^*}^{+\infty} G_{[Q_{c,1}, \sigma_{s,1}]}(q) \cdot q dq, \quad (A3)$$

600 where the lower bound of the interval q^* is implicitly defined to ensure cloud fraction consistency with C^+ found in (A2) as shown in Fig. A1. This condition gives the following equality:

$$\int_{q^*}^{+\infty} G_{[Q_{c,1}, \sigma_{s,1}]}(q) dq = \int_0^{+\infty} G_{[Q_{c,k}, \sigma_{s,k}]}(q) dq = C^+. \quad (A4)$$

Re-scaling left and right members of equation (A4) by $t = (q - Q_{c,1})/\sigma_{s,1}$ (left) and $t = (q - Q_{c,k})/\sigma_{s,k}$ (right) leads to:

$$\int_{(q^* - Q_{c,1})/\sigma_{s,1}}^{+\infty} G_{[0,1]}(t) dt = \int_{-Q_{c,k}/\sigma_{s,k}}^{+\infty} G_{[0,1]}(t) dt \quad (A5)$$

605 which, by identification of lower integration bounds gives:

$$q^* = Q_{c,1} - Q_{c,k} \frac{\sigma_{s,1}}{\sigma_{s,k}}. \quad (A6)$$

This expression leads to the following formulation for the computation of the mean condensate content:

$$\bar{q}_c^+ = \int_{Q_{c,1} - Q_{c,k} \frac{\sigma_{s,1}}{\sigma_{s,k}}}^{+\infty} G_{[Q_{c,1}, \sigma_{s,1}]}(q) \cdot q dq. \quad (A7)$$

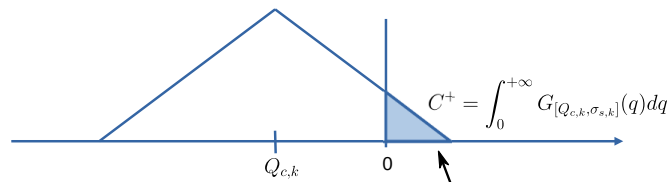


Then, introducing $t = (q - Q_{c,1}) / \sigma_{s,1}$ scaling gives the following expression for the mean cloud water content after adjustment:

610

$$\bar{q}_c^+ = \sigma_{s,1} \int_{-Q_{c,k}/\sigma_{s,k}}^{+\infty} G_{[0,1]}(t) \left(t + \frac{Q_{c,1}}{\sigma_{s,1}} \right) dt. \quad (\text{A8})$$

Distribution of $q_t - kq_{sat} \sim G_{[Q_{c,k}, \sigma_{s,k}]}$



Distribution of $q_t - q_{sat} \sim G_{[Q_{c,1}, \sigma_{s,1}]}$

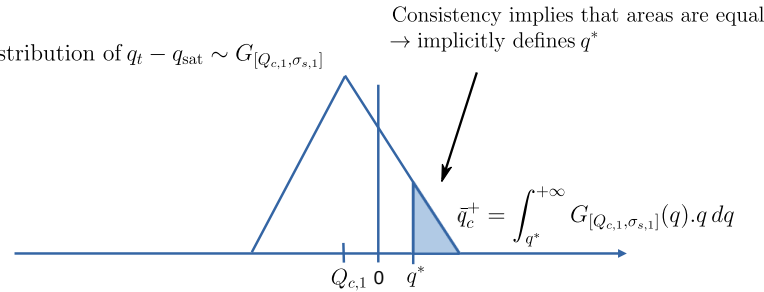


Figure A1. Illustration of integration steps to compute the mean cloud fraction C^+ and the mean condensate content \bar{q}_c^+ within the grid-box with triangular distributions. The first step is the integration of $q_t - kq_{sat}$ distribution on its positive support in order to compute cloudiness C^+ . The second step is the integration of local cloud contents defined by the $q_t - q_{sat}$ distribution on the grid-box cloudy part, leading to \bar{q}_c^+ . In this second step, the integration domain is $[q^*, +\infty[$ where q^* is defined to ensure consistency on cloudiness computation.

A2 Application with a triangular distribution

Symmetric triangular probability law is given by the following set of equations:

$$G_{[0,1]}(t) = \begin{cases} 0 & t \leq -\sqrt{6} \\ \frac{1}{6}t + \frac{1}{\sqrt{6}} & -\sqrt{6} < t \leq 0 \\ -\frac{1}{6}t + \frac{1}{\sqrt{6}} & 0 < t \leq \sqrt{6} \\ 0 & t > \sqrt{6} \end{cases} \quad (\text{A9})$$



615 Easier calculations are obtained by introducing a re-scaled function $H(T) = \sqrt{6}G_{[0,1]}(\sqrt{6}T)$:

$$H(t) = \begin{cases} 0 & T \leq -1 \\ 1+T & -1 < T \leq 0 \\ 1-T & 0 < T \leq 1 \\ 0 & T > 1 \end{cases} \quad (\text{A10})$$

A2.1 Computation of cloud fraction C^+

Integration of the cloud fraction can be expressed in the following manner:

$$C^+ = \int_{-Q_{c,k}/\sigma_{s,k}}^{+\infty} G_{[0,1]}(t) dt = \int_{-\alpha_k\sqrt{6}}^{+\infty} G_{[0,1]}(t) dt = \int_{-\alpha_k}^{+\infty} \sqrt{6} G_{[0,1]}(\sqrt{6}T) dT = \int_{-\alpha_k}^{+\infty} H(T) dT. \quad (\text{A11})$$

620 **Case 1:** $\alpha_k \leq -1$

If $\alpha_k \leq -1$, the lower bound of integration is greater than 1 then $C^+ = 0$.

Case 2: $-1 < \alpha_k \leq 0$

If $-1 < \alpha_k \leq 0$, then $0 < -\alpha_k \leq 1$:

$$C^+ = \int_{-\alpha_k}^1 1-T dT = \frac{1}{2} (1 + \alpha_k)^2. \quad (\text{A12})$$

625 **Case 3:** $0 < \alpha_k \leq 1$

If $0 < \alpha_k \leq 1$, then $-1 < -\alpha_k \leq 0$:

$$C^+ = \int_{-\alpha_k}^0 1+T dT + \int_0^1 1-T dT = \int_{-\alpha_k}^0 1+T dT + \frac{1}{2} = \frac{1}{2} - \frac{1}{2} (1 - \alpha_k)^2 + \frac{1}{2} = 1 - \frac{1}{2} (1 - \alpha_k)^2. \quad (\text{A13})$$

Case 4: $\alpha_k > -1$

In this case, $-\alpha_k < -1$, and result can be inferred from case 3:

$$630 \quad C^+ = \int_{-1}^0 1+T dT + \int_0^1 1-T dT = 1. \quad (\text{A14})$$

A2.2 Computation of mean condensed water \bar{q}_c^+

Integration of mean water content can be expressed in the following manner:

$$\bar{q}_c^+ = \sigma_{s,1} \int_{-Q_{c,k}/\sigma_{s,k}}^{+\infty} G_{[0,1]}(t) \left(t + \frac{Q_{c,1}}{\sigma_{s,1}} \right) dt = \sigma_{s,1} \int_{-\alpha_k\sqrt{6}}^{+\infty} G_{[0,1]}(t) \left(t + \alpha_1\sqrt{6} \right) dt = \sigma_{s,1}\sqrt{6} \int_{-\alpha_k}^{+\infty} H(T) (\alpha_1 + T) dT. \quad (\text{A15})$$



Case 1: $\alpha_k \leq -1$

635 If $\alpha_k \leq -1$, the lower bound of integration is greater than 1 then $q_c^+ = 0$.

Case 2: $-1 < \alpha_k \leq 0$

If $-1 < \alpha_k \leq 0$, then $0 < -\alpha_k \leq 1$:

$$\bar{q}_c^+ = \sigma_{s,1} \sqrt{6} \int_{-\alpha_k}^1 (1-T)(\alpha_1+T) dT. \quad (\text{A16})$$

Using integration by parts gives:

$$640 \quad \bar{q}_c^+ = \frac{\sigma_{s,1} \sqrt{6}}{2} \int_{-\alpha_k}^1 (1-T)^2 dT - \frac{\sigma_{s,1} \sqrt{6}}{2} [(1-T)^2(\alpha_1+T)]_{-\alpha_k}^1 \quad (\text{A17})$$

$$= \frac{\sigma_{s,1}}{\sqrt{6}} (1+\alpha_k)^3 + \frac{\sigma_{s,1} \sqrt{6}}{2} [(1+\alpha_k)^2(\alpha_1-\alpha_k)]. \quad (\text{A18})$$

Case 3: $0 < \alpha_k \leq 1$

If $0 < \alpha_k \leq 1$, then $-1 < -\alpha_k \leq 0$:

$$\bar{q}_c^+ = \sigma_{s,1} \sqrt{6} \int_{-\alpha_k}^0 (1+T)(\alpha_1+T) dT + \sigma_{s,1} \sqrt{6} \int_0^1 (1-T)(\alpha_1+T) dT. \quad (\text{A19})$$

645 Applying integration by parts on the first integral and using results of case 2 for the second integral gives:

$$\bar{q}_c^+ = \frac{\sigma_{s,1} \sqrt{6}}{2} \int_{-\alpha_k}^0 (1+T)^2 dT - \frac{\sigma_{s,1} \sqrt{6}}{2} [(1+T)^2(\alpha_1+T)]_{-\alpha_k}^0 + \left[\frac{\sigma_{s,1}}{\sqrt{6}} + \frac{\sigma_{s,1} \alpha_1 \sqrt{6}}{2} \right] \quad (\text{A20})$$

$$= -\frac{\sigma_{s,1}}{\sqrt{6}} [(1+T)^3]_{-\alpha_k}^0 + \frac{\sigma_{s,1} \sqrt{6}}{2} [(1+T)^2(\alpha_1+T)]_{-\alpha_k}^0 + \left[\frac{\sigma_{s,1}}{\sqrt{6}} + \frac{\sigma_{s,1} \alpha_1 \sqrt{6}}{2} \right] \quad (\text{A21})$$

$$= -\frac{\sigma_{s,1}}{\sqrt{6}} + \frac{\sigma_{s,1}}{\sqrt{6}} (1-\alpha_k)^3 + \frac{\sigma_{s,1} \alpha_1 \sqrt{6}}{2} - \frac{\sigma_{s,1} \sqrt{6}}{2} (1-\alpha_k)^2 (\alpha_1-\alpha_k) + \frac{\sigma_{s,1}}{\sqrt{6}} + \frac{\sigma_{s,1} \alpha_1 \sqrt{6}}{2} \quad (\text{A22})$$

$$= \sigma_{s,1} \alpha_1 \sqrt{6} + \frac{\sigma_{s,1}}{\sqrt{6}} (1-\alpha_k)^3 - \frac{\sigma_{s,1} \sqrt{6}}{2} (1-\alpha_k)^2 (\alpha_1-\alpha_k). \quad (\text{A23})$$

650 **Case 4:** $\alpha_k > 1$

In this case, $-\alpha_k < -1$, then,

$$\bar{q}_c^+ = \sigma_{s,1} \sqrt{6} \int_{-1}^0 (1+T)(\alpha_1+T) dT + \sigma_{s,1} \sqrt{6} \int_0^1 (1-T)(\alpha_1+T) dT. \quad (\text{A24})$$

Expression of q_c^+ can be inferred from case 3 by setting $\alpha_k = 1$. We obtain:

$$\bar{q}_c^+ = \sigma_{s,1} \alpha_1 \sqrt{6}. \quad (\text{A25})$$



655 *Code and data availability.* The Python code and the processed data that support the findings of this study and reproduce the main figures in this article are openly available at <https://doi.org/10.5281/zenodo.15303979> (Arriolabengoa, 2025). The IAGOS data can be downloaded from the IAGOS data portal at <https://doi.org/10.25326/06> (Boulangier et al., 2020). The forecast data used here are available upon reasonable request from the corresponding authors.

660 *Author contributions.* SA, PC, OJ and YB developed the modification of the ARPEGE cloud scheme. YL and AP prepared and provided the IAGOS dataset. SA and PC developed the verification methodology. SA and OJ carried out the implementation of the new scheme in ARPEGE. SA, PC and MP took the lead in writing the manuscript. YB, MP and BV supervised the findings of this work. All authors provided critical feedback and helped shape the research, analysis and manuscript.

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