





# Towards selective Ir/IrO<sub>2</sub> electrochemical dissolution of Ir-based electrocatalysts for enhanced proton exchange membrane water electrolyzer sustainability

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## HIGHLIGHTS

- Investigation of bifunctional Pt-Ir/C and Pt-IrO<sub>2</sub>/C OER electrocatalysts.
- Treatment protocol influences the respective dissolution rates of Pt and Ir.
- Selective Ir dissolution in OER electrocatalysts.
- Proof-of-concept demonstration for Ir recycling.

## ARTICLE INFO

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## ABSTRACT

Electrocatalysts containing Ir are commonly used in energy conversion devices such as proton exchange membrane water electrolyzers (PEMWEs). However, the scarcity and high cost of Ir hinder their large-scale use. Therefore, there is a need for advanced Ir recycling schemes when scaling up PEMWE technology. Prior work on Pt-IrO<sub>2</sub>/C nanocomposite catalysts indicates that IrO<sub>2</sub> has limited resistance to electrochemical degradation. Here, we built upon this observation to explore the selective dissolution of Ir/IrO<sub>2</sub> compared to Pt, using a scanning flow cell coupled to inductively coupled plasma mass spectrometry (SFC ICP-MS). We show that IrO<sub>2</sub> can even be selectively dissolved using a simple two-electrode setup. These findings are not only of fundamental interest for catalyst design but also highlight a potential pathway of electrochemically induced Ir recycling and regeneration strategies.

## 1. Introduction

One of the primary obstacles to the widespread commercialization of electrochemical energy conversion devices, such as proton exchange membrane water electrolysis (PEMWE) and proton exchange membrane fuel cells (PEMFCs), is the scarcity of the precious metals required to facilitate the electrochemical reactions [1–9]. Specifically, platinum (Pt) and iridium (Ir) are essential but limited resources, being among the rarest elements in the Earth's crust. The scarcity of these precious metals

not only drives up their prices but also poses challenges to the scalability of the conversion devices. Several analyses have been published on the implications of limited Pt and Ir resources for PEMFC and PEMWE technologies, respectively [1–3,6]. While it is beyond the scope of this study to discuss this aspect in detail, a rough “back on the envelope” estimation reveals that considering an assumed requirement of 500 kg of Ir per GW and an annual Ir mining of approximately 4 tons, only 8 GW a<sup>-1</sup> could be achieved – even if all mined Ir was allocated for PEMWEs, which is hardly a realistic scenario [1].

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Considering that to achieve renewable energy ‘production and storage’, often referred to as the “TeraWatt Challenge” [10], it becomes evident that the aforementioned estimations underscore the need for further advancements in catalysts for PEMWEs. However, equally significant is the urgent need to develop effective recycling schemes for precious metals. For instance, if implementing closed-loop Ir recycling by 2035, the PEMWE installed capacity in 2050 would increase by ~2.7x compared to that with no Ir recycling [11]. Platinum group metals (PGMs) are highly resistant to corrosion as well as electrically and thermally stable. Most literature concerning PGM recycling concentrates on Pt, Rh, and Pd, which are used in catalytic converters for cars [12]. The recycling schemes typically involve hydrometallurgical treatment of spent catalysts and focus on the leaching and separation of the individual elements [13]. For instance, certain recycling schemes involve the use of hot fuming *aqua regia* or pressurized alkaline cyanide solutions [14,15], which not only consume significant amounts of energy but are also harmful to the environment. Therefore, there is a need to improve in this area. Recently, an ‘electrode-less’ process platinum recycling scheme via induced surface potential alteration has been proposed [14]. Interestingly, in this concept, a so-called transient dissolution mechanism is exploited that is triggered by a repetitive change in platinum surface oxidation state via alternate purging with oxidizing and reducing gas. While the ‘electrode-less’ method mentioned above does not use external electric current or electrodes, the easiest way to introduce surface potential alteration is through electrochemical means. As for Ir, recycling schemes remain scarce, the state-of-the-art extraction methods for Ir are predominantly hydrometallurgical processes, which are typically carried out at high temperatures using harsh chemicals, e.g., *aqua regia* [16], tetrafluorobromate [17], etc. In these processes, the leaching/dissolution of Ir generally constitutes the rate-determining step [18]. Only recently, Ir dissolution by electrochemical means has been proposed [19].

Here we follow this recently suggested route and explore the potential of selective Ir electrochemical dissolution from Pt-Ir/Pt-IrO<sub>2</sub> bifunctional electrocatalysts. The focus and scope of this work is on providing a proof-of-concept demonstration of selective Ir dissolution via electrochemical methods, rather than evaluating the subsequent Ir recovery. As a model system for an electrocatalyst, we employed nanocomposites [20,21], which combine different nanoparticles (Pt and IrO<sub>2</sub>/Ir) on the same carbon support material. Previously, such catalysts have been prepared as bifunctional Pt-IrO<sub>2</sub>/Pt-Ir catalysts, but they demonstrated limited electrochemical stability of IrO<sub>2</sub> during repetitive changes in the electrode potential [20,22,23]. Following this observation, we studied the model nanocomposite catalysts to demonstrate the selective dissolution of IrO<sub>2</sub>/Ir, which could serve as a conceptual framework for an electrochemical Ir recycling strategy. We tested the principle using scanning flow cell measurements coupled with inductively coupled plasma mass spectrometry (SFC-ICP-MS) [24]. This approach allows us to monitor online metal dissolution as a function of the applied electrode potential, making it ideal for evaluating various electrochemical treatment protocols. It has been reported that when Pt-IrO<sub>2</sub> bifunctional catalysts are used at a reversal-tolerant anode for PEMFC, the H<sub>2</sub> gas at the anode with elevated temperature (80 °C) can chemically reduce a few outer monolayers of the surface of IrO<sub>2</sub> nanoparticles to metallic Ir, which then is more prone to dissolution [25]. Thus, to distinguish between two pathways of Ir dissolution – via a reduction of IrO<sub>2</sub> to Ir under a hydrogen atmosphere [25] and direct IrO<sub>2</sub> dissolution – we tested inert atmosphere and air conditions, as well as metallic Ir and IrO<sub>2</sub> nanoparticles.

## 2. Experimental

### 2.1. Synthesis of supported metallic Pt and nanocomposite

The synthesis methods for supported catalysts are detailed in previous studies [20,26], which includes the microwave-assisted preparation

of metal (Pt and Ir) NPs and the post-immobilization of metal NPs onto carbon support (Vulcan XC72R). Monometallic Pt NP solution, or Pt and Ir NP solutions, were simultaneously added to carbon suspension to differentiate the obtained catalyst was supported monometallic or nanocomposite catalysts. The content of Pt and Ir NPs was kept 20 % in weight (wt.%) throughout the prepared supported catalysts.

### 2.2. Transmission electron microscopy (TEM)

TEM was used for physical characterization of the as-prepared catalysts. A Jeol 2100 transmission electron microscope operated at 200 kV was used for TEM analysis. The catalyst dispersion diluted in ethanol was dropped on carbon coated copper TEM grids (Quantifoil) for TEM sample preparation. Images were recorded at least three randomly selected areas. The representative TEM micrographs of the studied catalysts are displayed in Fig. S1.

### 2.3. Small angle X-ray scattering (SAXS)

The size distributions of the studied catalysts were evaluated by SAXS and shown in Fig. S1. SAXS measurements and data analysis were performed as detailed in the previous study [21]. The scattering data are fitted to the expression:

$$I(q) = A \cdot q^{-n} + C \cdot \int P(q, R) V(R) D(R) dR$$

Where  $A \cdot q^{-n}$  is the power law in which  $A$  and  $n$  are free parameters,  $C$  is a scaling constant,  $P$  is a sphere form factor,  $V$  is the particle volume, and  $D$  the log-normal size distribution, and the scattering vector  $q = 4\pi \cdot \sin(\theta) / \lambda$ , The sphere form factor is expressed as:

$$P_s(q, R) = \left( 3 \frac{\sin(qR) - qR \cos(qR)}{(qR)^3} \right)^2$$

and the log-normal distribution is expressed as:

$$D(R) = \frac{1}{R\sigma\sqrt{2\pi}} e^{-\left[ \frac{\ln\left(\frac{R}{R_0}\right)}{2\sigma^2} \right]^2}$$

The fitting was conducted with a home written MATLAB code. The values obtained for free parameters in the model are listed in Table S1, note that the data from 20 wt% Pt were already previously reported [21] and shown here to compare with 20 wt% Pt + 20 wt% Ir (Pt-Ir/C).

In our previous work [21] using 20 wt% Pt and 40 wt% Ir, the SAXS data were best fitted using two size populations. However the size of the Pt and Ir nanoparticles are so closed that in the case of less scattering material for a 20 wt% Pt and 20 wt% Ir, a single size model is enough to fit the data and the mean retrieved size is around 2 nm, in agreement with the expected size of the Pt and Ir nanoparticles and the rather homogenous size of the nanoparticles observed by TEM on this sample.

### 2.4. Scanning electron microscope (SEM)-based energy dispersive X-ray spectroscopy (EDX)

The compositions of nanocomposites before and after treatments were evaluated with SEM-EDX. An equipment of Zeiss Gemini 450 SEM coupled with an Oxford Instruments UltimMax 65 EDX detector was used and a voltage of 25 kV was applied for analysis. Before treatment, a Ø 3 mm of pre-filtered catalyst layer was punched and fixed on top of a sticky carbon tape, which was placed on the metallic sample holder. The catalyst layer after composition analysis served as working electrode and used for electrochemical treatment. Afterwards, the Ø 3 mm catalyst layer was transferred again to SEM-EDX to determine the change of relative Pt/Ir weight ratio during electrochemical treatment. Five

independent spots of a catalyst layer were selected for analysis for each studied sample.

### 2.5. Inductively coupled plasma mass spectrometry (ICP-MS)

The contents of the dissolved Pt and Ir in electrolyte after jacketed-based electrochemical treatment were evaluated with ICP-MS (NexION 2000 ICP-MS). The ICP-MS was equipped with a cyclonic spray chamber and a PFA-nebulizer. 5 mL of electrolyte in cell after electrochemical treatment was taken and diluted with Milli-Q water to an ideal concentration for further ICP-MS analysis.

### 2.6. Scanning flow cell with inductively coupled plasma mass spectrometry (SFC-ICP-MS)

The outlet of scanning flow cell (SFC) was coupled with inductively coupled plasma mass spectrometry (ICP-MS) to detect dissolved metal ions during the applied electrochemical protocol. An Ar-purged 0.05 M H<sub>2</sub>SO<sub>4</sub> electrolyte was prepared by diluting concentrated H<sub>2</sub>SO<sub>4</sub> (Suprapure 96 %, Merck) with ultrapure water and then circulated through the SFC. Before entering the ICP-MS, an internal standard was introduced at a 1:1 mixing ratio using an ICP-MS peristaltic pump, with a flow rate of approximately 3.5  $\mu\text{L/s}$ . The counter electrode (graphite rod, 5 mm, HTW Sigradur G) and reference electrode (Ag/AgCl, Metrohm, Germany) were positioned at the SFC inlet and outlet. The working electrodes were prepared by drop-casting method onto glassy carbon (5  $\times$  5 cm, Sigradur G, HTW) backing electrode and approached from above with an XYZ position stage. All the electrodes were connected to a Gamry Reference 600 potentiostat (Gamry Instruments), while the potentials were calibrated against the RHE scale. ICP-MS instruments, PerkinElmer NexION 350X and 300X, were calibrated using 3-point calibration with solutions of investigated elements. Internal standard solutions were used to monitor potential instrument drifts and matrix effects. Further details can be found in our previous publications.

### 2.7. Preparation of working electrodes for SFC-ICP-MS measurements

The working electrodes were prepared by dispersing the powder in a 7:1 ratio of H<sub>2</sub>O (Merck, Milli-Q IQ 7000, 18 M $\Omega$ , total organic carbon < (TOC) < 3 ppb) and isopropanol (Emsure®, Merck,  $\geq 99.8$  % purity). To prevent catalyst detachment, Nafion ionomer solution (D-520, Sigma Aldrich, 5 wt %) was used as a binder at a catalyst-to-ionomer weight ratio of 4:1. The mixture underwent 15 min of sonication in an ice bath using a horn sonicator (Branson Ultrasonics SFX150) with 4 s on/2 s off pulses. Following sonication, the pH was adjusted to around 11 using 1 M KOH before drop-casting a 0.2  $\mu\text{L}$  suspension (0.66 mg/mL) onto glassy carbon (GC) substrates (5  $\times$  5 cm<sup>2</sup>, Sigradur G, HTW). The estimated catalyst loading of approximately 10  $\mu\text{g cm}^{-2}$  depended on the size of the catalyst ink spots, as evaluated using a Keyence VK-X250 profilometer.

### 2.8. Preparation of working electrodes for jacket-type cell measurements

The catalyst layer (nominal loading of 200  $\mu\text{g}_{\text{Pt/Ir}} \text{cm}_{\text{geo}}^{-2}$ ) was fabricated via vacuum filtration, which was detailed elsewhere [27]. Afterwards, a rectangular carbon-based GDL (1 cm  $\times$  3 cm, with MPL on the top) was applied for WE fixing, in which, a  $\varnothing$  3 mm of the pre-filtered catalyst layer was punched and placed on top of the rectangular GDL, which was further fixed with Teflon tape to ensure that the  $\varnothing$  3 mm WE was stabilized and exposed to electrochemical treatments.

### 2.9. Electrochemical measurements in a jacket-type cell

All electrochemical treatments based on the more realistic catalyst loading 400  $\mu\text{g}_{\text{Ir + Pt}} \text{cm}_{\text{geo}}^{-2}$ , i.e. 1000-1200  $\mu\text{g}_{\text{Cat}} \text{cm}_{\text{geo}}^{-2}$  were performed in a three-electrode system connected with a potentiostat (ECi-200,

Nordic Electrochemistry ApS), which was controlled by a computer. A jacket-type electrochemical cell with a hollow outer layer for water circulation for temperature controlling, was used for electrochemical treatments. A carbon rod was used as counter electrode (CE), the WE was detailed in the last section. All potentials were determined with respect to RHE, which was prepared prior to each measurement. Electrochemical measurements were conducted in air at 40 °C, maintained by circulating water through the outer layer of the jacket-type cell. After reaching the set temperature, an additional 10 min equilibration period was allowed to ensure the electrolyte within the inner compartment attained the target temperature. The electrolyte was stirred using a magnetic stirrer during measurements. Different electrolyte (1 M H<sub>2</sub>SO<sub>4</sub>, 1 M HClO<sub>4</sub>, 1 M HNO<sub>3</sub> and 1 M H<sub>2</sub>SO<sub>4</sub> + 0.5 M CH<sub>3</sub>OH) was used for electrochemical treatments. The following procedures were implemented sequentially in treatments: catalyst surface cleaning, catalyst oxidation/activation (only for nanocomposite) and degradation. For supported monometallic Pt/C, continuously swept potential between 0.05 and 1.10 V vs RHE at a scan rate of 500 mV s<sup>-1</sup> served as a typical protocol for catalyst surface cleaning,  $\sim 30$  repeats were performed to obtain a stable cyclic voltammograms. For supported Pt-Ir/C nanocomposite, potentials were swept in a limited window of 0.10 V–0.30 V vs RHE with a scanning speed of 100 mV s<sup>-1</sup> for  $\sim 20$  cycles, during which the solution resistance was compensated to between 2 and 3  $\Omega$  via an analog positive feedback scheme. An additional catalyst electrochemical oxidation/activation procedure by holding potential at 1.60 V vs RHE for 8 min was needed for Pt-Ir/C nanocomposites to form IrO<sub>2</sub>. Afterwards, potential was cycled between 0.05 and 1.10 V vs RHE at a scan rate of 500 mV s<sup>-1</sup> to obtain stable cyclic voltammograms. Concerning degradation test, a current control mode was employed, in which, the applied current was stepped between  $-1 \text{ mA cm}^{-2}$  and  $1 \text{ mA cm}^{-2}$  with a rest time of 1 s at each current, the total treatment lasted for 1 h. After electrochemical treatments, 5 mL of electrolyte was preserved for ICP-MS analysis.

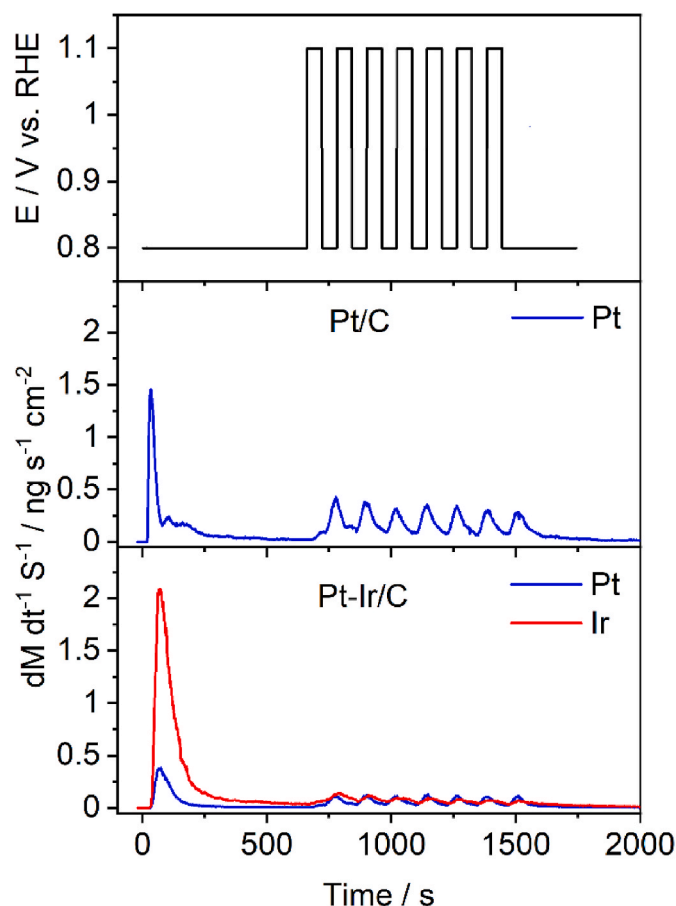
## 3. Results and discussion

### 3.1. Impact of measurement protocols on the dissolution rates of Pt and Ir from Pt-Ir/C catalysts

We begin our discussion by comparing the metal dissolution of two catalyst types: a standard Pt/C catalyst and a Pt-Ir/C nanocomposite catalyst. Both catalysts have a fixed Pt metal loading, i.e., 20 wt%, and similar particle sizes of Pt and Ir [20], as shown in Fig. S1 and Table S1. As mentioned in the introduction, to analyze the metal dissolution, we investigated thin catalyst films prepared by the drop-casting method in SFC-ICP-MS measurements [24].

For the first protocol, we choose a mild approach by applying potential steps between 0.80 and 1.10 V vs. reversible hydrogen electrode (RHE). This potential range simulates the cathode operation of PEMFCs under standard conditions. By selecting this range, our aim was to prevent the complete oxidation of Ir and the formation of an IrO<sub>2</sub> phase [28, 29]. Fig. 1 illustrates the initial dissolution of the metal upon establishing potential contact, primarily driven by the reduction of the native metal oxide formed due to catalyst exposure to air [30]. Interestingly, in the bifunctional Pt-Ir/C catalyst, the dissolution of Ir is significantly more pronounced compared to Pt. This finding can be attributed to the higher tendency for Ir to form oxide species in air, which are reduced upon establishing potential contact [30]. However, once the degradation protocol begins, both Ir and Pt dissolution occur at similar rates in the Pt-Ir/C catalyst. This finding suggests that an electrochemical recycling scheme based on such a protocol would require the separation of the individual elements after their dissolution. Nevertheless, in comparison to the standard Pt/C catalyst, the presence of Ir in the Pt-Ir/C catalyst inhibits Pt dissolution and bifunctional Pt-Ir/C catalysts can effectively mitigate the dissolution of the active Pt catalyst.

In a second protocol that was tested to identify conditions for



**Fig. 1.** Mass-specific metal dissolution rates of 20 wt% Pt/C (Pt/C, in the middle) and 20 wt% Pt + 20 wt% Ir/C (Pt-Ir/C, on the bottom). The applied treatment protocols are plotted at the same time scale as metal dissolutions. The applied potential steps between 0.80 and 1.10 V vs RHE with a rest time of 60 s on each and repeats for 7 times in total.

selective metal dissolution, the upper potential limit was adjusted from 1.10 V to 0.90 V vs RHE. As depicted in Fig. 2a, this modification in the protocol results in a reduction of Pt dissolution, while the dissolution of Ir remains unchanged as compared to that in Fig. 1. This finding aligns with a previous study that indicated the onset dissolution potentials of 0.85 V vs RHE for Ir and 0.95 V vs RHE for Pt, respectively [31]. However, altering the lower potential limit in the degradation protocol (lower voltage reached) from 0.80 to 0.05 V vs RHE has a significant influence on the dissolution of Ir, as illustrated in Fig. 2b, while it has a negligible impact on Pt dissolution. This suggests that the kinetic acceleration of Ir oxide reduction at low potentials leads to its substantial cathodic dissolution [28,32,33].

Our findings can be compared with previous studies of Pt-Ir/C bifunctional catalysts [23,25] which were performed with a focus on the activity and stability of the catalyst, not its selective dissolution. The work indicated significant performance limitations due to the dissolution of metallic Ir even at upper potential limits that were well below those experienced during abnormal operations of PEMFCs, such as hydrogen depletion conditions [34,35] and repeated start-up/shutdown cycles [36].

### 3.2. Investigation of Ir dissolution from Pt-IrO<sub>2</sub>/C catalysts

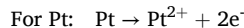
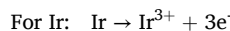
In another study [25], it was proposed that the reduction of IrO<sub>2</sub> to Ir plays a crucial role in Ir dissolution within the hydrogen atmosphere of a PEMFC anode. Consequently, we aimed to investigate whether the type of protocol proposed (e.g. shown in Fig. 2) is limited only to metallic Ir

or if IrO<sub>2</sub> is also susceptible to selective dissolution. To accomplish this, prior to the dissolution measurements we subjected the Pt-Ir/C catalyst to full activation (i.e., oxidation, see Experimental section for further details), creating a Pt-IrO<sub>2</sub>/C nanocomposite that is active for the OER [20,37,38]. We then subjected this composite to a treatment designed to trigger selective Ir dissolution. The results presented in Fig. 3 indicate that Ir dissolution is not confined to metallic Ir formed in a reductive hydrogen atmosphere. Significant Ir dissolution occurs regardless of whether Ir or IrO<sub>2</sub> is present in the catalyst. As described before, the introduction of Ir to Pt/C to form a bifunctional catalyst can protect the Pt catalyst and carbon support, but this protection comes at the cost of substantial Ir dissolution.

### 3.3. Underlying Ir/Pt dissolution mechanisms

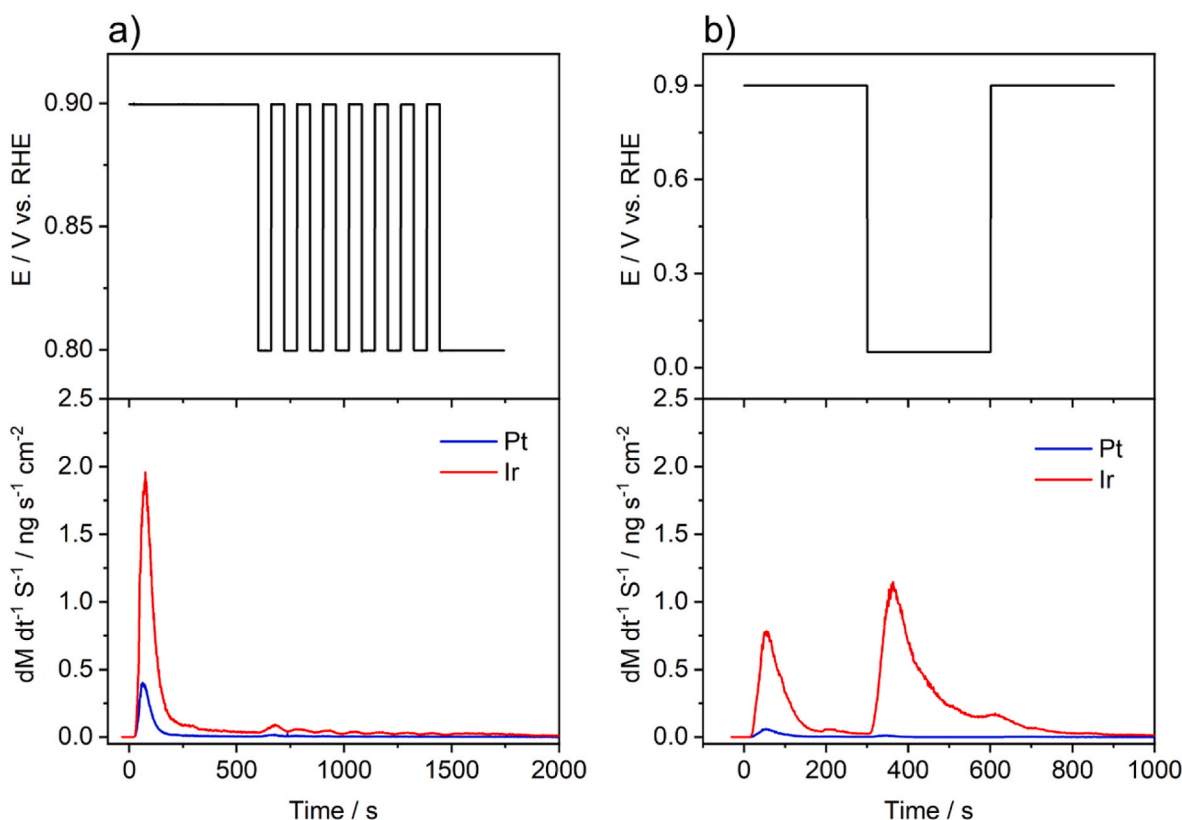
The dissolution observed in this study follows three well-established pathways for Ir [28,29,39], Pt [40–42], and other noble metals [30,32]. The first pathway emerges immediately upon contact with the electrolyte, marked by dissolution peaks associated with the reduction and/or chemical dissolution of native oxides formed during air exposure (Figs. 1–3), as discussed by Cherevko et al. [30]. In our measurements, Ir consistently exhibits larger initial peaks than Pt, suggesting the presence of thicker native oxides. The subsequent reduction of these oxides promotes greater cathodic and/or chemical dissolution, consistent with earlier observations.

A second pathway becomes active during potential transitions, where transient dissolution can occur through the loss of short-lived oxide or hydroxide species, direct electrochemical dissolution of the metal or its oxide [43], or via the place-exchange mechanism [44–47]. The latter initiates once a critical oxygen coverage is reached, producing soluble Ir<sup>3+</sup> or Pt<sup>2+</sup> prior to continuous oxide growth. Based on Pourbaix diagrams, neglecting kinetic and mass-transport effects, the thermodynamically favoured anodic reactions are:



Nernst-derived anodic dissolution “onset potentials” at 1 nM (estimated for SFC-ICP-MS measurements) are 0.98 V vs RHE for Ir (0.82 V vs RHE in other reports) and 0.92 V vs RHE for Pt, while experimental “onset potentials” of 0.85 and 0.95 V vs RHE have been reported [48]. These distinct thresholds enable selective tuning of the dissolution behaviour. In Pt-only samples pulsed between 0.8 and 1.1 V vs RHE (Fig. 1, middle), anodic dissolution via Pt–O place exchange predominates, competing with passivation, whereas cathodic transient dissolution exceeds the anodic contribution only when the upper limit surpasses 1.1 V vs RHE [40] or the lower limit falls below 0.8 V vs RHE [41].

In Pt–Ir nanocomposites (Fig. 1, bottom), pulsing between 0.8 and 1.1 V vs RHE suppresses Pt dissolution relative to Pt-only samples. Lowering the upper limit to 0.9 V vs RHE decreases Pt dissolution while leaving Ir largely unaffected (Fig. 2a), a trend reflecting Pt’s higher oxide-formation potential, which limits oxide growth and subsequent reduction at 0.8 V vs RHE, thereby reducing cathodic dissolution. In a complementary protocol (Fig. 2b), Pt dissolution is completely eliminated, while, as in the previous case, Ir dissolution remains unchanged. For Ir, most dissolution occurs during the low-potential hold due to reduction of oxide formed during the preceding anodic step, whereas for Pt, the potential is insufficient to form such oxides. The strong dependence of cathodic dissolution on the lower potential limit, and its correlation with oxide coverage, aligns with earlier studies [33,41].



**Fig. 2.** Mass-specific metal dissolution rates of Ir (red curve) and Pt (blue curve) of 20 wt% Pt + 20 wt% Ir/C (Pt-Ir/C) nanocomposite exposed to different treatments for (a) the applied potential steps between 0.90 and 0.80 V vs RHE with 60 s resting on each and repeats for 7 times and (b) the applied potential steps between 0.90 and 0.05 V vs RHE with 300 s resting on each potential. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)

The third pathway becomes dominant under OER-relevant, transpassive conditions [28,32,43], where Ir can further oxidize to  $\text{Ir}^{5+} / \text{Ir}^{6+}$ , and dissolution likely shares intermediates with the OER [49]. As shown in Fig. 3, Ir, owing to its lower OER overpotential in acid [32,43,50], facilitates both oxygen evolution and associated dissolution, whereas Pt remains largely inactive or passivated. Under these conditions, dissolution arises from combined contributions of transient anodic dissolution and steady-state dissolution coupled to the OER. Ir oxides formed during OER also promote cathodic transient dissolution in subsequent galvanostatic pulses. Over time, incomplete oxide reduction leads to progressive surface passivation [28], shifting the system from a mixed transient/steady-state regime to a predominantly steady-state dissolution mode.

### 3.4. Envisioning Ir electrochemical recycling via its selective dissolution

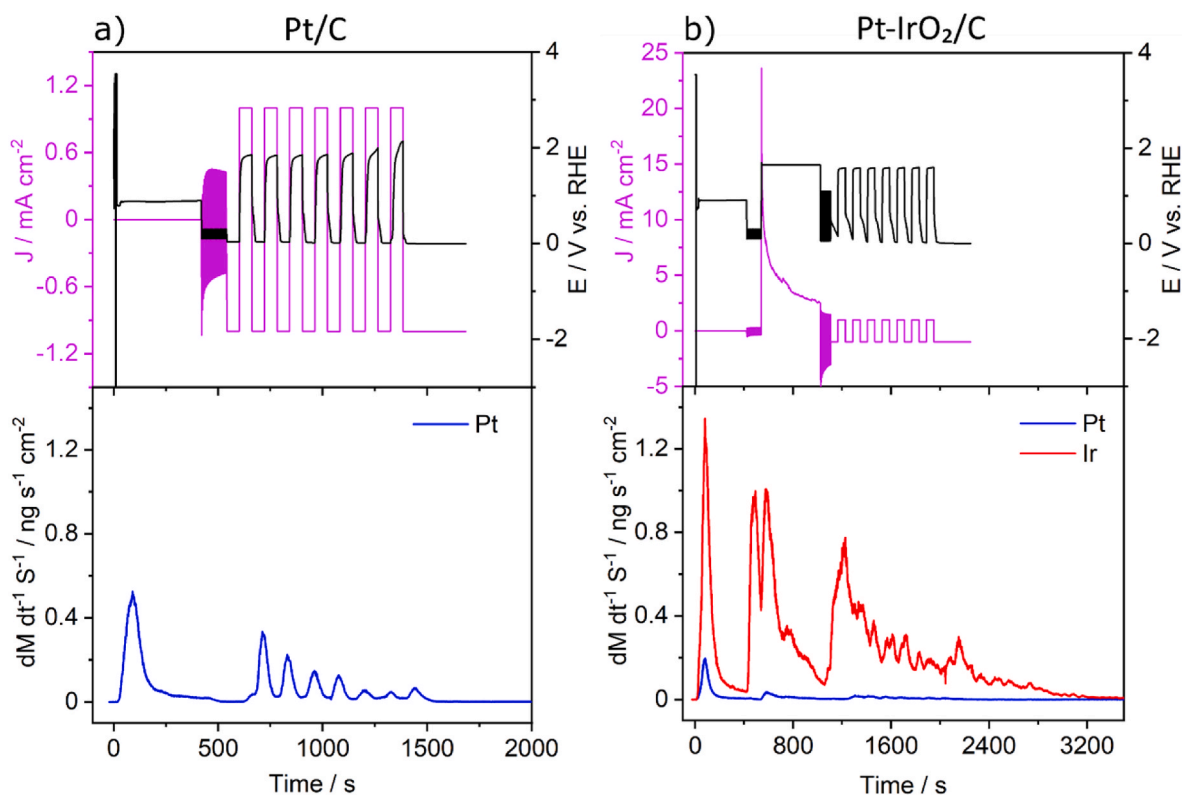
The results depicted in Figs. 2b and 3, however, unveil a fascinating aspect of Ir dissolution selectivity, which we envision to be exploitable in an electrochemical recycling scheme. Notably, when the potentials are varied between 0.90 and 0.05 V vs RHE, a selectivity in Ir dissolution of approximately 25 % is achieved, while Pt dissolution remains below 0.5 % for the Pt-Ir/C bifunctional catalyst, see Fig. 4. Furthermore, by employing a protocol that alternates the electrode current between  $+1 \text{ mA cm}^{-2}$  and  $-1 \text{ mA cm}^{-2}$  (corresponds to a potential pulse ranging from approximately 0 V–2 V vs RHE) the relative amount of dissolved Ir in comparison to dissolved Pt is significantly higher for the Pt-IrO<sub>2</sub>/C catalyst, see Fig. 3. During the current pulse, Ir dissolution is approximately 30 times higher than Pt dissolution (approximately 30 % Ir and 0.8 % Pt dissolution), and it is even possible to selectively dissolve almost all Ir (96 %) from the Pt-IrO<sub>2</sub>/C catalyst throughout the entire protocol, as detailed in Fig. 4.

In other words, in both cases, the potential excursions result in nearly exclusive Ir dissolution, while the Pt remains relatively stable. Although this phenomenon does not alleviate the limitations of bifunctional catalysts in mitigating the carbon oxidation reaction (COR) during abnormal PEMFC operations, it suggests the potential development of a low temperature electrochemical pathway for Ir recycling from bifunctional catalysts, capitalizing on the observed selectivity. Ir recycling is a crucial process for reusing Ir-containing electrocatalysts [51]. Particularly for bifunctional Pt-Ir/Pt-IrO<sub>2</sub> catalyst layers, the first step involves removing the precious metals from the catalyst layer and subsequently selectively recovering them. If selective removal from the catalyst layer can be achieved, the selective recovery of Ir and Pt would not be necessary.

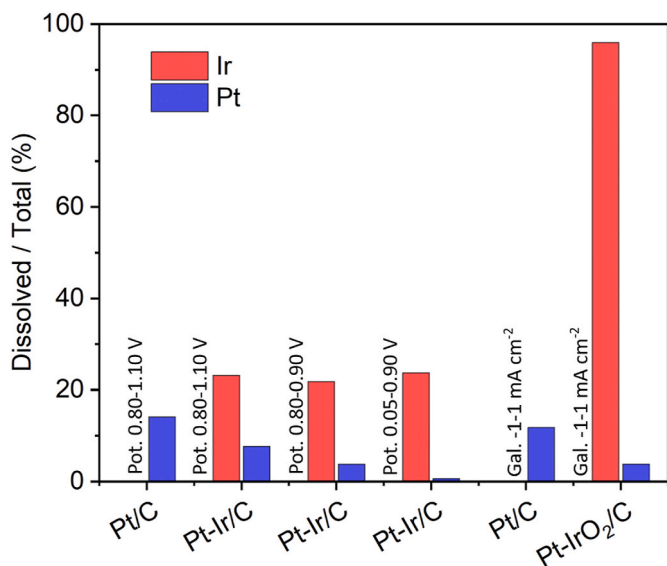
However, for an industrial metal leaching process, utilizing an electrochemical three-electrode setup as required in SFC-ICP-MS measurements is not favorable. It would be cost-intensive and limit its applicability. On the other hand, two-electrode processes, which allow for the utilization of current control (galvanostatic) protocols, are considerably less complex. As demonstrated by our results using a current control measurement protocol reported in Fig. 3, it is feasible to selectively dissolve nearly all Ir from a bifunctional Pt-IrO<sub>2</sub>/C catalyst (Fig. 4) by using such a current-based protocol. Moreover, this approach offers the advantage of being applicable in a simple two-electrode configuration, eliminating the need for a potentiostat.

### 3.5. Proof-of-concept for Ir selective dissolution using application-relevant catalyst loading onto gas diffusion layers (GDLs)

Finally, to provide proof of scalability of the presented approach, the bifunctional Pt-IrO<sub>2</sub>/C nanocomposite was evaluated at an application-relevant loading of  $400 \mu\text{g}_{\text{Pt} + \text{Ir}} \text{ cm}^{-2}$ , as outlined in Table 1. The



**Fig. 3.** Mass-specific metal dissolution rate of (a) 20 wt% Pt/C and (b) Pt (blue curves) and Ir (red curves) dissolution rates of 20 wt% Pt + 20 wt% Ir/C (Pt-IrO<sub>2</sub>/C) nanocomposites. Applied treatment protocols and metal dissolution rates are plotted at the same time scale. The treatments were started with potential cycling between 0.10 and 0.30 V vs RHE at a scan rate of 100 mV s<sup>-1</sup> for 30 cycles to reduce chemically formed native metal oxides, as indicated at ~400 s. This was followed by Ir electrochemically oxidation/activation to form bifunctional Pt-IrO<sub>2</sub>/C nanocomposite by holding potential at 1.60 V vs RHE for 8 min, subsequently, sweeping potential between 0.05 and 1.10 V vs RHE at a scan rate of 500 mV s<sup>-1</sup> for 20 cycles to stabilize the catalysts. Afterwards, switching to current control mode with current stepping between -1 mA cm<sup>-2</sup> and 1 mA cm<sup>-2</sup>, for each current the holding time is 60 s and 7 repeats in total. (For interpretation of the references to colour in this figure legend, the reader is referred to the Web version of this article.)



**Fig. 4.** Summary of total metal dissolution yields during measurements with different treatment protocols. Pt-Ir/C and Pt-IrO<sub>2</sub>/C are used to differentiate the metallic and the activated Ir in the nanocomposites, respectively. Pt and Ir are introduced with the same weight ratio (20 wt%, respectively) in the nanocomposites. Pot.: potentiostatic, Gal.: galvanostatic. All potentials are relative to RHE.

experimental measurements were conducted in a straightforward jacketed-type electrochemical cell, and the extent of metal dissolution was assessed through ICP-MS analysis of the bulk electrolyte. Additionally, scanning electron microscopy coupled with energy dispersive X-ray spectroscopy (SEM-EDX) analysis was employed to examine the elemental changes in the catalyst layers before and after treatments, allowing for the determination of Ir dissolution selectivity.

It is seen that the choice of electrolyte noticeably influences the selectivity of Ir dissolution. Nevertheless, irrespective of the tested electrolyte media, selective Ir dissolution is observed when comparing the relative changes in surface elements using SEM-EDX analysis. Among the tested electrolytes, an H<sub>2</sub>SO<sub>4</sub>-based aqueous electrolyte yields the most favorable results, i.e. higher dissolution of Ir vs. Pt, which is likely resulted from a stronger interaction of HSO<sub>4</sub><sup>-</sup> and SO<sub>4</sub><sup>2-</sup> with surface Ir atoms [52] compared with, e.g., ClO<sub>4</sub><sup>-</sup>. Methanol enhances the dissolution of Ir possibly via the facilitation of soluble IrO<sub>4</sub><sup>2-</sup> formation [19]. In contrast, the metallic Pt surface remains relatively unaffected in the corresponding potential regime (Fig. S2d in supporting information). However, when comparing offline and online dissolution measurements, it becomes apparent that the selectivity in Ir dissolution is less pronounced in a jacket-type cell. For instance, in 1 M H<sub>2</sub>SO<sub>4</sub>, the maximum Ir dissolution normalized to its total loading is approximately 15%. Several factors contribute to this observed difference. Firstly, there are variations in catalyst loadings on the working electrode. In the flow cell experiments, a typical catalyst loading of 4–10 μg<sub>Cat.</sub> cm<sup>-2</sup> was employed (see Table S2), whereas substantially higher loadings of 1000–1200 μg<sub>Cat.</sub> cm<sup>-2</sup> were used for the jacket-type cell measurements. Under these conditions, the resulting mass-normalized current densities are approx. 14 A g<sup>-1</sup> in the jacket-type cell and approx. 140 A

**Table 1**

The calculated Ir/Pt weight ratio via SEM-EDX analysis before and after treatment, the change in Ir/Pt weight ratio and the dissolved Pt and Ir amount determined by ICP-MS during treatments to 20 wt% Pt + 20 wt% Ir/C (Pt-IrO<sub>2</sub>/C). The averaged composition values in weight fraction are calculated from five different areas of catalyst layers (400 μg<sub>Ir+Pt</sub> cm<sup>-2</sup>), the calculation of Ir/Pt weight ratio change is based on the averaged wt. Ir/Pt values. All measurements are performed under 40 °C in air, and in a jacketed-type electrochemical cell. The error is the standard deviation of five independent measurements. 5 mL of electrolyte after treatment is taken out and diluted to an ideal concentration for ICP-MS measurements. ICP-MS measurements were not performed for 1 M H<sub>2</sub>SO<sub>4</sub> + 0.5 M CH<sub>3</sub>OH due to the potential harmful effects of CH<sub>3</sub>OH on the ICP-MS equipment. BOT: before test, EOT: end of test.

| Electrolyte   | BOT wt. Ir/Pt | EOT wt. Ir/Pt | wt. Ir/Pt change (%) | Pt in electrolyte (μg) | Ir in electrolyte (μg) |
|---|---------------|---------------|----------------------|------------------------|------------------------|
| 1 M H <sub>2</sub> SO <sub>4</sub>                            | 1.14 ± 0.07   | 0.44 ± 0.11   | 61.4                 | 0.570                  | 2.025                  |
| 1 M HClO <sub>4</sub>   | 1.16 ± 0.09   | 0.93 ± 0.06   | 19.8                 | 0.105                  | 0.255                  |
| 1 M HNO <sub>3</sub>  | 1.16 ± 0.12   | 0.58 ± 0.02   | 50.0                 | 0.555                  | 1.755                  |
| 1 M H <sub>2</sub> SO <sub>4</sub> + 0.5 M CH <sub>3</sub> OH | 1.19 ± 0.03   | 0.36 ± 0.03   | 69.7                 | –                      | –                      |

g<sup>-1</sup> in the SFC, representing a 10-fold higher mass-normalized current in the SFC, which results in an approx. 6.5-fold higher Ir dissolution (Table 1 and Fig. 4). Furthermore, in the jacketed-type cell, the redox processes of metal catalysts in the catalyst layer itself may be sufficient to maintain the current. In the simplest case the applied current 1 mA exclusively flows to Ir to drive its valence change between 4+ and 3+ during one current hold, which requires only about 2 μg Ir that is only one seventh of the Ir total mass (~14 μg) in catalyst layer. However, in the case of the SFC measurements, the catalyst loading is too low to sustain the current by redox processes. Instead, only the OER and hydrogen evolution reaction (HER) can maintain the applied current which requires substantially higher electrode potentials. As a consequence, the corresponding applied potentials differ. In the flow cell, the potentials varied between 0 and 2 V vs. RHE, while in the jacket-type cell, they were limited within the range of 0.70 and 1.20 V vs. RHE (Fig. S2). A third difference lies in the test environment. In a jacket-type cell, dissolved metals can redeposit onto the working electrode, whereas in a flow cell, they are flushed away. Furthermore, discrepancies in test temperatures and atmospheres may also contribute to the differences in selective Ir dissolution.

#### 4. Conclusions and outlook

We presented the preparation and investigation of bifunctional Pt-Ir/C and Pt-IrO<sub>2</sub>/C electrocatalysts using a nanocomposite concept to evaluate the viability of selective Ir electrochemical dissolution. The findings reveal that the treatment protocols employed significantly influence the dissolution rates of Pt and Ir. Comparatively, the reference catalyst, 20 wt% Pt/C, demonstrates the highest dissolution rate under both potential-based and current-based treatments when compared to the bifunctional nanocomposites. This suggests that the incorporation of Ir/IrO<sub>2</sub> in carbon-supported Pt-Ir/IrO<sub>2</sub> bifunctional catalysts effectively mitigates Pt degradation. However, it comes at the expense of substantial Ir dissolution. Thus, the inclusion of Ir/IrO<sub>2</sub> as an additional catalyst to Pt/C highlights the issue at hand but also presents a potential strategy for selectively recycling Ir.

Notably, the observation of Ir selective dissolution from Pt-Ir/IrO<sub>2</sub> bifunctional catalysts suggests that metallic Ir-based Pt-Ir/C catalysts can achieve selective Ir dissolution by lowering the potential to 0.05 V vs. RHE and subsequently switching back to 0.90 V vs. RHE, thereby minimizing Pt dissolution. Similarly, for Pt-IrO<sub>2</sub>/C catalysts, selective Ir dissolution is achieved by employing a current-based protocol that is relevant for practical application and switching between approximately 0 and 2 V vs. RHE, while maintaining Pt dissolution at a minimum.

Remarkably, nearly all (96 %) Ir can be selectively dissolved while minimizing Pt dissolution. Furthermore, the concept is demonstrated using catalyst films with realistic catalyst loading on a carbon-based GDL. Therefore, these results indicate that electrochemically selective Ir recycling, based on its preferential dissolution, could be a promising strategy to address the issue of Ir scarcity further to achieve a sustainable implementation of PEMWE technology based on PGM materials.

While the various successful proof-of-concept demonstrations

reported here on the selective dissolution of Ir, the possibility of using a 2-electrode setup, and the viability of the process at application-relevant catalyst loadings are promising, there is still room for optimization before the approach can be fully implemented at a large scale. Future areas of research include, for example, a deeper understanding of the Ir species involved, the Ir electrochemical dissolution mechanism, recovery efficiency, and/or post-recovery activity evaluation. Nevertheless, the results presented provide a solid ground for developing new strategies for Ir recovery from bifunctional catalyst layers in PEMWE.

#### CRediT authorship contribution statement

**Jia Du:** Writing – original draft, Visualization, Validation, Investigation, Data curation. **Matej Zlatař:** Writing – review & editing, Investigation, Formal analysis, Data curation. **Damin Zhang:** Writing – review & editing, Investigation, Formal analysis. **Daniel Escalera-López:** Writing – review & editing, Investigation, Formal analysis, Data curation. **Jonathan Quinson:** Writing – review & editing, Validation, Formal analysis. **Serhiy Cherevko:** Writing – review & editing, Validation, Supervision, Funding acquisition, Conceptualization. **Matthias Arenz:** Writing – review & editing, Supervision, Funding acquisition, Conceptualization.

#### Declaration of Generative AI and AI-assisted technologies in the writing process

During the preparation of this work the authors used ChatGPT to review individual sections of the manuscript to improve the readability and style of the text. After using ChatGPT, the authors reviewed and edited the content as needed and take full responsibility for the content of the publication. ChatGPT was not used to suggest, select nor include any of the references reported.

#### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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#### Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.jpowsour.2025.238224>.

## Data availability

Data will be made available on request.

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