An automated approach to magnetic divertor configuration design

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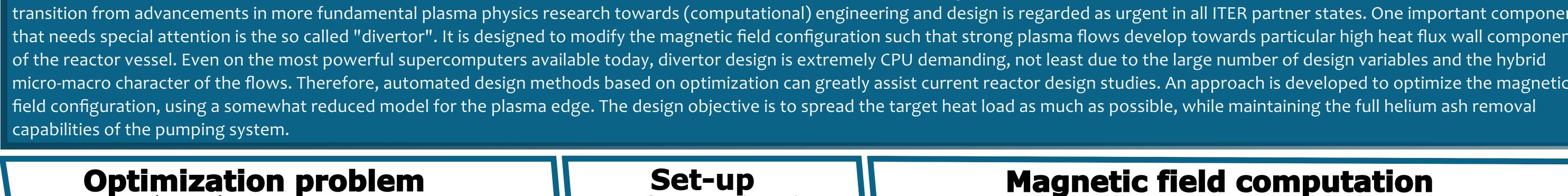
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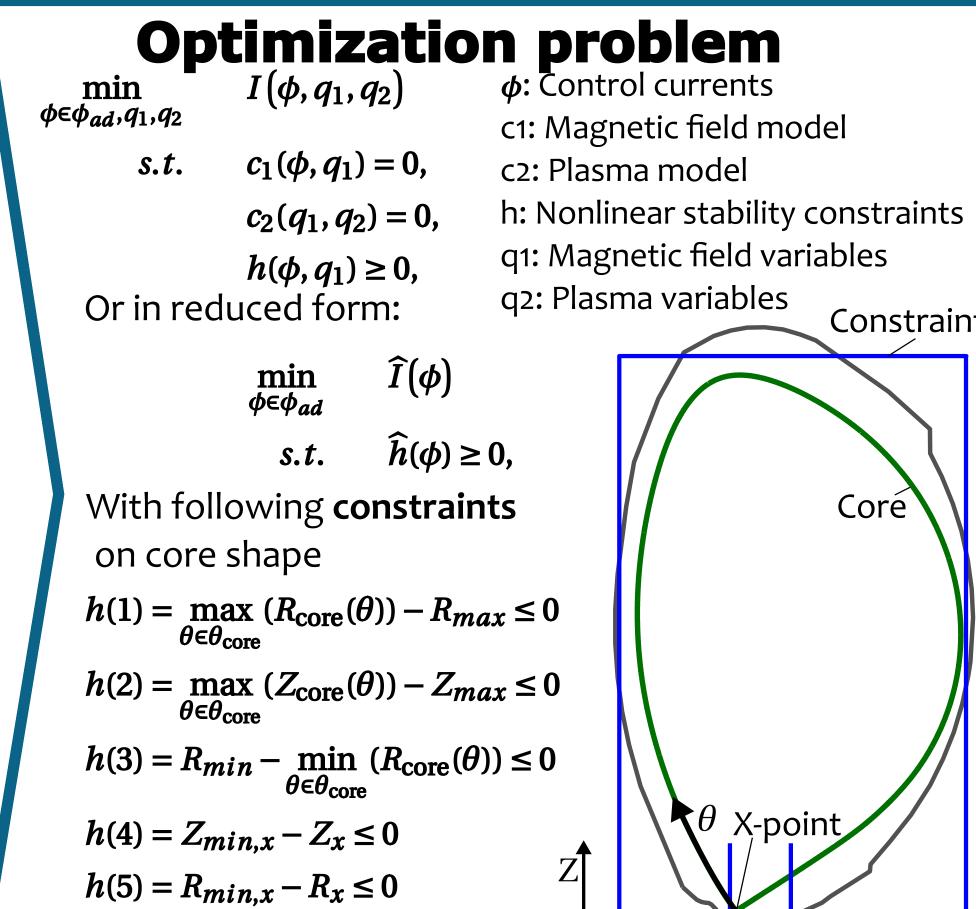
Core

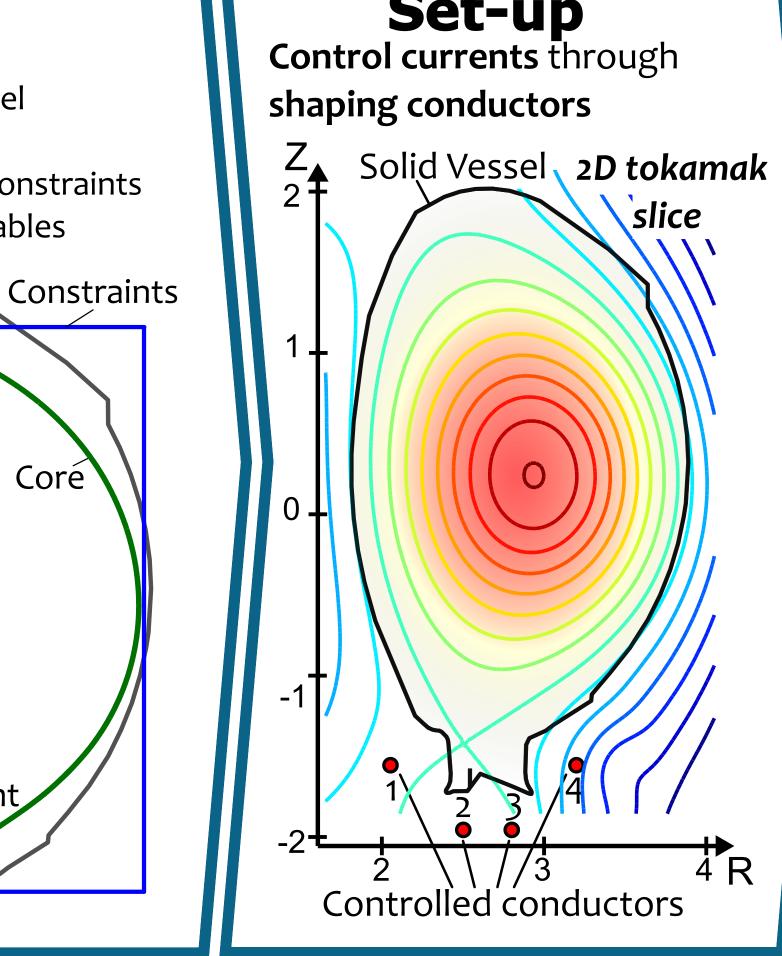
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The first fusion reactor ITER is currently under construction in Cadarache, France and fusion power plant conceptual design activities are intensified in Europe, US and Asia. Within this context the transition from advancements in more fundamental plasma physics research towards (computational) engineering and design is regarded as urgent in all ITER partner states. One important component that needs special attention is the so called "divertor". It is designed to modify the magnetic field configuration such that strong plasma flows develop towards particular high heat flux wall components of the reactor vessel. Even on the most powerful supercomputers available today, divertor design is extremely CPU demanding, not least due to the large number of design variables and the hybrid micro-macro character of the flows. Therefore, automated design methods based on optimization can greatly assist current reactor design studies. An approach is developed to optimize the magnetic



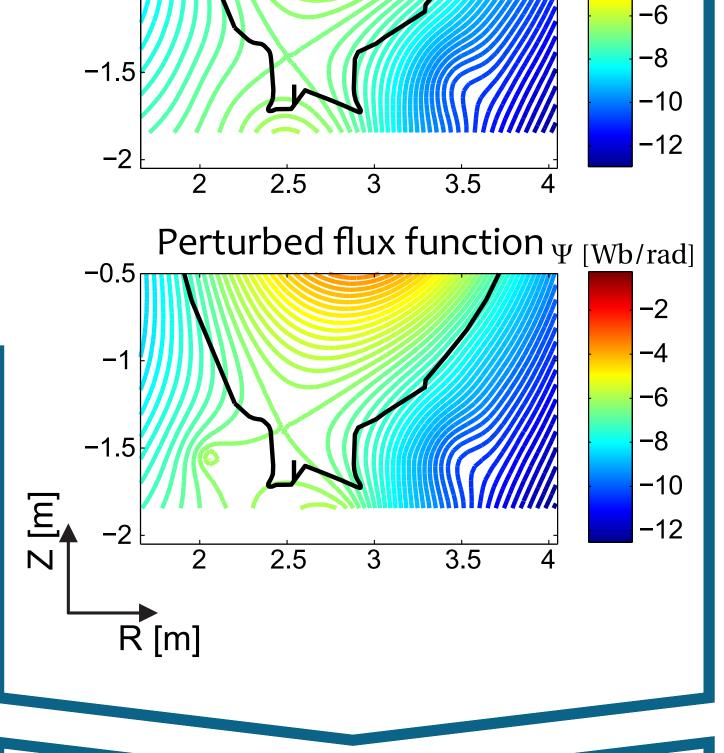




Use perturbation approach to avoid full MHD calculations Starting from $\Delta^* \Psi_0 + \Delta^* \delta \Psi = -\mu_0 R \left(J_{\phi,0} + \delta J_{\phi,int} + \delta J_{\phi,ext} \right)$ Original Perturbation • Calculate effect of additional conductors in vacuum $\Delta^* \delta \Psi = -\mu_0 R \left| \delta J_{\phi,int} + \delta J_{\phi,ext} \right|$



$$\Psi = \Psi_0 + \delta \Psi$$



Grid generation

Perturbation

Original flux function Ψ [Wb/rad]

Ψ [Wb/rad]

Next iteration

 $h(6) = R_x - R_{max,x} \le 0$

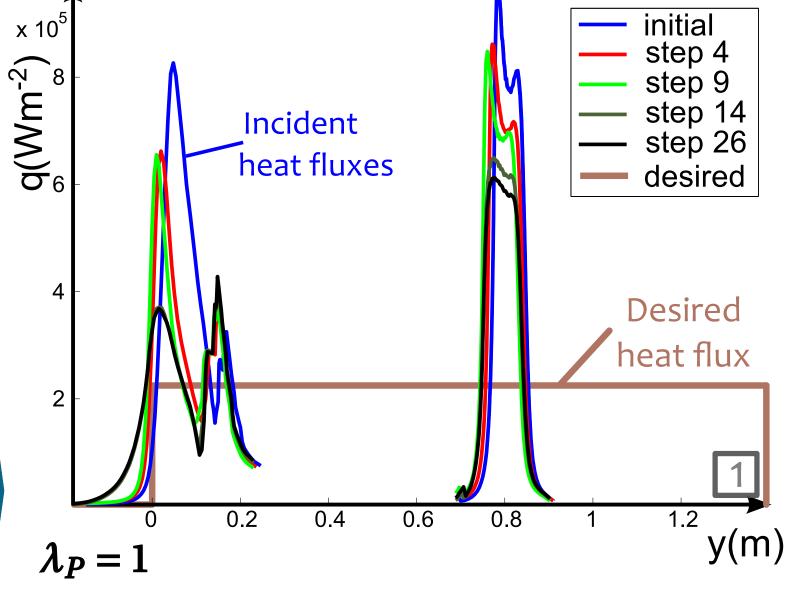
Optimization

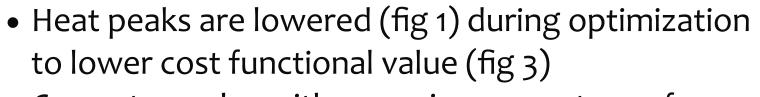
Solution through:

- **SQP** Optimization
- **FD** gradient computation
- Bracketing line search with Wolfe conditions
- Gradient projection optimization subproblem

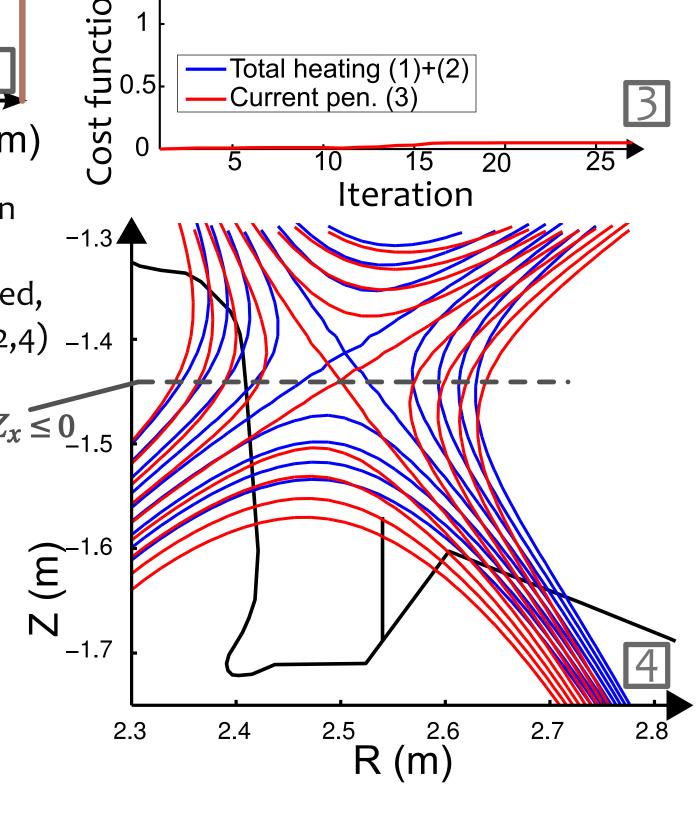
Cost functional

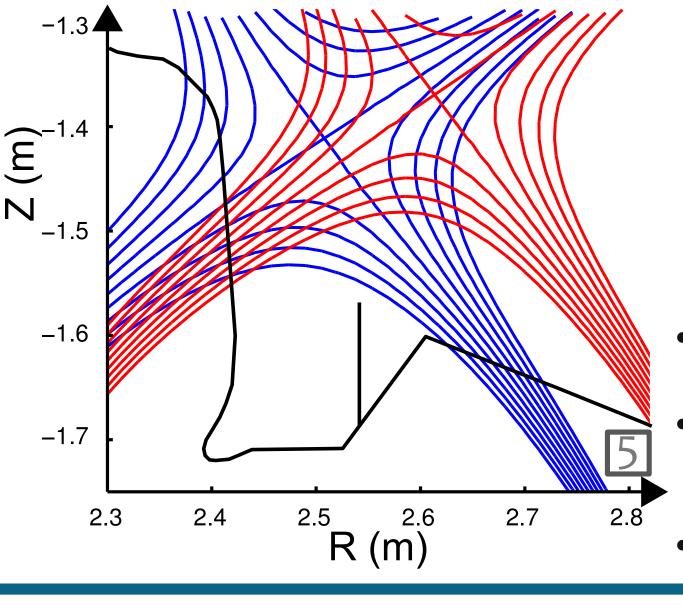
computation





- Current couples with opposing currents are formed, widening the flux tubes towards target area (fig 2,4) $^{-1.4}$
- The optimum is found to be at the boundary of the h(4) constraint (fig 4) $h(4) = Z_{min,x} - Z_x \le 0_{1.5}$

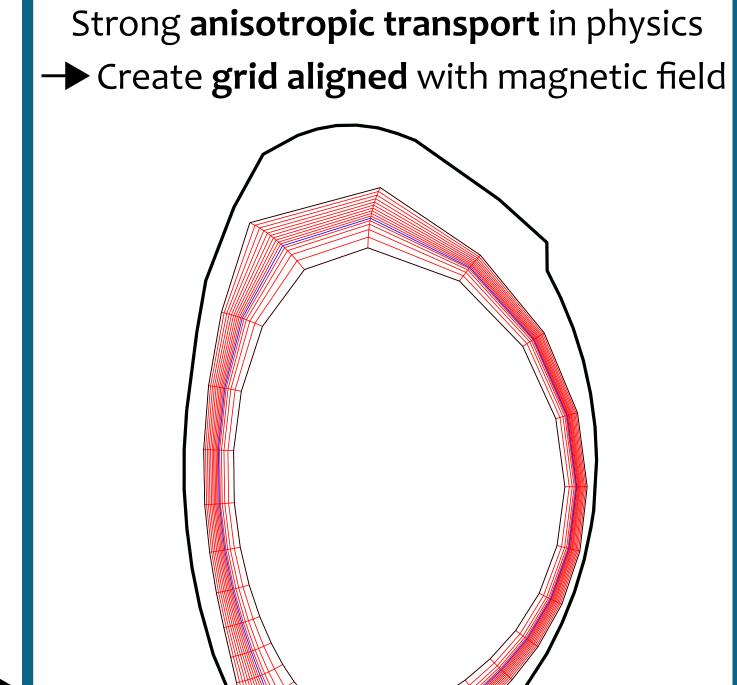


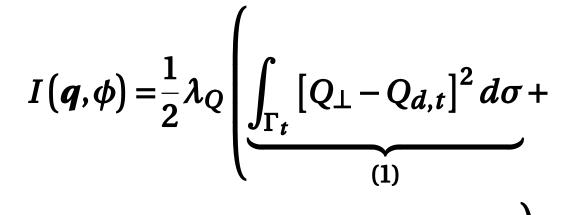




 \rightarrow

- The optimization pushes the separatrix towards the center of the target area to avoid high penalty (fig 5)
- This increases the heat peaks at the target but reduces the parallel heat flux outside the target area to zero.
- No active constraints, current penalty limits field shifting





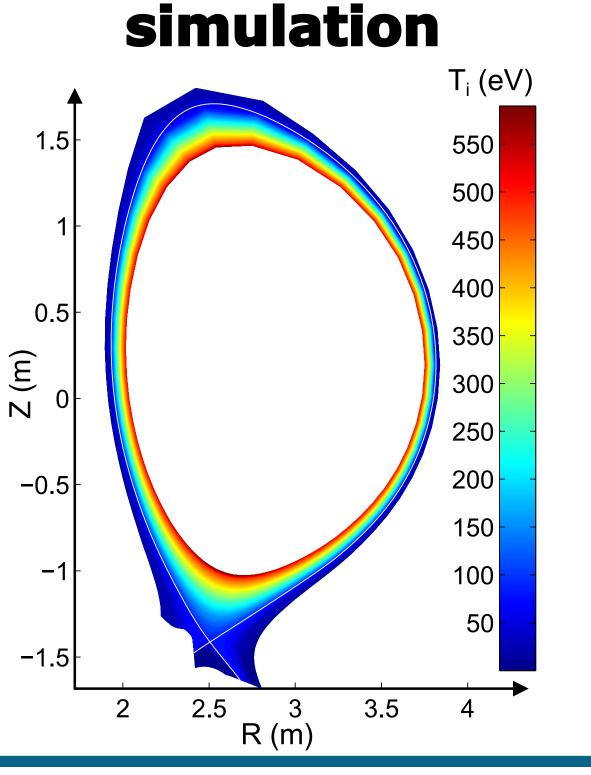
$$\underbrace{\int_{\Gamma_P} \left[\lambda_P \left(Q_{\perp} - Q_{d,p} \right) \right]^2 d\sigma}_{(2)} + \underbrace{\frac{1}{2} \lambda_{\phi} \sum_{i} \phi_i^2}_{(3)}$$

- (1) Maximal target heat load spreading
- (2) Wall heating penalty
- (3) Current penalty, regularization term

Solve **plasma edge** conservation equations

- **Ion continuity** equation
- Ion parallel momentum equation
- Internal **energy** equation
 - Sum of ion, electron and neutral internal energy equations
 - $T = T_i = T_e = T_n$
- Neutral continuity equation
- Pressure diffusion equation
- State variables: n_i, n_n, u_{//},T

Plasma flow



Conclusions

provided

target area

Incident

heat flux

Desired

heat flux

(1)

_y(m)

- Optimization framework with FD gradient calculation succesfully adjusts the magnetic field design to reduce the heat peak at the target area
- When increasing the relative importance of the heat flux outside the target area, the optimization avoids using all non-target material as desired
- Plasma edge simulation are computationally extremely expensive, even for this reduced model and limited set of control variables

Future work

- Use adjoint gradient calculation to allow for more control variables and reduce computational costs
- Extend magnetic model to allow larger changes to the magnetic configuration
- Incorporate more MHD-stability criteria, to account for unstable configurations in the optimization results

x 10⁵

 $q(Wm^{-2})$