

On the contact area and mean gap of rough, elastic contacts

Dimensional analysis, numerical corrections and reference data

Nikolay Prodanov · Wolf B. Dapp · Martin H. Müser

Received: date / Accepted: date

Abstract The description of elastic, nonadhesive contacts between solids with self-affine surface roughness seems to necessitate knowledge of a large number of parameters. However, few parameters suffice to determine many important interfacial properties as we show by combining dimensional analysis with numerical simulations. This insight is used to deduce the pressure dependence of the relative contact area and the mean interfacial separation $\Delta\bar{u}$ and to present the results in a compact form. Given a proper unit choice for pressure p , i.e., effective modulus E^* times the root-mean-square gradient $\bar{g}$, the relative contact area mainly depends on p but barely on the Hurst exponent H even at large p . When using the root-mean-square height $\bar{h}$ as unit of length, $\Delta\bar{u}$ additionally depends on the ratio of the height spectrum cutoffs at short and long wavelengths. In the fractal limit, where that ratio is zero, solely the roughness at short wavelengths is relevant for $\Delta\bar{u}$. This limit, however, should not be relevant for practical applications. Our work contains a brief summary of the employed numerical method Green's function molecular dynamics including an illustration of how to systematically overcome numerical shortcomings through appropriate finite-size, fractal, and discretization corrections. Additionally, we outline the derivation of Persson

theory in dimensionless units. Persson theory compares well to the numerical reference data.

Keywords Contact mechanics, Surface Roughness Analysis and Models

PACS 46.55.+d Tribology and mechanical contacts · 68.35.-p Solid surfaces and solid-solid interfaces: structure and energetics · 68.35.Gy Mechanical properties; surface strains

1 Introduction

Most solids have surfaces with self-affine roughness, which means that the height spectra of their undeformed surfaces scale with a power of the wave vector over several decades [33, 28, 18]. As a consequence of this roughness, solids tend to touch intimately only at a miniscule fraction of the apparent contact area [34]. Central quantities characterizing mechanical contact are the relative contact area a_r , the mean gap $\Delta\bar{u}$ between the solids, and the contact stiffness K , which is the derivative of $\Delta\bar{u}$ with respect to pressure [22, 24, 5]. Predicting either one of those descriptors for a given system — with well-defined height spectra and elastic properties — had not been possible until the beginning of the last decade. This changed when Persson proposed a scaling approach to contact mechanics and rubber friction [25]. The theory prompted the first numerical simulations which addressed systematically the contact mechanics of solids with self-affine rough surfaces [13].

Traditional approaches to contact mechanics neglect long-range elasticity [12, 6, 26]. This approximation is not only undesirable from a mathematical point of view, because it is uncontrolled, but also for practical reasons. Calculations neglecting long-range elasticity almost always lead to qualitatively wrong results [22, 26]. One

Nikolay Prodanov · Wolf B. Dapp · Martin H. Müser
Jülich Supercomputing Centre
Institute for Advanced Simulation
FZ Jülich, 52425 Jülich, Germany

Nikolay Prodanov · Martin H. Müser
Department of Materials Science and Engineering
Saarland University, Campus
66123 Saarbrücken, Germany
E-mail: martin.mueser@mx.uni-saarland.de

example is that traditional contact theories predict that the gap distribution remains Gaussian even under load when in fact it is exponential. As a consequence, traditional approaches to contacts grossly underestimate by how much additional load reduces the mean gap. This can easily lead to a several-decades overestimation of the leakage current through a mechanical interface at a given relative contact area even far away from the percolation transition [10].

In contrast, Persson theory has passed all comparisons to simulations so far, in the sense that the correct functional dependencies or constitutive laws follow from it, at least for relative contact areas of less than 50%. The coefficients of the constitutive laws tend to be within $\mathcal{O}(10\%)$ of those produced by high-quality simulations [24, 10, 4, 8, 35]. For example, it predicts the area-load dependence and gap distribution functions to within 15% accuracy between extremely small and 50% contact area [4, 8, 35].

The field of contact mechanics of randomly rough surfaces has much matured in the last ten years. Persson extended his theory to many interfacial problems, such as adhesion [15, 31, 19], plasticity [26, 2], contact stiffness [24, 9], leakage [32, 20, 29], squeeze-out [21], and the transition from elastohydrodynamic to boundary lubrication [30]. As far as numerics are concerned, various groups now have the expertise to simulate solids with surfaces containing several million grid points in the top layer, although considering billions of grid points per plane (as we did in the preparation of this work) still necessitates the use of supercomputers. Despite much progress, well-defined reference data is lacking and, moreover, estimates for the ratio of relative contact area and dimensionless load at small load have not yet converged [13, 8, 35, 38]. One of the reasons for the lack of such data is that no dimensional analysis has been conducted assessing which parameters are relevant and which quantities should be used to dimensionalize data. Such an analysis is useful to simplify the comparison between experiment, theory, and simulation.

In this work, we provide reference data for two interfacial properties: a_r and $\Delta\bar{u}$, including instructions on how to dimensionalize the data. Note that the contact stiffness K can subsequently be obtained from the mean gap, which is the reason why we do not consider K in the present work. One aim of our endeavor is to put experimentalists in a position to deduce reasonable approximations to, say, the mean gap as a function of pressure. At the same time, we wish to enable theoretically inclined practitioners to deduce some of the answers by themselves. For this purpose, we review Persson's contact mechanics theory (finding occasional shortcuts to some of the original calculations)

and also describe the Green's function molecular dynamics (GFMD) method [7, 16], which allows one to conduct simulations of planes with several million grid points on a standard single CPU core. This includes guidelines on how to systematically extrapolate the observable of interest to large system sizes (finite-size scaling), to large ratios of short- and long-wavelength cut-offs (fractal scaling), and to the continuum limit. Last but not least, we introduce a way to nondimensionalize the data with the goal to facilitate the comparison of data from different research groups.

The paper is organized as follows. In Section 2 we introduce the basic model assumptions and describe the means of characterizing the surface roughness. Section 3 presents the results of GFMD calculations for the scaling of relative contact area and mean gap with different corrections. Section 3 also contains the reference data. Section 4 summarizes the main findings. In the appendix, we briefly review Persson's theory as well as the GFMD technique.

2 Theory and method

2.1 Basic model assumptions

Throughout this work we make some basic assumptions and approximations. These are (i) linear elasticity of the solids, (ii) hard-wall repulsion between them, and (iii) the small-slope approximation. We make no additional (uncontrolled) approximations in our numerical solutions of the contact problem, unlike traditional contact mechanics approaches such as the Greenwood-Williamson theory [12, 26], one assumption of which are circular or elliptical shapes of contact patches (numerical simulations reveal that contact predominantly lives in fractal patches, which arise through the merging of many Hertzian contacts). We note that dropping any of our assumptions would make it impossible to present a complete set of reference data without making use of three-dimensional representations or tables. This means that plastic deformation and adhesion of the surfaces are not included in our model.

Nevertheless, our assumptions can be considered to be a good approximation for many applications. Plasticity only becomes relevant when the locally averaged stress in a contact exceeds a threshold, namely the hardness. At macroscopic scales, the stress is much smaller than the macroscopic hardness. When fine features of the height or the contact geometry are resolved, stresses become large, but so does the hardness, which is a scale-dependent quantity [23]. Persson theory allows one to estimate these effects and reveals that for many quantities plasticity will only induce small perturbations.

Likewise, direct adhesive interactions between solids are confined to those points where the two surfaces touch microscopically or are about to do so. Nevertheless, adhesion can become relevant (for soft solids) when capillaries are present. We point the reader to Refs. [31] and [19] for a more detailed discussion. In this work we assume, as already mentioned, hard-wall interactions, i.e., at no position at the interface may the z -coordinate of the top solid be smaller than that of the substrate. Formally, this nonholonomic boundary condition can be written as:

$$z_{\text{top}}(x, y) \geq z_{\text{bottom}}(x, y), \quad (1)$$

where $z_{\text{top}}(x, y)$ and $z_{\text{bottom}}(x, y)$ are the z -coordinates of the contacting surfaces for top and bottom solid, respectively, while x and y indicate in-plane coordinates. No forces act between the solids when they are not in contact and infinitely high repulsion occurs when they overlap.

The assumption of linear elasticity together with the small-slope approximation makes it possible to combine both roughness and compliance of the two solids into an effective roughness and an effective compliance [14]. These can then be assigned to either side of the interface. The effective local height then becomes $h(x, y) = z_{\text{top}}(x, y) - z_{\text{bottom}}(x, y)$ and the effective modulus reads

$$\frac{1}{E^*} = \frac{1 - \nu_1^2}{E_1} + \frac{1 - \nu_2^2}{E_2}, \quad (2)$$

where the E_i and ν_i denote the elastic moduli and the Poisson ratios of the two contacting solids.

The small-slope approximation permits neglecting the sideways motion of atoms, so that it suffices to consider scalar displacement fields. Put differently, by restricting ourselves to a scalar displacement field and by using the effective modulus E^* , we implicitly implement the small-slope approximation, even if the slopes for which we solve the contact mechanics problem are large.

2.2 Quantifying surface roughness

Let us define the effective height of the undeformed interface $h(x, y)$ as the gap between the surfaces when they touch in a single point, i.e., in the limit of a vanishingly small normal load $L = 0^+$. The values of $h(x, y)$ can be interpreted as a field of (spatially correlated) random numbers. The main assumption usually made for their stochastic properties is homogeneity across the surface, e.g., no wear tracks or systematic surface structuring. In addition, we will also assume isotropy, i.e., a

Peklenik number of one. As a consequence of homogeneity and isotropy any point is expected to yield the same average height for different realizations of the interface. Moreover, local gradients average to zero, although their magnitudes are finite. Lastly, the expected magnitude of the height change between two points (on a self-affine surfaces) increases as a power law of the distance between them. This can be expressed mathematically as:

$$\langle h(\mathbf{r}) \rangle = \bar{h}_0, \quad (3)$$

$$\langle h(\mathbf{r}) - h(\mathbf{r} + \Delta\mathbf{r}) \rangle = 0, \quad (4)$$

$$\langle \{h(\mathbf{r}) - h(\mathbf{r} + \Delta\mathbf{r})\}^2 \rangle \propto \Delta r^{2H}, \quad (5)$$

where $\mathbf{r}$ and $\Delta\mathbf{r}$ are vectors in the (x, y) plane. H is the Hurst roughness exponent [28], which also determines the fractal dimension of a surface, i.e., $D_f = 3 - H$.

In Fourier space, the stochastic properties of the surface roughness read:

$$\langle \tilde{h}(\mathbf{q}) \rangle = 0 \text{ for } q \neq 0, \quad (6)$$

$$\langle \tilde{h}^*(\mathbf{q}) \tilde{h}(\mathbf{q}') \rangle = \delta_{\mathbf{q}, \mathbf{q}'} C(\mathbf{q}), \quad (7)$$

where the surface height spectrum $C(\mathbf{q})$ exhibits the power law scaling

$$C(\mathbf{q}) = C(q_0) \left(\frac{q}{q_0} \right)^{-2-2H} \quad (8)$$

within a range $2\pi/\lambda_l < q < 2\pi/\lambda_s$, i.e., in between cutoffs at long and at short wavelengths, respectively. q_0 indicates an arbitrary reference wavenumber, which one can choose to coincide with $q_l = 2\pi/\lambda_l$. In Eq. (7), $\delta_{\mathbf{q}, \mathbf{q}'}$ represents the Kronecker symbol, which needs to be replaced with the $\delta(\mathbf{q} - \mathbf{q}')$ Dirac delta function for infinite systems in the continuum limit instead of discrete, periodically repeated systems.

For experimental systems [28] $0 \leq H \leq 1$. While it is formally possible to assume values outside this interval, we are not aware of any experiment finding such Hurst exponents, so we disregard that possibility here. The typical situation is that a surface power spectrum has a rolloff [28] at wave vector q_r so that $H = -1$ for $q < q_r$ is a reasonable approximation and $H = 0.85 \pm 0.05$ for $q > q_r$. From a computational point of view, a rolloff is as easily implemented as in a theoretical approach. We nevertheless disregard the rolloff here and instead focus on the contact mechanics for wavelengths shorter than the rolloff wavelength. Our motivation for this choice is that this makes a comparison between theory and simulation more transparent. Moreover, it is not possible to produce meaningful reference data when the limits $\lambda_r/\mathcal{L} \rightarrow 0$ and $\lambda_s/\lambda_r \rightarrow 0$ do not interchange, where $\mathcal{L}$ is the linear system size. When using a long wavelength

cutoff rather than a rolloff, the interchangeability of limits is much less problematic.

The stochastic properties of the surface — or an interface — are fully defined by the following variables: H , $\mathcal{L}$, λ_l , λ_s , $C(q_l)$, and, in the case of numerical calculations, a , which is the resolution of the lattice, i.e., the (smallest) grid spacing of the discrete elastic manifold. These six parameters can be replaced by the following set of parameters: H , $\bar{h}$, $\bar{g}$, $\mathcal{L}' = \mathcal{L}/\lambda_l$, $\lambda'_l = \lambda_l/\lambda_s$, and $\lambda'_s = \lambda_s/a$.

The RMS height $\bar{h}$ and RMS gradient $\bar{g}$ can be computed either in real space or in Fourier space. For a discrete set of heights we use the transform

$$h(\mathbf{r}) = \sum_{\mathbf{q}} \tilde{h}(\mathbf{q}) \exp[i\mathbf{q} \cdot \mathbf{r}] \quad (9)$$

$$\tilde{h}(\mathbf{q}) = \frac{1}{N} \sum_{\mathbf{r}} \tilde{h}(\mathbf{r}) \exp[-i\mathbf{q} \cdot \mathbf{r}], \quad (10)$$

where N is the number of points in the surface, and where $\mathbf{q}$ should be chosen in the image in which q is minimized. Thus,

$$\bar{h}^2 = \frac{1}{N} \sum_{\mathbf{q}} |\tilde{h}(\mathbf{q})|^2, \quad (11)$$

$$\bar{g}^2 = \frac{1}{N} \sum_{\mathbf{q}} q^2 |\tilde{h}(\mathbf{q})|^2, \quad (12)$$

for discrete systems. In order to connect to continuum theories, one needs to replace the discrete Fourier sums for finite, discrete and periodically repeated systems with Fourier integrals representing infinite and continuous systems. Going from the discrete to continuous representation in Fourier space implies that the thermodynamic limit $\mathcal{L} \rightarrow \infty$ is satisfied. Taking into account that nominal contact area $A_0 \rightarrow \infty$ when $\mathcal{L} \rightarrow \infty$, the following expression should be used:

$$\sum_{\mathbf{q}} \rightarrow \lim_{A_0 \rightarrow \infty} \frac{A_0}{(2\pi)^2} \int d^2 q. \quad (13)$$

Evaluating $\bar{h}$ and $\bar{g}$ for continuous systems analytically (for $0 < H < 1$), one can recognize that they are dominated by long and short wavelengths, respectively:

$$\bar{h}^2 = \frac{q_l^2 C(q_l)}{H} \left\{ 1 - (q_l/q_s)^{2H} \right\}, \quad (14)$$

$$\bar{g}^2 = \frac{q_s^4 C(q_s)}{2 - 2H} \left\{ 1 - (q_l/q_s)^{2-2H} \right\}, \quad (15)$$

because $\epsilon_f \equiv q_l/q_s$ disappears in the “fractal” limit (defined as $\epsilon_f \rightarrow 0$). Specifically, $\bar{h}_f = q_l \sqrt{C(q_l)/H}$ (for $H > 0$) depends only on the spectral features at q_l in the fractal limit, while $\bar{g}_f = q_s^2 \sqrt{C(q_s)/(2 - 2H)}$ (for $H < 1$) only depends on the spectral features near q_s .

Any observable $\mathcal{O}$ measured or computed for a given normal pressure p will be a function of many variables,

i.e.,

$$\mathcal{O} = \mathcal{O}(p, E^*, H, \bar{h}, \bar{g}, 1/\mathcal{L}', 1/\lambda'_l, 1/\lambda'_s). \quad (16)$$

However, in most cases of practical interest, one should be close to the following two limits: (i) the thermodynamic limit $1/\mathcal{L}' \rightarrow 0$ and (ii) the fractal limit $1/\lambda'_l \equiv \lambda_s/\lambda_l \rightarrow 0$. Moreover, when comparing to continuum theories, one should reduce discretization effects, which leads to (iii) the continuum limit $1/\lambda'_s \rightarrow 0$. In most cases, one should therefore be interested only in the dependence of a quantity on three surface-topography-related variables, namely H , $\bar{h}$, and $\bar{g}$. Since we are still free to choose the unit of length, H and $\bar{g}$ are the only dimensionless parameters that can matter in the thermodynamic/fractal/continuum (TFC) limit.

In consequence, the mean gap in a self-affine fractal interface in the TFC limit can only depend on three variables, i.e.,

$$\Delta \bar{u} = \bar{h} \cdot \Delta u_{\text{dl}}(p/E^*, H, \bar{g}), \quad (17)$$

where Δu_{dl} is the dimensionless mean gap, which can only depend on dimensionless numbers. Any other dependence is not possible, because $\Delta \bar{u}$ must have the dimension of length. Of course, Eq. (17) is only meaningful under the assumption that the TFC limit exists and is unique, i.e., that it does not matter in what order the limits $1/\mathcal{L}' \rightarrow 0$ and $1/\lambda'_l \rightarrow 0$ are taken.

Given the above analysis, one can conclude that not only the gap but *any* quantity can depend in a nontrivial fashion on at most two surface topography-related, dimensionless parameters, namely H and $\bar{g}$. This constitutes a dramatic reduction of complexity as compared to the initial set of six topography-defining variables. As a caveat we note that it is nevertheless possible that $\Delta u_{\text{dl}} = 0$. In that case, the leading order is a correction $\propto \epsilon_f$.

2.3 Dimensional analysis of the elasticity of half spaces

In three-dimensional space, the elastic energy density U_{el}/V is a bilinear function of the strain $(\partial u_\alpha / \partial R_\beta + \partial u_\beta / \partial R_\alpha)/2$ in the harmonic approximation. Here, $u_\alpha(\mathbf{R})$ is the displacement field, and it is proportional to the elements of the elastic tensor $C_{\alpha\beta\gamma\delta}$ [17]. For a homogeneous medium this implies that the energy density is bilinear in the wave vector if the energy is calculated in Fourier space. The elasticity of a half-space must still be harmonic in the displacements (which are now only defined on the surface) and it will still be proportional to the elements of the elastic tensor. However, the energy density is no longer normalized to a volume element but to a surface element. Since the areal energy density

must still be harmonic and thus quadratic in the displacements, the prefactor can only be proportional to the wave vector. This means that $U \propto qE^*|\tilde{u}(\mathbf{q})|^2$ is the only possible dependence. Fixing the prefactor requires lengthy calculations [31], the result of which is

$$U_{\text{el}}/A_0 = \frac{E^*}{4} \sum_{\mathbf{q}} q |\tilde{u}(\mathbf{q})|^2, \quad (18)$$

where A_0 is the nominal surface area of the solid experiencing an external force. In Eq. (18), we have restricted the displacement to be normal to the surface, which is justified in the small-slope approximation as long as forces are normal, too.

From Eq. (18) the elastic force onto the surface layer can be derived. In static equilibrium, it must be balanced by some external pressure. This leads to the following equilibrium condition:

$$\frac{E^*}{2} q \tilde{u}(\mathbf{q}) + \tilde{p}_{\text{if}}(\mathbf{q}) + \tilde{p}_{\text{ext}}(\mathbf{q}) = 0, \quad (19)$$

where $\tilde{p}_{\text{if}}(\mathbf{q})$ is the interfacial force, e.g., the Fourier transform of the pressure that the top solid exerts on the bottom solid, and $\tilde{p}_{\text{ext}}(\mathbf{q})$ is an externally exerted pressure. For a constant external pressure, i.e., $\tilde{p}_{\text{ext}}(\mathbf{q}) = p_0 \delta_{0,\mathbf{q}}$ the equilibrium condition can be written as:

$$\tilde{p}_{\text{if}}(\mathbf{q}) = \begin{cases} -p_0 & \text{if } \mathbf{q} = 0, \\ -\frac{E^*}{2} q \tilde{u}(\mathbf{q}) & \text{else.} \end{cases} \quad (20)$$

Let $\tilde{u}_{\text{old}}(\mathbf{q})$ be a solution for a given height profile $h(\mathbf{r})$. One can then construct a new solution for a system in which all in-plane coordinates are scaled according to $(x, y)_{\text{new}} = s \cdot (x, y)_{\text{old}}$, which implies $\mathbf{q}_{\text{new}} = \mathbf{q}_{\text{old}}/s$:

$$\frac{E^*}{2} (s \cdot \mathbf{q}_{\text{new}}) \tilde{u}_{\text{old}}(s \cdot \mathbf{q}_{\text{new}}) = -\tilde{p}_{\text{if,old}}(s \cdot \mathbf{q}_{\text{new}}). \quad (21)$$

This equation can be reexpressed as

$$\frac{E^*}{2} \mathbf{q}_{\text{new}} \tilde{u}_{\text{new}}(\mathbf{q}_{\text{new}}) = -\tilde{p}_{\text{if,new}}(\mathbf{q}_{\text{new}}) \quad (22)$$

with

$$\tilde{p}_{\text{if,new}}(\mathbf{q}_{\text{new}}) = \frac{1}{s} \cdot \tilde{p}_{\text{if,old}}(\mathbf{q}_{\text{new}}/s). \quad (23)$$

Thus, all interfacial forces scale with $1/s$, which then must also hold for the external pressure.

Our scaling transformation leaves $\bar{h}$ invariant and only changes $\bar{g}$ to $\bar{g}/s$. However, by renormalizing p to p/s , we get back our old solution. Therefore, $p/E^*\bar{g}$ is the only variable which the mean separation can depend on. This simplifies Eq. (17) to

$$\Delta \bar{u} = \bar{h} \cdot \Delta u_{\text{dl}}(p/E^*\bar{g}, H). \quad (24)$$

For other observables, similar relationships can be found, where the prefactor is a product of a power of $\bar{h}$ and the elastic constant E^* , and the relevant dimensionless parameters are $p/E^*\bar{g}$ and H .

In some cases, one might find that $\Delta u_{\text{dl}} = 0$. This, however, does not imply that $\Delta \bar{u}$ is zero when expressed as a multiple of a *microscopic* length. It can still be finite, but since $\bar{h}$ can have diverged in the fractal limit, the ratio $\Delta \bar{u}/\bar{h}$ has become zero. In that case, it can be more appropriate to nondimensionalize the gap — or other quantities of unit length — by a microscopic or mesoscopic length. One possibility to achieve this is the use of the following alternative dimensionless expression for the mean gap Δu_{adl} via

$$\Delta \bar{u} = (\bar{g}\lambda_s) \cdot \Delta u_{\text{adl}}(p/E^*\bar{g}, H). \quad (25)$$

This is shown in Fig. 7 below. Using Eqs. (8), (11), (12), the leading-order term of $\lambda_s(\epsilon_f)$ can be written as

$$\bar{g}\lambda_s = 2\pi\bar{h} \begin{cases} 1/\sqrt{-2\ln\epsilon_f} & H = 0, \\ \sqrt{H/(1-H)}\epsilon_f^H & 0 < H < 1, \\ \epsilon_f\sqrt{-2\ln\epsilon_f} & H = 1, \end{cases} \quad (26)$$

with $\epsilon_f = \lambda_s/\lambda_l < 1$.

3 Results

3.1 Continuum, fractal, and finite size corrections

3.1.1 Contact area

Any contact mechanics simulation is conducted at a finite system size $\mathcal{L}$ rather than in the thermodynamic limit. The ratio λ_l/λ_s is also finite and the roughness at the smallest wavelength is discretized only down to a finite ratio a/λ_s . In this section we investigate to what extent one can express a dimensionless observable $\mathcal{O}_{\text{d}}^{\text{sim}}$ computed at finite values of $\epsilon_t = \lambda_l/\mathcal{L}$, $\epsilon_f = \lambda_s/\lambda_l$, and $\epsilon_c = a/\lambda_s$ through

$$\mathcal{O}_{\text{d}}^{\text{sim}}(p/E^*\bar{g}, H, \epsilon_t, \epsilon_f, \epsilon_c) = \mathcal{O}_{\text{d}}^{\text{TFC}}(p/E^*\bar{g}, H) + C_t\epsilon_t^{\alpha_t} + C_f\epsilon_f^{\alpha_f} + C_c\epsilon_c^{\alpha_c} \quad (27)$$

and extrapolate to the TFC limit by computing the observable of interest at finite values of ϵ_t , ϵ_f , and ϵ_c . Both the exponents α_i and also the proportionality constants C_i can be functions of H and $p/E^*\bar{g}$, though one would expect the exponents to depend only weakly on the pressure.

Note that any of the three corrections *can be significant* and it is not *a priori* clear which correction is important for a given combination of H and $p/E^*\bar{g}$. Therefore, it is important to systematically control the

values of the parameters independently of each other, i.e., by only changing one ϵ_i at a time. This point is taken into account in our calculations in the following way: we choose a reference system, namely, $\mathcal{L}/\lambda_l = 2$, $\lambda_l/\lambda_s = 1024$, $\lambda_s/a = 2$, and run simulations by varying each value of ϵ_i while keeping the other two constant. To estimate stochastic error bars, we perform calculations with up to four different realizations of the randomly rough surfaces.

All the calculations have been carried out using the GFMD technique described in Appendix B and implemented in our in-house parallel code. Note that to get reliable extrapolated results in one of the limits, it is necessary to approach the limit as closely as possible. This requires considering quite large system sizes $\mathcal{L}$. The typical “close to a limit” system size in the present study is $\mathcal{L} = 2^{15}$ which corresponds to about 1 billion grid points in the 2D contact plane. The largest linear size presented here is $\mathcal{L} = 2^{17}$ (about 17 billion grid points in the contact plane) which we used to ascertain the scaling of the mean gap with ϵ_f (see Fig. 6 below).

We start our analysis with the continuum corrections to the contact area, which historically were the first ones to come under scrutiny. Hyun and Robbins [13] evaluated contact area using $\epsilon_c = 1/2$ arguing that roughness extends down to the smallest scale. This argument is valid if one is interested in determining the contact area of real systems, although a rigorous definition of contact may only be possible in the realm of continuum mechanics. We therefore feel that the limit $\epsilon_c \rightarrow 0$ is more appropriate for our purpose, all the more when testing the validity of a solution in continuum mechanics. To this date, no consensus has been reached to the precise value of the dimensionless ratio $\kappa \equiv a_t \bar{g} E^* / p$ for small p . Recent numerical estimates range from $\kappa = 2$ ($\epsilon_c = 1/32$, $\epsilon_f = 1/64$, $\epsilon_t = 1$) in Ref. [35] to values exceeding 2.5 (e.g., $\epsilon_c = 1/16$, $\epsilon_f = 1/8$, $\epsilon_t = 1/16$) in Ref. [38], while Persson theory predicts that $\kappa = \sqrt{8/\pi} \approx 1.6$.

In Fig. 1 we show how the proportionality coefficient κ depends on ϵ_c for fixed values of $\epsilon_f = 1/1024$ and $\epsilon_t = 1/2$. Here, κ is defined as

$$\kappa = \frac{A}{A_0 p^*}, \quad (28)$$

where A and A_0 are real and apparent contact area, respectively, and $p^* = p/E^* \bar{g}$. We find that the ϵ_c correction follows a power law with the exponent $\alpha_c \approx 0.67$ at small loads. This is in agreement with the work by Campañá and Müser [8] who found the same exponent, although their work was not yet based on the continuum Green’s functions but rather on the Green’s functions describing a *discrete* elastic manifold. Other differences

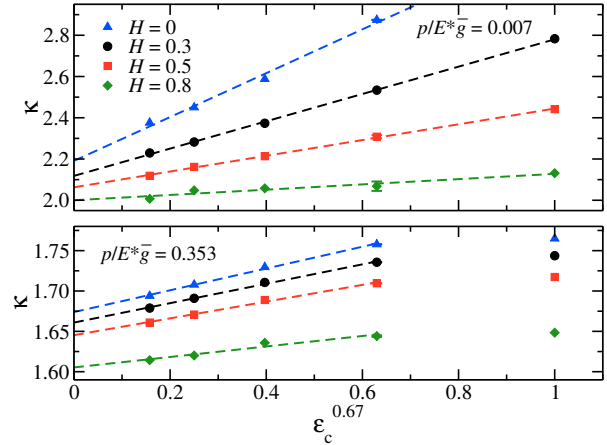


Fig. 1 Proportionality coefficient κ as a function of the discretization ϵ_c for fixed values $\epsilon_t = 1/2$ and $\epsilon_f = 1/1024$. One set of curves is evaluated at a low pressure $p^* = p/E^* \bar{g} = 0.007$ (top panel), while another one is evaluated at $p^* = 0.353$ (bottom panel).

are that Campañá and Müser [8] did not keep ϵ_f constant and used $\epsilon_t = 1$. Despite these distinctions, we confirm that κ in the continuum limit is indeed close to 2 and that it increases marginally as H decreases. This is also consistent with Putignano *et al.* who found virtually no dependence on H for values of H close to unity [35,36], and also with Persson theory in which κ is independent of H .

While previous work focused on the low-load limit, we extend the analysis of discretization corrections to larger pressures, where the $A \propto p$ is no longer accurate. In this regime κ falls below the value of 2. The contact area over pressure still appears to converge with $\epsilon_c^{0.67}$. The corrections are smaller, and convergence starts at smaller values of ϵ_f than at lower pressures. It is interesting to note that the relative contact area still seems to be rather independent of H . At the given values of ϵ_f and ϵ_t , its value ranges from 0.837 for $H = 0.8$ to 0.802 for $H = 0$ at $p^* = 0.353$.

Figure 2 depicts the influence of the fractal correction ϵ_f on κ for two pressures at the default reference values of ϵ_c and ϵ_t . For both pressures, we find an exponent of $\alpha_f \approx 0.67$. One can see that larger values of ϵ_f can lead to substantial errors in particular at small pressures and Hurst exponents close to 1. For example, on the $p^* = 0.007$ curve for $H = 0.8$ the error initially increases with $\approx 3\epsilon_f^{0.67}$ so that to a zeroth-order approximation, κ may be overestimated by as much as $\mathcal{O}(30\%)$ if $\lambda_l/\lambda_s = 32$ is chosen. This might explain why recent work by Yastrebov *et al.* [38], who focused on continuum corrections, found particularly large values for κ in contrast to studies [8,35] employing smaller values of ϵ_f . The problem appears to be that if one keeps λ_l/a constant but varies λ_s , it might remain unnoticed that

the error is converted from a continuum correction to a fractal correction, all the more as both corrections are positive and each scales only sublinearly with ϵ .

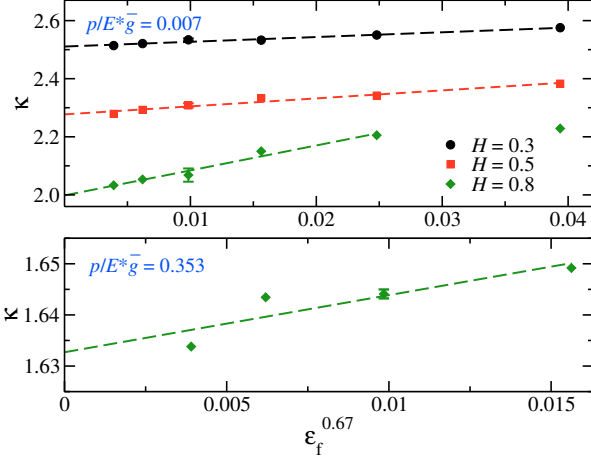


Fig. 2 Proportionality coefficient κ as a function of the fractal correction $\epsilon_f = \lambda_s/\lambda_l$ for fixed values $\epsilon_c = 1/2$ and $\epsilon_t = 1/2$. One set of curves is obtained at a low pressure $p^* = p/E^*\bar{g} = 0.007$, while another one is evaluated at $p^* = 0.353$. At higher pressure only one set of data ($H = 0.8$) is shown to emphasize a small value of the fractal correction. For other values of H the effect of ϵ_f is even smaller.

It may also be interesting to note that Yastrebov *et al.* [38] found values for κ close to the predictions based on the Bush-Gibson-Thomas (BGT) theory [26], which is an asperity-based model neglecting that individual contact patches can merge to form fractal shaped contact patches. This suggests that systems with small values of ϵ_f do not always behave like self-affine randomly rough surfaces but more like the collection of (elastically uncoupled) bumps.

For larger values of p^* we again find small prefactors for the corrections to κ . Within the stochastic scatter, leading-order corrections are consistent with an $\mathcal{O}(\epsilon_f^{0.67})$ dependence. However, prefactors are small. In the case of $H = 0.3$ the fractal corrections are even below our (statistical) detection capabilities. Despite the small prefactors, it seems as if convergence starts at smaller values of ϵ_f than for smaller pressures.

In the study of TFC corrections to the contact area, we also investigate how the thermodynamic limit is approached. Figure 3 reveals that the dependence of κ on ϵ_t is rather weak. In fact, corrections are so small that we cannot determine with certainty the exponent α_t . The fluctuations in κ are of order 1% and 0.1% for $p^* = 0.007$ and $p^* = 0.353$, respectively.

With regards to finding the TFC limit for the contact area, we summarize that continuum and fractal corrections are quite substantial, while those related to

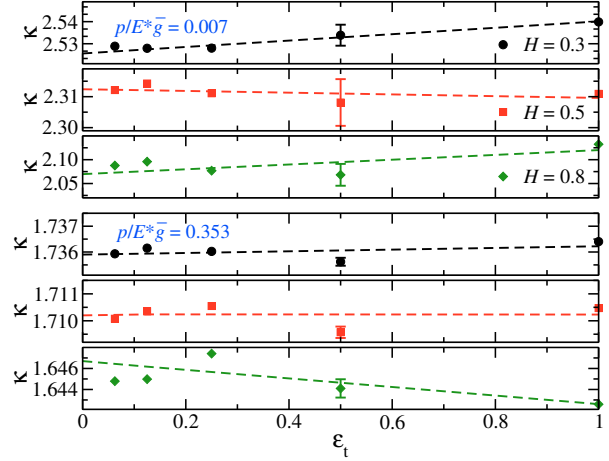


Fig. 3 Dimensionless ratio κ as a function of the thermodynamic correction ϵ_t for fixed values $\epsilon_c = 1/2$ and $\epsilon_f = 1/1024$. Dotted lines indicate linear fits. κ is nearly independent of the thermodynamic correction.

the thermodynamic limit are minor. The FC corrections have a larger prefactor at smaller pressures; however, the asymptotic convergence to the limits starts at larger values of ϵ_c and ϵ_f than at higher pressures. As expected, fine discretizations (small ϵ_c) are required for small values of H , where roughness lives more strongly on short wavelengths than at large values of H . Conversely, one must ensure relatively small values of ϵ_f for large H .

From the GFMD results we obtained Tables 1 and 2 containing coefficients and powers to be used in Eq. (27). This information allows extrapolating κ to the TFC limit. As a specific example, to extrapolate κ^{sim} at $p^* = 0.007$ and $H = 0.8$, one can add the computed corrections according to Eq. (27) for the values of ϵ_t , ϵ_f and ϵ_c used in the simulations:

$$\kappa^{\text{TFC}}(p^* = 0.007, H = 0.8) \approx \kappa^{\text{sim}}(p^*, H, \epsilon_t, \epsilon_f, \epsilon_c) - 0.0421\epsilon_t - 8.5879\epsilon_f^{0.67} - 0.1279\epsilon_c^{0.67}. \quad (29)$$

H	C_c	C_f	C_t	α_c	α_f	α_t
0.3	0.6621	1.6322	0.0132	0.67	0.67	1
0.5	0.3817	2.7518	-0.0028	0.67	0.67	1
0.8	0.1279	8.5879	0.0421	0.67	0.67	1

Table 1 Coefficients and powers in Eq. (27) for κ at $p^* = 0.007$ obtained from the GFMD results.

Unfortunately, it is difficult to predict for what range of pressures the data for $p^* = 0.007$ can be used without considerable loss of accuracy. Although a_r is linear in p^* at low p^* ($\lesssim 10^{-1}$), one averages over a different distribution of contact patches when decreasing p^* , e.g., the largest contact patch shrinks with decreasing p^* ,

H	C_c	C_f	C_t	α_c	α_f	α_t
0.3	0.1202	0.0535	$3.1658 \cdot 10^{-4}$	0.67	0.67	1
0.5	0.1037	0.0796	$8.4447 \cdot 10^{-5}$	0.67	0.67	1
0.8	0.0650	1.1145	$-3.1623 \cdot 10^{-3}$	0.67	0.67	1

Table 2 Coefficients and powers in Eq. (27) for κ at $p^* = 0.353$ obtained from the GFMD results.

and the relative importance of small contact patches increases. Thus, our tables only convey trends as to which corrections become important for different H in the high- or low-pressure regime.

Despite potentially large corrections, well-chosen parameters allow one to produce quite meaningful results, even without extrapolation. For example, for $H = 0.8$ and $p^* = 0.007$ if one chooses $a/\lambda_s = 1/2$, $\lambda_s/\lambda_l = 1/1024$, and $\lambda_l/\mathcal{L} = 1$, the expected error in κ is only 6% (for a system size of 2048). However, to keep the error for a system with $H = 0.3$ similarly small, it is better to use $a/\lambda_s = 1/16$ and $\lambda_s/\lambda_l = 1/256$. A system of total size 2048×2048 can be easily handled on a single CPU core, and convergence with a well-tuned GFMD code is reached within less than an hour of computing time on modern hardware.

3.1.2 Mean gap

Unlike the contact area, the TFC analysis of the mean gap $\Delta\bar{u}$ has not attracted much attention in the literature. Therefore, there are not many references for the $\Delta\bar{u}$ to compare with (in contrast to a_r or κ for which there exist computational results from several research groups). Additionally, the TFC analysis for the mean gap is more challenging than that for a_r . As was mentioned in Section 2.3 and as will be clear from the GFMD results, the choice of the unit for the length scale considerably influences the value of $\Delta\bar{u}$ in the fractal limit. However, when the continuum and thermodynamic corrections are considered, the question about the unit of length is not very important and we use the RMS height $\bar{h}$ for normalization in these cases. Note that we also compare the GFMD results with Persson theory, which can predict scaling of the $\Delta\bar{u}$ with the fractal correction (see the Appendix A for more information on Persson theory). For other two corrections such a comparison is not possible as the theory assumes that the continuum and thermodynamic limits are satisfied.

As before, the continuum limit is examined first. From Fig. 4 one can see that the discretization corrections are largest for the smallest values of H . At high pressures the corrections follow a linear law. At the lower pressure, numerical noise does not allow one to establish a scaling law. Nevertheless, the linear fits

can again be used with high accuracy. Prefactors can be large; for $p^* = 0.353$ and $H = 0$, the gap is almost three times larger for $\epsilon_c = 1/2$ (which is the reference value) than in the (extrapolated) limit of $\epsilon_c = 0$. In contrast, the corrections for $H = 0.8$ are relatively moderate, e.g., they only amount to roughly 20% of the observable at $\epsilon_c = 1/2$. For this larger value of H , we are plagued with large stochastic error at small p , which is readily seen from the top panel of Fig. 4.

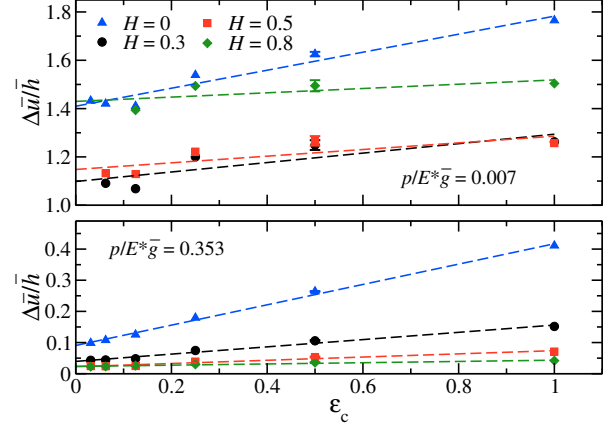


Fig. 4 Dimensionless gap in units of the RMS height as a function of the discretization ϵ_c for fixed $\epsilon_t = 1/2$ and $\epsilon_f = 1/1024$. One set of curves is evaluated at a low pressure $p^* = p/E^*\bar{g} = 0.007$ (top panel), while another one is evaluated at $p^* = 0.353$ (bottom panel). Dashed lines indicate least-squares linear fits.

Thermodynamic corrections show similar trends as continuum corrections, as one can see in Fig. 5. Specifically, we find that $\Delta\bar{u}$ varies linearly in ϵ_t . The numerical scatter is again particularly large for low p and larger H .

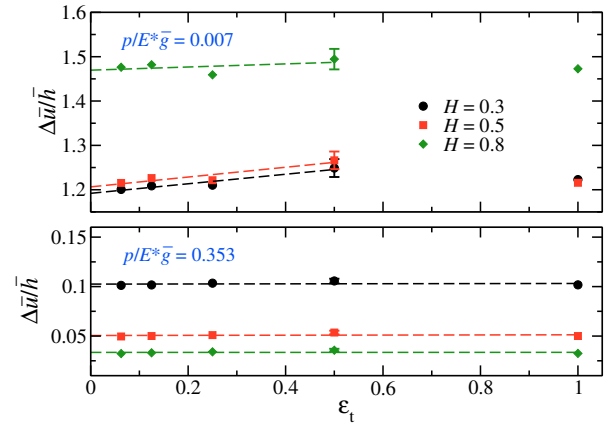


Fig. 5 Dimensionless gap in units of the RMS height as a function of the thermodynamic correction ϵ_t for fixed values $\epsilon_c = 1/2$ and $\epsilon_f = 1/1024$. Dashed lines indicate least-squares linear fits.

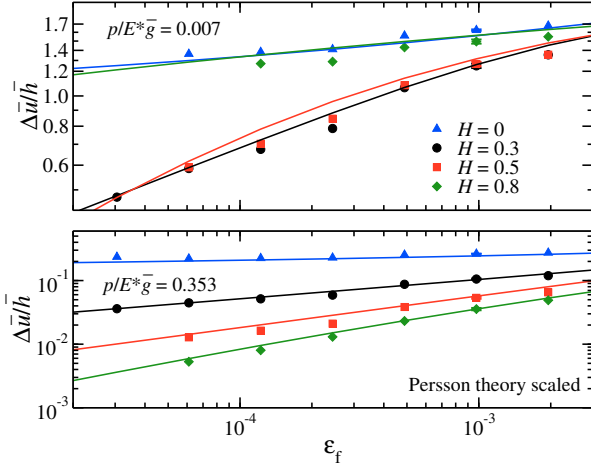


Fig. 6 Dimensionless gap in units of the RMS height as a function of the fractal correction $\epsilon_f = \lambda_s/\lambda_l$ for fixed values $\epsilon_c = 1/2$ and $\epsilon_t = 1/2$. One set of curves is evaluated at a low pressure $p^* = p/E^*\bar{g} = 0.007$ (top panel), while another one is evaluated at $p^* = 0.353$ (bottom panel). Dots show GFMD results, lines are obtained using Persson theory. To match with the simulations within 10% at the higher pressure theory results are scaled by factors of 3 and 2 for $H = \{0, 0.3, 0.5\}$ and $H = 0.8$, respectively. No scaling is required at the lower pressure.

Fractal corrections obtained with GFMD and Persson theory are shown in Figs. 6, 7 and 8. At the lower pressure, theory and simulations fit within about 10% accuracy. Although the theory gives correct functional dependencies at the higher pressure, the prefactors are about 2–3 times smaller than in the simulations (see captions of Figs. 6, 7 for the exact values of the scaling factors). Independent of the normalization, there exists a region where the mean gap varies with ϵ_f approximately according to a power law with pressure-dependent exponents. When normalizing with the RMS height $\bar{h}$, the exponents at $p^* = 0.007$ are $\alpha_f = \{0.067, 0.26, 0.25, 0.079\}$ for $H = \{0, 0.3, 0.5, 0.8\}$ respectively. At $p^* = 0.353$ the exponents are $\alpha_f = \{0.048, 0.30, 0.51, 0.67\}$ for $H = \{0, 0.3, 0.5, 0.8\}$ respectively. Using $\bar{g}\lambda_s$ as the normalization factor leads to the increase of the mean gap with ϵ_f according to power laws with almost zero exponents for $H = \{0, 0.3\}$ both at higher and lower pressures. The exponents for the cases of $H = \{0.5, 0.8\}$ are $\alpha_f = \{0.25, 0.75\}$ at $p^* = 0.007$ and $\alpha_f = \{0.002, 0.14\}$ at $p^* = 0.353$. These results imply that the mean gap in the fractal limit is zero in units of $\bar{h}$ at relatively small pressures, although the gap measured in microscopic units such as λ_s must be greater than zero as long as contact is not complete.

From Figs. 6–8 one can learn that extrapolating to the fractal limit is far from trivial. One reason is that when $\epsilon_f \rightarrow 0$, $\Delta\bar{u}$ expressed in units of $\bar{h}$ does not show a clear plateau, while for $\bar{g}\lambda_s$ extremely small values of

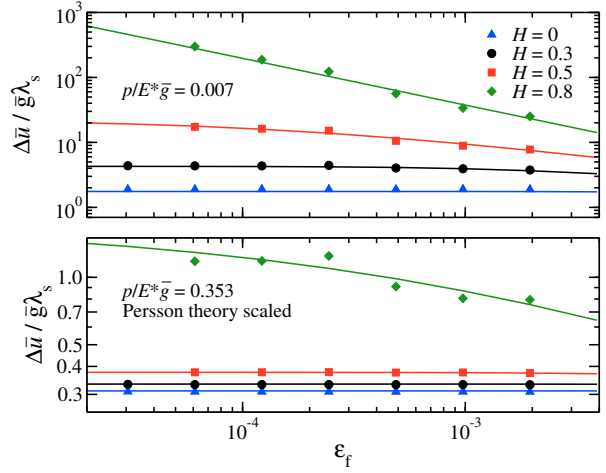


Fig. 7 Dimensionless gap in units of $\bar{g}\lambda_s$ as a function of the fractal correction $\epsilon_f = \lambda_s/\lambda_l$ for fixed values $\epsilon_c = 1/2$ and $\epsilon_t = 1/2$. The focus is on the larger values of ϵ_f captured by the GFMD. Dots show GFMD results, lines are obtained using Persson theory. To match with the simulations within 10% at the higher pressure theory results are scaled by factors of $\{3.3, 3.1, 2.75, 2\}$ for $H = \{0, 0.3, 0.5, 0.8\}$, respectively. No scaling is required at the lower pressure.

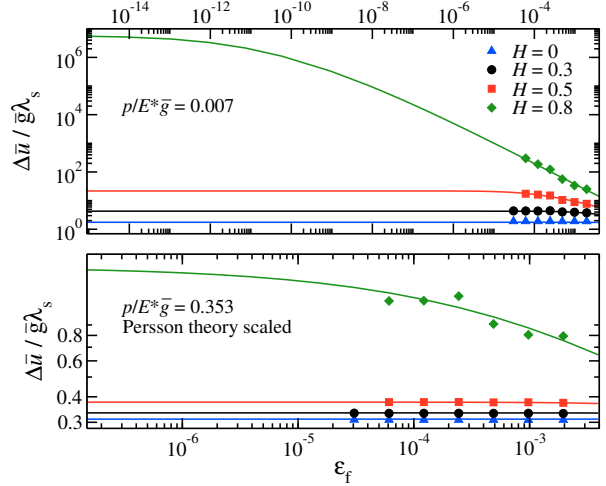


Fig. 8 Dimensionless gap in units of $\bar{g}\lambda_s$ as a function of the fractal correction $\epsilon_f = \lambda_s/\lambda_l$ for fixed values $\epsilon_c = 1/2$ and $\epsilon_t = 1/2$. Values of ϵ_f span almost 15 decades. According to the theory, the mean gap eventually converges in the fractal limit. Designations and scaling are the same as in Fig. 7.

ϵ_f are required in order to see the convergence. Having only smaller (though practically relevant) values of ϵ_f may lead to the incorrect conclusion that $\Delta\bar{u}/(\bar{g}\lambda_s)$ diverges according to a power law. In fact, even though we are using systems sizes up to $\mathcal{L} = 2^{17}$ spanning 5 orders of magnitude in length, we are still in the “large ϵ_f regime” where we only see the power law divergence (Fig. 7). Nevertheless, the theory predictions — that agree well with the simulations at larger ϵ_f — clearly indicate the eventual convergence of $\Delta\bar{u}/(\bar{g}\lambda_s)$ to the fractal limit (Fig. 8). These observations may also sug-

gest that for the mean gap, ϵ_f should be considered as an additional independent variable and not as a correction, in contrast to the situation for relative contact area.

Let us discuss in more detail the implications of finding either (i) a finite value of $\Delta\bar{u}/\bar{h}$ or (ii) a finite value of $\Delta\bar{u}/\bar{g}\lambda_s$. Observation (i) goes hand in hand with having only one or very few mesoscale asperity contacts per area of size λ_1^2 . Those contacts are found in the vicinity of the highest peak on a domain of size λ_1^2 . If contact is distributed more or less homogeneously throughout the apparent contact area, gaps must automatically disappear when expressed in units of $\bar{h}$. In this case, i.e., for pressures so small that contact occurs only near the highest asperity, the original Persson theory presented in this work is inappropriate and finite-size corrections need to be applied [24].

Observation (ii) implies contacts that start to look homogeneous when spatial features on length scales only slightly larger than λ_s are resolved. In fact, given Eq. (15), one could argue that the root-mean-square height due to the roughness on the shortest wavelengths is of order $\sqrt{2-2H}\bar{g}\lambda_s$. Then, the gaps for large pressures ($p^* = 0.353$ and $H = \{0, 0.3, 0.5\}$ in Fig. 7) are of order of (but smaller than) the root-mean-square height associated with short wavelengths. Thus, non-trivial scaling of the gap with ϵ_f can occur when the contacts start to look heterogeneous at wavelengths much less than λ_1 but distinctly more than λ_s .

We conclude this section by identifying reasonable reference systems for the evaluation of the mean gap. For the $H = 0.8$, $p^* = 0.007$ system, discretization corrections appear to be rather minor. Choosing a/λ_s as large as $1/2$ does not seem to introduce artifacts. Finite-size corrections also do not lead to considerable errors. Choosing $\lambda_1/\mathcal{L} = 1/4$ makes the estimated error for the mean gap be less than 10%. Lastly, the ratio λ_s/λ_1 has to be sufficiently small, i.e., below $1/1024$. Thus, for such a system, a calculation should be as large as 8192×8192 to achieve an accuracy of $\mathcal{O}(10\%)$ (in the absence of extrapolation). This is the largest system that is commonly run on a single commodity CPU core or on a single GPU. The choice for the reference system for $H = 0$, $p^* = 0.353$ differs quite substantially from that just discussed. Now, one would probably be better off with $a/\lambda_s = 1/16$. However, this time $\mathcal{L}/\lambda_s = 1/512$ is more than sufficient. (For $H = 0$, the value of λ_1 is irrelevant, once $\mathcal{L}/\lambda_s$ has been fixed). Thus, one needs a system of similar size as before to approach the desired limits.

For smaller system sizes it is still possible to get accurate values of $\Delta\bar{u}/\bar{h}$ by extrapolating the computed

value to the TFC limit using Eq. (27) and the information from Tables 3, 4.

H	C_c	C_f	C_t	α_c	α_f	α_t
0.3	0.1956	7.4279	0.1076	1	0.2639	1
0.5	0.1376	7.0747	0.1107	1	0.2544	1
0.8	0.0891	2.5573	0.0353	1	0.0788	1

Table 3 Coefficients and powers in Eq. (27) for $\Delta\bar{u}/\bar{h}$ at $p^* = 0.007$ obtained from the GFMD results.

H	C_c	C_f	C_t	α_c	α_f	α_t
0.3	0.1166	0.8058	$6.5851 \cdot 10^{-4}$	1	0.3009	1
0.5	0.0515	1.6523	$7.0326 \cdot 10^{-4}$	1	0.5072	1
0.8	0.0199	3.4070	$1.3495 \cdot 10^{-5}$	1	0.6665	1

Table 4 Coefficients and powers in Eq. (27) for $\Delta\bar{u}/\bar{h}$ at $p^* = 0.007$ obtained from the GFMD results.

3.2 Extrapolated results

We present reference data for the relative contact area and the mean gap. From the previous sections we conclude that extrapolating these quantities to the TFC limit does not have simple and universal rules. Therefore, to get a reasonably small error with the smallest possible computational expenditures in a contact mechanics simulation, one has to take into account the quantity of interest, the statistical properties of the surface roughness (i.e., the Hurst exponent and $\bar{g}$) and the pressure. For example, for the mean gap at low pressures and $H \lesssim 1$, one has to be careful with the thermodynamic correction, while at higher pressures and $H \gtrsim 0$ most attention should be paid to the continuum correction. We tried to satisfy the corresponding conditions for each data point in the reference plots shown below.

Figures 9 and 10 show the dependence of the relative contact and non-contact area on the dimensionless pressure obtained using GFMD for systems with several different values of the Hurst exponent. Predictions of Persson theory are also presented in the same plot, for which, as was mentioned before, the contact area does not depend on the Hurst exponent H . This is consistent with the GFMD results, which suggest that in the TFC limit the contact area for H close to 0 and to 1 should not differ by more than about 10%. Both our simulations and Persson theory show the contact area to be a linear function of the pressure at low loads (Fig. 9), which is consistent with previous studies [26, 35, 38]. At low pressures the contact area obtained using GFMD is somewhat higher than that predicted by Persson, which

Year	Authors	H values	κ	$\kappa(H = 0.8)$	ϵ_c	ϵ_f	ϵ_t
1976	Bush, Gibson, Thomas [6]	0 ... 1	$\equiv \sqrt{2\pi} \approx 2.51$	2.51	0	~ 1	0
2001	Persson [25]	0 ... 1	$\equiv \sqrt{8/\pi} \approx 1.60$	1.60	0	0	0
2004	Hyun, Pei, Molinari, Robbins [13]	0.3 ... 0.9	2.2 ... 1.8	1.8	0.5	$\approx 10^{-3}$	1
2007	Campaná, Müser [8]	0.2 ... 0.8	2.09 ... 1.98	1.98	ext.	$\approx 10^{-3}$	1
2012	Putignano, Afferrante <i>et al.</i> [35]	0.7 ... 1	2	2	$\ll 1$	$\approx 10^{-2}$	1
2012	Yastrebov, Anciaux, Molinari [38]	0.2 ... 0.84	2.7 ... 2.3	≈ 2.65	$\ll 1$	0.5 ... 0.01	$\ll 1$
2013	Current work	0 ... 0.8	2.16 ... 1.93	1.93	ext.	ext.	ext.

Table 5 Values of κ at $p/E^* \approx 0.01$ obtained by different authors. Note that for Persson theory, κ does not depend on the choice of ϵ_f . The notation “ $\ll 1$ ” means the value of a correction which is close enough to the corresponding limit such that the error due to the correction is less than about 5 %. For example, at low pressures $\epsilon_c = 1/32$ and $\epsilon_t = 1/4$ correspond to “ $\ll 1$ ”. The term “ext” means that an extrapolation to the corresponding limit is made.

is consistent with the fact that according to GFMD $\kappa \approx 2$, while Persson predicts $\kappa = \sqrt{8/\pi} \approx 1.6$. Close to the complete contact at high pressures (Fig. 10) the contact area changes nonlinearly with pressure. In this regime Persson theory is closer to the GFMD results, which is also consistent with the results of the previous section.

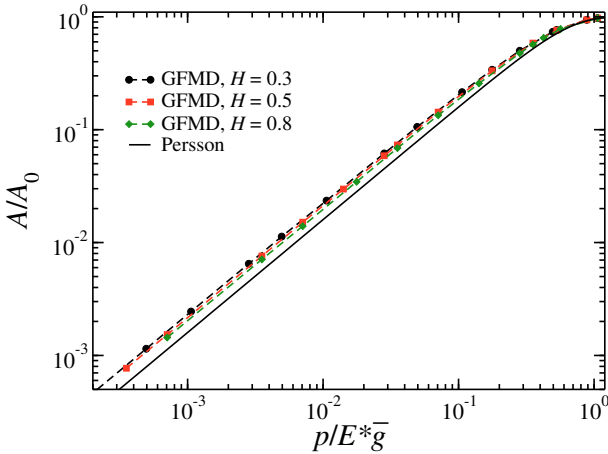


Fig. 9 Relative contact area as a function of the dimensionless pressure (at low pressures) obtained using GFMD simulations as well as predicted by the Persson theory. Both theory and simulations indicate a linear dependence, for Persson theory with a slope of 1.6, while the simulations give a slope of 1.93.2.16. The dependence on H is minor. High pressures are shown in Fig. 10.

A concise summary of the effects of the TFC corrections on a_r is given in Table 5. It contains the values of κ obtained at $p/E^* \approx 0.01$ by different authors. The data is presented in a chronological order and reflects the historical development of the insight to the problem. The corollary is that in the last few years most of the research groups have been performing computations close to the continuum limit. However, this has been often achieved by sacrificing either the fractal or the thermodynamic limit because of the scarce computational resources. According to our results, it is more important to satisfy the fractal limit because the fractal

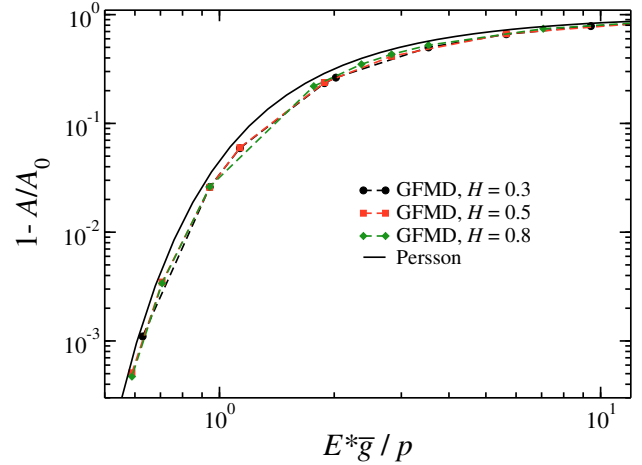


Fig. 10 Continuation of Fig. 9. In order to better show the non-linearity both in Persson theory and simulations, we plot the non-contact area vs. the inverse pressure.

correction ϵ_f leads to much larger errors than the thermodynamic one, unless pressures are extremely small.

Representing reference data for the mean gap meets some complications. As was shown in the previous section, $\Delta\bar{u}/\bar{h} \rightarrow 0$ in the fractal limit, following a power law with an exponent depending on H . This means that for $\Delta\bar{u}$ it is not possible to find a normalization factor that would allow superimposing the curves for different values of H , and necessitates a separate plot for each value of H . Additionally, as real surfaces have a limited range of self-affinity (which means that the fractal limit is never reached in practice, even though ϵ_f may be as small as 10^{-6}) and the functional dependence of the approaching the fractal limit is also pressure-dependent, it may also be helpful to have reference data for several values of ϵ_f .

We present such a set of reference data in Figs. 11, 12, and 13 along with the Persson theory predictions. The $\Delta\bar{u}$ versus p^* curves obtained in simulations and theory match within about 20% over almost the whole pressure range (except for the highest p^*) and have the functional form established in the literature [4]. Specifically, at low pressures (but high enough to avoid finite-

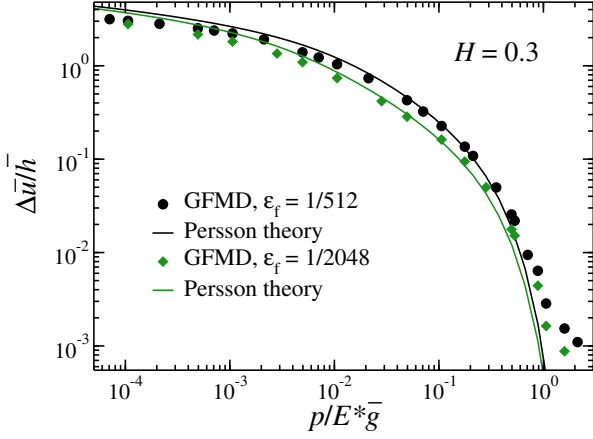


Fig. 11 Pressure as a function of the mean gap at different values of the fractal correction and $H = 0.3$. The continuum and thermodynamic corrections are close to the corresponding limits.

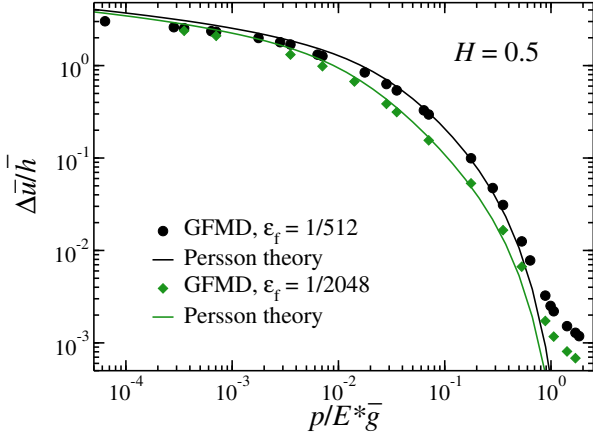


Fig. 12 Pressure as a function of the mean gap at different values of the fractal correction and $H = 0.5$. The continuum and thermodynamic corrections are close to the corresponding limits.

size effects [24]) there is a logarithmic region, while at higher pressures a more complicated non-linear dependence exists. As one would expect from the previous section, $\Delta\bar{u}$ decreases while approaching the fractal limit for all the pressures. However, we did not find a simple normalization factor that depends solely on ϵ_f such that the curves with different ϵ_f (but with the same H) would superimpose in the whole pressure range.

We stress that all points stem from simulations that fulfill the TC limit within 10%. As an example, for low pressures and $H = 0.8$, the continuum limit necessitates $\epsilon_c \leq 1/32$, and therefore very large systems, while for higher pressure $\epsilon_c \leq 1/4$ is sufficient. In all cases $\epsilon_t \leq 1/2$ suffices.

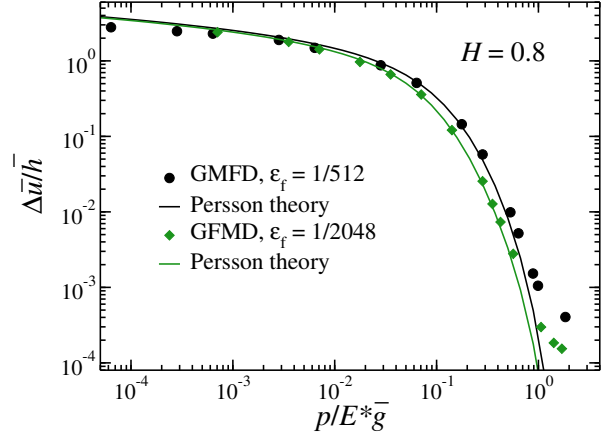


Fig. 13 Pressure as a function of the mean gap at different values of the fractal correction and $H = 0.8$. The continuum and thermodynamic corrections are close to the corresponding limits.

4 Conclusions

In this work we review analytical and computational techniques as well as present results of GFMD calculations for two interfacial quantities — the relative contact area a_r and the mean gap $\Delta\bar{u}$. The contact stiffness K , which is the derivative of $\Delta\bar{u}(p)$, is implicitly given by our data. We show that it is possible to considerably diminish the number of quantities necessary for the description of a contact mechanics problem by choosing proper units of measurements. In particular, the pressure should be expressed as a multiple of the effective elastic modulus times the RMS gradient, at least in the absence of adhesion. The proper choice for the unit of length is less obvious. While the RMS height is the intuitive choice, it does not turn out to be sufficient when expressing the mean interfacial gap. In fact we find that in the fractal limit $\epsilon_f \equiv \lambda_s/\lambda_l \rightarrow 0$, only short-wavelength properties matter, i.e., $\Delta\bar{u}$ is proportional to $\bar{g}\lambda_s$.

The observation that $\Delta\bar{u}$ is determined by short-wavelength properties of the height spectra in the fractal limit should not let one conclude that precise knowledge of the roughness at small length scales is needed to predict $\Delta\bar{u}$ in practice. Most surfaces have roughness exponents around $H = 0.8$ and most relative contact areas for practical applications tend to be much below 1%. For $H = 0.8$ and $a_r = \mathcal{O}(0.01)$, we find that the roughness spectrum must be self-affine over 14 decades, e.g., from nanometer to hundreds of kilometers in order to reach the fractal limit. Thus, most applications should be very far from it, unless H is small or surfaces are unusually soft. Knowledge of ϵ_f is therefore needed to predict $\Delta\bar{u}$ as a function of H and $p/\bar{g}E^*$ in addition to either $\bar{g}\lambda_s$ or $\bar{h}$. If $\bar{g}$ cannot be resolved accurately down

to the smallest scales, estimates for $\Delta\bar{u}$ can still be accurate, as that quantity is determined by roughness on mesoscopic scales. This behavior differs from that of a_r , which turns out to be inversely proportional to $\bar{g}$ and thus to be dominated by small wavelength properties of the surface spectra. In the latter case fractal corrections are relatively small, even if they are still more serious than thermodynamic and finite-size corrections.

In the present work we not only investigated the relevance of the ratio λ_s/λ_l but also the importance of continuum corrections as well as finite-size or thermodynamic corrections. The contribution of a *particular* correction depends on a number of factors, such as the pressure and the Hurst exponent and there are no general simple rules to select the appropriate values for ϵ_c and ϵ_t . However, the finite-size corrections tend to be the least problematic. Choosing the system size twice λ_l is sufficient to see the well-established linearity between normal pressure and contact stiffness down to $\mathcal{O}(0.01\%)$ relative contact area. Finite-size effects are only significant when contact is localized near the highest asperity. However, macroscopic surfaces must rest at least on three points to be mechanically stable so that averaging over at least three microscopic points of contact should be given. For a detailed discussion on how to include finite-size effects into contact mechanics, we point the reader to Ref. [24].

One purpose of this work has been to further explore the validity of Persson theory of contact mechanics. We find that it is not only suitable to describe the contact area but also the non-contact area at high pressure. The first finding was to be expected, as Persson theory is valid at small p^* and moreover becomes exact at full contact. However, this does not imply that the *deviation* from full contact is also predicted correctly, i.e., the asymptotic behavior of the non-contact area at high pressure. Moreover, we observe that the dependence of $\Delta\bar{u}$ on the fractal correction – at fixed values for H , $\bar{h}$, and p^* – is predicted correctly, that is, it finds the correct functional dependence and exponents. Other numerical parameters, such as prefactors, are only slightly off. Merely the mean gap for relative contact areas close to unity does not appear to match the trends conveyed by the numerical results. This, however, only occurs for relative contact areas greater than 90%, which is an irrelevant regime for applications. Another point of criticism — not further elaborated herein — relates to the pressure distribution. It deviates from the predicted linear scaling at small pressure. For brevity, we chose to not present this here but rather to discuss it in future work together with an in-depth analysis of how to modify Persson theory to reflect the observed trends. However, concerning the observables investigated in this

work, the current Persson theory already provides an excellent description.

Acknowledgements We thank the Jülich Supercomputing Centre for computing time on JUGENE, JUQUEEN and JU-ROPA. MHM also thanks DFG for support through grant No. Mu 1694/5-1.

A Appendix. Persson contact mechanics theory for contact area and mean gap

A promising approach to contact mechanics and related topics is Persson theory [25, 26, 4]. The principal idea is to investigate how distributions, such as pressure and gap distribution functions, broaden when roughness is ignored initially but then is included gradually by considering roughness at larger and larger wave vectors — or greater “magnification.” Here, we will summarize those aspects of Persson theory which pertain to the reference data presented in the result section, namely for contact area and mean gap. Unlike the original literature, our presentation will be focused on the use of the dimensionless variables introduced in the main text.

Consider a contact in which the pressure distribution is locally constant, i.e., $p(x_0 \pm \lambda, y_0 \pm \lambda) \approx p_0$. One can then approximate the pressure distribution function locally with $\Pr(|\mathbf{r} - \mathbf{r}_0| < \lambda, p) = \delta(p - p_0)$. Now assume that we add some roughness to the interface by adding a Fourier component $\tilde{h}(\mathbf{q}) \exp(i\mathbf{q} \cdot \mathbf{r})$ to the roughness, where $q = 2\pi/\lambda$. If the amplitude $\tilde{h}(\mathbf{q})$ is small, contact in the domain will remain essentially perfect. This leads to a change of the local stress, see Eqs. (18) and (19), according to

$$p(|\mathbf{r} - \mathbf{r}_0| < \lambda) \approx p(\mathbf{r}_0) + \frac{E^*}{2} q \tilde{h}(\mathbf{q}) \exp(i\mathbf{q} \cdot \mathbf{r}). \quad (30)$$

This means that in the vicinity of $\mathbf{r}_0$ there is no change of the pressure, but there is a broadening of the pressure distribution. In other words, the average pressure remains p_0 , but the second moment increases from $\Delta p_{\text{old}}^2 = 0$ to $\Delta p_{\text{new}}^2 = \Delta p_{\text{old}}^2 + |E^* q \tilde{h}(\mathbf{q})/2|^2$. One of the main approximations of Persson theory is that the broadening of the pressure distribution would be similar even if Δp_{old}^2 were not zero. The pressure distribution then broadens, whenever we include roughness at smaller scales. Since the broadening does not depend on pressure or location, the total broadening, averaged over the entire contact, will then be

$$\Delta p^2 = \sum_{\mathbf{q}} \left(\frac{qE^*}{2} \right)^2 C(\mathbf{q}) = \left(\frac{E^*}{2} \right)^2 \bar{g}^2. \quad (31)$$

In the last step, we have made use of the fact that differentiating (heights) in real space corresponds to multiplying with wave vectors in Fourier space.

It is known from the law of large numbers that folding distributions functions iteratively according to

$$\Pr_{\text{new}}(p) = \int dp' \Pr_{\text{old}}(p') \text{Tr}(p'|p) \quad (32)$$

ultimately leads to a Gaussian, where $\text{Tr}(p'|p)$ is the probability that the local pressure changes from p' to p after (additional) roughness is included in the calculation. As a first approximation, one therefore finds $\Pr(p) \approx \exp[-(p - p_0)^2 / 2\Delta p^2] / \sqrt{2\pi\Delta p^2}$ for the pressure distribution.

The problem of having a single Gaussian is that negative pressures have finite probability. However, we know that negative pressures are not allowed for nonadhesive hard-wall interactions. This problem can be solved by absorbing into noncontact any part of the pressure distribution function that becomes negative (there, the pressure is set to zero). If two surfaces do not touch when spatial features are resolved down to wavelength λ , they should not come back into contact when roughness at even smaller wavelengths is resolved. One can implement an absorbing boundary condition, similar to the way how mirror charges are introduced in electrostatics, by subtracting another Gaussian from the original Gaussian:

$$\Pr(p > 0) = \frac{\exp\left\{-\frac{(p-p_0)^2}{2\Delta p^2}\right\} - \exp\left\{-\frac{(p+p_0)^2}{2\Delta p^2}\right\}}{\sqrt{2\pi}\Delta p^2}. \quad (33)$$

The effect of the mirror Gaussian is to implement the boundary condition, while leaving the mean pressure $\bar{p} = \int p \, dp \, \Pr(p > 0)$ invariant, i.e., independent of Δp . Persson finds Eq. (33) through a small detour by mapping the integral equation for the broadening of the pressure distribution to a differential equation, which is isomorphic to the diffusion equation. This detour, however, can be avoided without loss of information.

Eq. (33) enables one to deduce the relative contact area

$$a_r = \int_{0^+}^{\infty} dp \, \Pr(p) \quad (34)$$

because any finite local pressure is interpreted as occurring where the solids are in contact. The solution of the integral reads

$$a_r = \operatorname{erf}\left(\frac{p_0}{\sqrt{2}\Delta p}\right) = \operatorname{erf}\left(\frac{\sqrt{2}p_0}{E^*\bar{g}}\right) \quad (35)$$

$$= \sqrt{\frac{8}{\pi}} \frac{p_0}{E^*\bar{g}} + \mathcal{O}\left\{\left(\frac{p_0}{E^*\bar{g}}\right)^3\right\}. \quad (36)$$

Three properties of the solution are interesting to observe: (i) it satisfies the finding of Sect. 2.3 that observables should depend on external pressure divided by the product of E^* and $\bar{g}$ but they should not depend on any other dimensionless variable other than possibly H . (ii) The solution turns out to not depend on H for any value of p_0 . (iii) Corrections to the linear relationship between contact area and pressure are only of order p_0^3 . This implies that linearity between load and contact area should persist up to at least 10% contact. These predictions are confirmed by Fig. 9.

Next, we wish to express the gap as a function of normal pressure. For $p_0 \rightarrow \infty$, the mean gap tends to zero, while the two surfaces touch in just one point for $p_0 = 0^+$. Given the nature of our problem, there is a monotonic dependence of the gap on load in between the two limiting cases of no contact and full contact. This allows us to express the work done by the pressure on the elastic manifold as follows:

$$\frac{1}{A_0} dU_{el} = -p(\bar{u}) d\bar{u} = -p \frac{d\bar{u}}{dp} dp, \quad (37)$$

where $\bar{u} = u_0 + \tilde{u}(\mathbf{q} = 0)$ denotes the displacement with respect to some well-chosen reference point u_0 . We choose u_0 in such a way that it corresponds to the full contact at the external pressure $p_{ref} = \infty$. Thus, if we knew U_{el} as a function of p , we could obtain the displacement $\bar{u}$ via

$$\Delta \bar{u} = \bar{u}(p_0) - \bar{u}(p_{ref}) = \frac{1}{A_0} \int_{p_0}^{p_{ref}} dp' \frac{1}{p'} \frac{dU_{el}}{dp'}. \quad (38)$$

To solve for the elastic energy, Persson argues [25] that the displacement field $\tilde{u}(\mathbf{q})$ follows $\tilde{h}(\mathbf{q})$ for the fraction of the interface that is in contact at a resolution of $\mathbf{q}$. Thus,

$$\frac{1}{A_0} U_{el}(p_0) = \frac{E^*}{4} \sum_{\mathbf{q}} \gamma(p_0, \mathbf{q}) q |\tilde{h}(\mathbf{q})|^2, \quad (39)$$

where

$$\gamma(p_0, \mathbf{q}) = a_r(p_0, \mathbf{q}) [\gamma + (1 - \gamma) a_r^2(p_0, \mathbf{q})] \quad (40)$$

is an *ad hoc* helper function which approximates the dependence of the elastic energy on the resolution-dependent contact area $a_r(p_0, \mathbf{q})$ in different pressure regimes. At low external pressures $\gamma(p, \mathbf{q})$ is proportional to $a_r(p_0, \mathbf{q})$ while at the complete contact it is equal to 1. The contact area $a_r(p_0, \mathbf{q})$ follows from Eq. (35) or (36) by confining the evaluation of $\bar{g}$ to wave numbers less than q_s . An empirical correction factor γ has the value of the order of unity (a value of 0.42 has been used in the literature [27,37]) and reflects the fact that the elastic energy stored in the contact region is less than the average elastic energy for perfect contact [27,37].

Substituting Eq. (39) into Eq. (38) and assuming an *ideal self-affine surface* characterized with the power spectrum from the Eq. (8), after some algebra we obtain the following expression for the mean gap $\Delta \bar{u}$ as a function of the external pressure p_0 :

$$\Delta \bar{u} = \frac{\bar{h}}{\sqrt{2\pi}} \sqrt{\frac{H}{1-H}} \sqrt{\frac{1}{1-\epsilon_f^{2H}}} \times \int_0^c dk (k^2 + 1)^{1/(2H-2)} \left[\gamma E_1(x^2) + 3(1-\gamma) \times \int_1^\infty [\operatorname{erf}(tx)]^2 \exp(-t^2 x^2) \frac{dt}{t} \right], \quad (41)$$

where we have replaced the Fourier sum with a Fourier integral. Other quantities in Eq.(41) are $x \equiv \sqrt{2} p_0 c / (E^* \bar{g} k)$, $c^2 \equiv (1 - \epsilon_f^{2-2H}) / \epsilon_f^{2-2H}$, and E_1 is a variant of the exponential integral given by

$$E_\alpha(x) = \int_1^\infty \frac{\exp[-tx]}{t^\alpha} dt, \quad (42)$$

and available as a special function in standard libraries (e.g., the Boost library for C++ [1]).

Eq. (41) is not analytically tractable. However, in future work we will investigate $\gamma(p_0, \mathbf{q})$ in more detail and an expression might be found that allows to simplify the integral further.

The pseudocode for computing Persson theory is as follows:

- Specify the input parameters
These mainly include the characteristics of the rough surface.
- Express the input in the dimensionless form.
- Calculate the contact area using Eq. (35)
- Calculate the mean gap using Eq. (41)

Note that choosing a logarithmic mesh for the nested integral to ∞ in Eq. (41) will improve efficiency without significant loss of accuracy. This effect can also be achieved through a variable substitution of the form $p = p_0 \exp(\mu)$.

B Appendix. A review of Green's function molecular dynamics

Green's function molecular dynamics (GFMD) makes it possible to calculate the response of a semi-infinite elastic solid to external forces acting solely on the surface [7, 16]. It can be described as a classical boundary value method which is solved with regular molecular dynamics. In principle, it is possible to simulate natural dynamics. However, in this work we are only concerned with the static limiting case, which is why we content ourselves with damped dynamics. These should be set up in such a way that the static solution is found in the quickest possible way. Using natural dynamics would not be efficient, as these would suffer from critical slowing down. The number of steps to reach equilibrium would scale with the square of the linear dimension.

In principle, GFMD attempts the solution of Eq. (19). However, the interfacial pressure is not known explicitly but only implicitly through the boundary condition Eq. (1). This implies that the curvature of the potential diverges when the two surfaces start to overlap, which, in principle, makes the use of an infinitely small time step necessary. In the early days of molecular and computational fluid dynamics, several strategies were designed for related problems in the context of hard-disk interactions [3]. One approach was to assign a coefficient of restitution to a collision of two hard disks which specifies how much of the kinetic energy is conserved during a collision. For our contact mechanics problem, we set this coefficient to zero.

In the following, we will describe how we implement these dynamics and also describe all other main aspects of our GFMD program in terms of pseudocode.

- Setup of rigid substrate

Assign uniform random numbers of zero mean and finite variance for the real and imaginary parts of $\tilde{h}(\mathbf{q})$. All $\tilde{h}(\mathbf{q})$ are divided by q^{1+H} . Next, heights are transformed into real space. For this purpose, we use the FFTW library [11]. We shift the elastic surface such that it touches the rigid substrate in one (or more) points without applying pressure (i.e., $h_{\min} = 0$). The largest height is then stored in $h_{\max}$. RMS gradient and RMS height are best evaluated in Fourier space.

- Setup of elastic top solid

Set all grid points to $h_{\max}$ and define this as a reference. Initialize the damping η such that the slowest mode, i.e., the center-of-mass mode is critically damped or slightly underdamped. This can be achieved with $\eta \propto p/E^* \bar{g} \mathcal{L}$, unless a_r is close to 0. When a_r is close to 0 we use $\eta \propto (p/E^* \bar{g})^\alpha \sqrt{\beta/\mathcal{L}}$, where α and β are the parameters which depend on $\mathcal{L}$ and typically are found empirically. Note that neither the mass nor the damping should be made a function of wave vector if nonholonomic boundary conditions are in place.

- Loop over time steps until converged

- Transform displacements into Fourier space
- Calculate elastic restoring forces
 $\tilde{F}(\mathbf{q}) = -q(E^*/2)\tilde{u}_{\text{now}}(\mathbf{q})$
- Add external pressure
 $\tilde{F}(0) \leftarrow \tilde{F}(0) + p$
- Add damping forces
 $\tilde{F}(\mathbf{q}) \leftarrow \tilde{F}(\mathbf{q}) + \eta\{\tilde{u}_{\text{now}}(\mathbf{q}) - \tilde{u}_{\text{old}}(\mathbf{q})\}$
- Use Verlet to solve equation of motion
 $\tilde{u}_{\text{new}}(\mathbf{q}) = 2\tilde{u}_{\text{now}}(\mathbf{q}) - \tilde{u}_{\text{old}}(\mathbf{q}) + \tilde{F}(\mathbf{q})\Delta t^2$
- Transform displacement into real space
- Implement the boundary condition
 $u_{\text{new}}(\mathbf{r}) \leftarrow \max\{u_{\text{new}}(\mathbf{r}), -h(\mathbf{r})\}$

- Assign $u_{\text{old}}(\mathbf{r}) \leftarrow u_{\text{now}}(\mathbf{r})$
 $u_{\text{now}}(\mathbf{r}) \leftarrow u_{\text{new}}(\mathbf{r})$
- Check termination conditions, e.g. that the contact area, defined as the relative number of points satisfying $u(\mathbf{r}) = -h(\mathbf{r})$, may not have changed in many steps; kinetic energy of each individual mode less than a threshold, etc.

References

1. Boost C++ Libraries. <http://boost.org>
2. Aifantis, E.C.: The physics of plastic deformation. *International Journal of Plasticity* **3**, 211 (1987)
3. Allen, M.P., Tildesley, D.J.: *Computer Simulation of Liquids*. Oxford University Press, Oxford (1987)
4. Almqvist, A., Campañá, C., Prodanov, N., Persson, B.N.J.: Interfacial separation between elastic solids with randomly rough surfaces: Comparison between theory and numerical techniques. *J. Mech. Phys. Solids* **59**, 2355 (2011)
5. Barber, J.R.: Incremental stiffness and electrical contact conductance in the contact of rough finite bodies. *Phys. Rev. E* **87**, 013,203 (2013)
6. Bush, A.W., Gibson, R.D., Thomas, T.R.: Elastic contact of a rough surface. *Wear* **35**, 87 (1975)
7. Campañá, C., Müser, M.H.: Practical green's function approach to the simulation of elastic semi-infinite solids. *Phys. Rev. B* **74**, 075,420 (2006)
8. Campañá, C., Müser, M.H.: Contact mechanics of real vs. randomly rough surfaces: A Green's function molecular dynamics study. *Europhys. Lett.* **77**, 38,005 (2007)
9. Campañá, C., Persson, B.N.J., Müser, M.H.: Transverse and normal interfacial stiffness of solids with randomly rough surfaces. *J. Phys.: Condens. Matter* **23**, 085,001 (2011)
10. Dapp, W.B., Lücke, A., Persson, B.N.J., Müser, M.H.: Self-affine elastic contacts: percolation and leakage. *Phys. Rev. Lett.* **108**, 244,301 (2012)
11. Frigo, M., Johnson, S.G.: The design and implementation of fftw3. *Proceedings of the IEEE* **93**(2), 216 (2005)
12. Greenwood, J.A., Williamson, J.B.P.: Contact of nominally flat surfaces. *Proc. R. Soc. London* **A295**, 300 (1966)
13. Hyun, S., Pei, L., Molinari, J.F., Robbins, M.O.: Finite-element analysis of contact between elastic self-affine surfaces. *Phys. Rev. E* **70**, 026,117 (2004)
14. Johnson, K.L.: *Contact Mechanics*. Cambridge University Press, New York (1985)
15. Kendall, K.: *Molecular Adhesion and its Applications: The Sticky Universe*. Kluwer Academic, New York (2001)
16. Kong, L.T., Bartels, G., Campañá, C., Denniston, C., Müser, M.H.: Implementation of greens function molecular dynamics: An extension to lammmps. *Computer Physics Communications* **180**, 1004 (2009)
17. Landau, L.D., Lifshitz, E.M.: *Theory of Elasticity*, 3rd ed. Pergamon Press, Oxford (1970)
18. Lechenault, F., Pallares, G., George, M., Rountree, C., Bouchaud, E., Ciccotti, M.: Effects of finite probe size on self-affine roughness measurements. *Phys. Rev. Lett.* **104**, 025,502 (2010)
19. Lorenz, B., Krick, B.A., Mulakaluri, N., Smolyakova, M., Dieluweit, S., Sawyer, W.G., Persson, B.N.J.: Adhesion: role of bulk viscoelasticity and surface roughness. *J. Phys.: Condens. Matter* **25**, 225,004 (2013)

20. Lorenz, B., Persson, B.N.J.: Leak rate of seals: Effective-medium theory and comparison with experiment. *Eur. Phys. J. E* **31**, 159 (2010)
21. Lorenz, B., Persson, B.N.J.: Time-dependent fluid squeeze-out between solids with rough surfaces. *Eur. Phys. J. E* **32**, 281 (2010)
22. Lyashenko, I., Pastewka, L., Persson, B.N.J.: On the validity of the method of reduction of dimensionality: Area of contact, average interfacial separation and contact stiffness. *Tribology Letters* **52**, 223–229 (2013)
23. Ma, Z.S., Zhou, Y.C., Long, S., Lu, C.: On the intrinsic hardness of a metallic film/substrate system: Indentation size and substrate effects. *International Journal of Plasticity* **34**, 1 (2012)
24. Pastewka, L., Prodanov, N., Lorenz, B., Müser, M.H., Robbins, M.O., Persson, B.N.J.: Finite-size scaling in the interfacial stiffness of rough elastic contacts. *Phys. Rev. E* **87**, 062,809 (2013)
25. Persson, B.N.J.: Theory of rubber friction and contact mechanics. *J. Chem. Phys.* **115**, 3840 (2001)
26. Persson, B.N.J.: Contact mechanics for randomly rough surfaces. *Surf. Sci. Rep.* **61**, 201 (2006)
27. Persson, B.N.J.: Relation between interfacial separation and load: A general theory of contact mechanics. *Phys. Rev. Lett.* **99**, 125,502 (2007)
28. Persson, B.N.J., Albohr, O., Tartaglino, U., Volokitin, A.I., Tosatti, E.: On the nature of surface roughness with application to contact mechanics, sealing, rubber friction and adhesion. *J. Phys. Condens. Matter* **17**, R1–R62 (2005)
29. Persson, B.N.J., Prodanov, N., Krick, B.A., Rodriguez, N., Mulakaluri, N., Sawyer, W.G., Mangiagalli, P.: Elastic contact mechanics: Percolation of the contact area and fluid squeeze-out. *Eur. Phys. J. E* **35**, 5 (2012)
30. Persson, B.N.J., Scaraggi, M.: On the transition from boundary lubrication to hydrodynamic lubrication in soft contacts. *J. Phys. Condens. Matter* **21**, 185,002 (2009)
31. Persson, B.N.J., Tosatti, E.: The effect of surface roughness on the adhesion of elastic solids. *J. Chem. Phys.* **115**(12), 5597 (2001)
32. Persson, B.N.J., Yang, C.: Theory of the leak-rate of seals. *J. Phys. Condens. Matter* **20**, 315,011 (2008)
33. Power, W.L., Tullis, T.E.: Euclidean and fractal models for the description of rock surface roughness. *Journal of Geophysical Research* **96**, 415 (1991)
34. Prodanov, N., Gachot, C., Rosenkranz, A., Mücklich, F., Müser, M.H.: Contact mechanics of laser-textured surfaces: Correlating contact area and friction. *Tribol. Lett.* **50**, 41 (2013)
35. Putignano, C., Afferrante, L., Carbone, G., Demelio, G.: The influence of the statistical properties of self-affine surfaces in elastic contacts: A numerical investigation. *J. Mech. Phys. Solids* **60**, 973 (2012)
36. Putignano, C., Afferrante, L., Carbone, G., Demelio, G.: A multiscale analysis of elastic contacts and percolation threshold for numerically generated and real rough surfaces. *Tribology International* **64**, 148 (2013)
37. Yang, C., Persson, B.N.J.: Contact mechanics: contact area and interfacial separation from small contact to full contact. *J. Phys. Condens. Matter* **20**, 215,214 (2008)
38. Yastrebov, V.A., Anciaux, G., Molinari, J.F.: Contact between representative rough surfaces. *Phys. Rev. E* **86**, 035,601R (2012)