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Evaluation of the MOZAIC Capacitive Hygrometer during the airborne field study CIRRUS-III

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Abstract. The MOZAIC Capacitive Hygrometer (MCH) is usually operated aboard passenger aircraft in the framework of MOZAIC (Measurement of Ozone by Airbus In-Service Aircraft) for measuring atmospheric relative humidity (RH). In order to evaluate the performance of the MCH, the instrument was operated aboard a Learjet 35A research aircraft as part of the CIRRUS-III field study together with a closed-cell Lyman- α fluorescence hygrometer (Fast in situ Stratospheric Hygrometer, or FISH) and an open-path tunable diode laser system (Open-path Jülich Stratospheric TDL ExpeRiment, or OJSTER) for water vapour measurement. After reducing the CIRRUS-III data set to data corresponding to MOZAIC aircraft operation conditions, the 1 Hz RH data cross correlation between the MCH and reference instruments FISH (clear sky) and OJSTER (in-cirrus) yielded a remarkably good agreement of $R^2 = 0.92$ and slope m = 1.02 and provided a MCH uncertainty of 5 % RH. Probability distribution functions of RH deduced from the MCH and reference instruments agreed well between 10 and 70 % RH with respect to liquid water in the ambient temperature range of ca. -70 to -40 °C. The use of MCH data is limited to sensor temperatures above the calibration limit of $T_{\rm sensor} = -40\,^{\circ}{\rm C}$ (corresponds to ambient temperature of $T_{\text{ambient}} = -70 \,^{\circ}\text{C}$ at typical cruising speed of long-haul passenger aircraft). Good performance of the MCH for clear sky as well as for in-cirrus conditions demonstrated the sensor robustness also for operation inside ice clouds.

1 Introduction

Water vapour is one of the most important variables for weather prediction and climate research. Particularly, the interaction between the water vapour in the UT–LS (upper troposphere and lowermost stratosphere) and tropopause dynamics is not well understood. Thus, in the latest IPCC report (IPCC, 2013), it is stated that the knowledge about potential trends and climate feedback mechanisms of uppertropospheric water vapour is poor because of the lack of long data records of high quality in this specific region of the global atmosphere. Neither the global radiosonde network nor satellites can provide measurements of the required spatial and temporal resolution, while the regular in situ measurement of upper-tropospheric humidity (UTH) is still difficult.

Since 1994, the European research programme MOZAIC (Measurement of Ozone by Airbus In-Service Aircraft; Marenco et al., 1998) and its successor IAGOS (In-service Aircraft for a Global Observing System; Petzold et al., 2013) have been providing regular data for relative humidity (RH) and other meteorological quantities like temperature and pressure as well as data on atmospheric composition (e.g. ozone and CO) with high spatial and temporal resolution on a global scale. The long-term observations are obtained by in situ measurements aboard civil passenger aircraft using the existing infrastructure of the international air transport system. However, the continuous high-quality in situ measurements are restricted to the major global flight routes and to the cruising altitude band of 9–13 km; i.e. the observations refer to a large extent to the UT–LS region. Relative humidity

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data from the MOZAIC programme have been used for various climatological studies, including the distribution of UTH (Kley et al., 2007; Luo et al., 2007, 2008), the distribution of RH with respect to ice (RH_{ice}; e.g. Gierens et al., 1997, 1999) and ice-supersaturation regions (e.g. Gierens et al., 2000; Spichtinger et al., 2003) in the upper troposphere.

Atmospheric RH is measured in the MOZAIC/IAGOS programme through a compact airborne humidity sensing device using capacitive sensors (MOZAIC Capacitive Hygrometer: MCH). The sensor itself and the applied calibration techniques are described in detail by Helten et al. (1998). The first validation studies from formation flights of a MOZAIC aircraft and a research aircraft are reported by Helten et al. (1999), while Smit et al. (2008) present an approach for a potential in-flight calibration of the MCH. A reanalysis of the global MOZAIC RH data set for the period 2000–2009 was performed recently (Smit et al., 2014).

In order to assess the validity of the long-term water vapour data and their limitations, Helten et al. (1999) provided an in-flight comparison of MOZAIC and POLINAT (Schlager et al., 1997; Schumann, 1997) water vapour measurements. However, this formation flight intercomparison was difficult to analyse because the twin-engine research aircraft Falcon 20 had to follow the MOZAIC Airbus A340-300 with changing time lags and distances whereby sampling of identical air masses can not always be ensured. In 2006, there was the opportunity to participate in the aircraft campaign CIRRUS-III along with high-precision researchgrade instruments for measuring the water vapour volume mixing ratio (VMR). The in-flight single-platform measurements permitted a blind intercomparison of the MCH with high-performance water vapour instruments by measuring the same air masses and under different atmospheric conditions. A similar analysis of the improved IAGOS Capacitive Hygrometer is in preparation and will be published elsewhere.

2 MOZAIC Capacitive Hygrometer

A detailed description of the MOZAIC Capacitive Hygrometer is given by Helten et al. (1998, 1999) and Smit et al. (2014). In the following, we summarise the original descriptions.

The compact airborne MCH consists of a capacitive sensor (Humicap-H, Vaisala, Finland) whose capacitance depends on the relative humidity of the dielectric layer of the condenser and a platinum resistance sensor (Pt100) for the direct measurement of the temperature at the humidity sensing surface. The basic measurement process is based on the diffusion-limited adsorption of the H₂O molecules by the dielectric membrane of the sensor. Since diffusion is strongly temperature-dependent, the sensor response slows down with decreasing temperatures. Figure 1 shows how both sensors are mounted in the used air sampling hous-

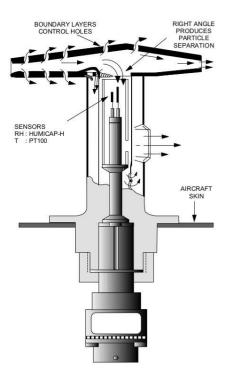


Figure 1. Cross section of the airborne capacitive sensing element. Right angle protects against particles, and control holes in the side wall minimise internal boundary layer effects (Helten et al., 1998).

ing (Model 102 BX, Rosemount Inc.; see Stickney et al., 1990). The relative humidity and temperature signals are fed into a microprocessor-controlled transmitter unit (HMP230, Vaisala) which passes the signals to the data acquisition system. The data conversion from capacitance signals to relative humidity values is performed offline in a separate data quality assurance and analysis step.

In its original MOZAIC mounting position aboard an Airbus A340-400 the sensor housing is placed ca. $7\,\mathrm{m}$ downstream of the aircraft nose on the left side with a $7\,\mathrm{cm}$ distance from the aircraft skin to avoid possible contaminating interferences of the aircraft skin. Inside the Rosemount housing the air flow is separated into the main flow, which traverses straight through the housing, and the minor flow, which follows a sharp right angle into a smaller channel where the sensors are placed. The housing is equipped with small holes in the side wall to neglect internal boundary layer effects by sucking the internal boundary layer air through the holes. The right angle of the minor flow protects the RH and T sensors against dust, water and particles.

Due to the strong speed reduction in the inlet part of the housing, the sampled air flow is significantly heated through adiabatic heating. Assuming $100\,\%$ conversion of kinetic energy into heat during flow deceleration, the ambient temperature $T_{\rm ambient}$ (static air temperature, SAT) increases to the temperature at the sensor inside the housing, i.e. the sensor temperature $T_{\rm sensor}$ (total air temperature, TAT). Given the

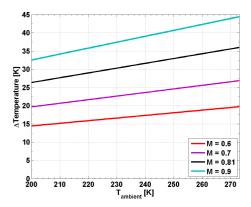


Figure 2. Sampled air flow is heated through adiabatic heating effects when entering the inlet. Δ Temperature describes the increase relative to the ambient temperature $T_{\rm ambient}$ (static air temperature, SAT; see Helten et al., 1998) for several aircraft speeds, i.e. the Mach number M, by assuming 100% conversion of kinetic energy to heat during flow deceleration.

fact that the adiabatic conversion of energy is not exactly 100%, the latter's quantity ($T_{\rm sensor}$) is calculated from the actually measured sensor temperature, i.e. the typically $0.1-1.0\,\rm K$ colder recovery temperature (total recovery temperature, TRT), and the so-called recovery factor. This aircraft-speed-dependent and empirically determined factor is provided by the housing manufacturer.

The relationship between T_{ambient} and T_{sensor} is a function of the aircraft speed, i.e. its Mach number M:

$$T_{\text{sensor}} = T_{\text{ambient}} \cdot \left(1 + \left(\frac{c_p - c_v}{2c_v} \right) \cdot M^2 \right),$$
 (1)

where c_p (= 1005 J kg $^{-1}$ K $^{-1}$) and c_v (= 717 J kg $^{-1}$ K $^{-1}$) are the specific heat of dry air at constant pressure and volume, respectively. The resulting difference between $T_{\rm sensor}$ and $T_{\rm ambient}$ at 10–12 km cruising altitude for different Mach numbers is displayed in Fig. 2: for the MOZAIC-typical aircraft speed of M=0.81 the adiabatic heating effect is ca. 30 K. $T_{\rm ambient}$ is derived from Eq. (1) with an uncertainty of less than ± 0.5 K resulting from uncertainties in $T_{\rm sensor}$ (± 0.25 K) and M. Because of the strong temperature increase, the detected dynamic relative humidity RH_{dynamic} is significantly lower than the static relative humidity RH_{static} of the ambient air at $T_{\rm ambient}$:

$$RH_{\text{static}} = (2)$$

$$RH_{\text{dynamic}} \cdot \left(\frac{T_{\text{ambient}}}{T_{\text{sensor}}}\right)^{\frac{c_p}{c_p - c_v}} \cdot \frac{e_{\text{s,liquid}}(T_{\text{sensor}})}{e_{\text{s,liquid}}(T_{\text{ambient}})},$$

where $e_{s,liquid}$ is the water vapour saturation pressure over liquid water at T_{sensor} and $T_{ambient}$, respectively. The water vapour saturation pressure over liquid water $e_{s,liquid}$ follows the Goff and Gratch (1946) formulation of saturation water vapour pressure over a plane surface of pure water or ice,

which was recommended by the World Meteorological Organization (WMO, 1983) and adapted to the international temperature scale 1990 (ITS-90) by Sonntag (1994). For fast, high-flying aircraft the relation $RH_{\text{static}}\,/\,RH_{\text{dynamic}}$ reaches a factor of ca. 13, which leads to the fact that the RH sensor operates in the lowest 10 % of its full dynamic range. Since the sensor is operating in the lower part of its full dynamic range, an individual calibration of each sensor is necessary, which is accomplished in the atmospheric simulation chamber at Jülich (Smit et al., 2000) before installation on the aircraft and after detachment past 500 h of flight. This corresponds to about 4-6 weeks between installation and deinstallation. These calibrations are made over a sensor temperature range between -40 and +20 °C against (i) a Lyman- α fluorescence hygrometer (Kley and Stone, 1978) at water vapour mixing ratios below 1000 ppmv (relative accuracy $\pm 4\%$, Helten et al., 1998) and (ii) a dew/frost point hygrometer (General Eastern, Type D1311R) at water vapour mixing ratios above 1000 ppmv with an accuracy of ± 0.5 K. The relative humidity of a calibrated sensor (RH_C) at constant temperature T is found to be linearly related to the uncorrected output value (RH_{UC}) provided by the HMP230 transmitter unit.

$$RH_{C}(T) = a(T) + b(T) \cdot RH_{UC}(T)$$
(3)

In Sect. 3.2 the calibration procedure of the MCH is described which was used during the CIRRUS-III field study. It combines the standard procedure based on Helten et al. (1998) and the in-flight calibration described by Smit et al. (2008).

Evaluation of 9 years of pre- and post-flight calibrations in MOZAIC has shown that the offset a(T) is the most critical parameter in determining the uncertainty of the measurements with a shift of about -5% RH, while the sensitivity (slope) b(T) is less critical and only changes by about -2%.

3 Experimental section

3.1 The CIRRUS-III field campaign

To extend the performance assessment of the MCH from the formation flight intercomparison (Helten et al., 1999), the sensor was operated aboard a Learjet 35A twin-engine business-jet aircraft as part of the CIRRUS-III field study, which was coordinated by Forschungszentrum Jülich.

The overarching goals of CIRRUS-III were to understand the formation mechanism of cirrus clouds in different background conditions, their radiative effects and the microphysical properties of the cirrus cloud particles. In total six flights were conducted in the period between 23 and 29 November 2006 at mid-latitudes (45–70° N; see Fig. 3) and at flight altitudes between 7 and 12 km. These flights in the UT–LS were launched from the Hohn Air Base in northern Germany with the Learjet 35A operated by *enviscope* GmbH.

Table 1. CIRRUS-III flight overview at cruise altitude. Air masses are divided into "troposphere" and "stratosphere" with the ozone VMR threshold of 125 ppmv.

Flight no.	Date	Take-off/ landing (UTC)	Temperature range	H ₂ O VMR range	In/out of cirrus	Stratosphere/ troposphere
1	24 Nov	10:47/14:53	-62.6 to −52.8 °C	24–107 ppmv	95/96 min	2/190 min
2	28 Nov	08:22/12:07	-62.4 to -44.1 °C	17-138 ppmv	4/160 min	11/153 min
3	28 Nov	13:31/17:25	-60.0 to -42.4 °C	27-360 ppmv	56/124 min	5/175 min
4	29 Nov	09:16/13:51	-61.2 to -45.8 °C	16–216 ppmv	62/158 min	2/218 min
Sum			-62.6 to −42.4° C	16-360 ppmv	217/537 min	19/735 min



Figure 3. CIRRUS-III flight track overview (map data ©2008 Google, Sanborn).

For the sensor intercomparison studies CIRRUS-III provided 4 flights (see Table 1). The data set consists of ca. 13 flight hours in air masses colder than $-40\,^{\circ}$ C at cruise altitude, ca. 4 flight hours in cirrus clouds and 9 flight hours out of clouds. Furthermore, stratospherically influenced air masses were sampled for 19 min with ozone VMR above 125 ppmv, measured by the dual-beam UV-absorption ozone photometer JOE (Jülich Ozone Experiment) (Mottaghy, 2001). Two flights had to be discarded due to inlet heating problems at the reference instrument FISH (Fast in situ Stratospheric Hygrometer). An overview of the individual flights is provided in Table 1.

3.2 Instrumentation

During the CIRRUS-III field campaign, high-precision research-grade instruments were operated aboard the aircraft to characterise the air masses probed during flight patterns in frontal cirrus clouds. An important part of the instrumentation was dedicated to the measurement of gas-phase and total water. The instrumentation included a MCH and an open-

path tunable diode laser (TDL) system (Open-path Jülich Stratospheric TDL ExpeRiment, OJSTER; MayComm Instruments, May and Webster, 1993; Krämer et al., 2009) to measure gas-phase water vapour VMR. Simultaneously, total water VMR (i.e. gas-phase plus ice water) was measured by the reference measurement instrument FISH (Zöger et al., 1999). The closed-cell Lyman- α fluorescence hygrometer was equipped with a forward-facing inlet to sample gasphase water in clear sky and total water inside cirrus clouds. To determine whether a data point is in a cirrus cloud or not, the ratio of RH_{ice} from FISH (total water) and OJSTER (water vapour) was used (see Krämer et al., 2009). FISH was calibrated using a laboratory calibration facility with the capability to simulate realistic atmospheric conditions, i.e. water vapour VMR from several hundred to a few ppmv and pressure from 1000 to 10 hPa. During the calibration, the water vapour mixing ratio was determined using a commercial dew point hygrometer (MBW DP30). The instruments and the parameters derived from their measurements are listed in Table 2.

Instrument	Detection quantity	Measurement technique	Response time	Uncertainty	Reference
FISH	VMR [ppmv]	Lyman-α fluores- cence hygrometer	1 s	$7\% \pm 0.3 \text{ ppmv}$ (precision 1%)	Zöger et al. (1999)
OJSTER	VMR [ppmv]	Open-path TDL	1 s	10–15 %	May and Webster (1993)
MCH	RH _{liquid} [% RH]	Capacitive sensor	LT: 1 s, UT: 10 s LS: 1 min	$\pm (4-7) \%$ RH @ 10–13 km below $10 \text{ km} \pm (4-6) \%$ RH	Helten et al. (1998)

Table 2. Instruments and parameters used during the CIRRUS-III field campaign.

FISH: Fast in situ Stratospheric Hygrometer; OJSTER: Open-path Jülich Stratospheric TDL ExpeRiment; MCH: MOZAIC Capacitive Hygrometer; LT: lower troposphere; UT: upper troposphere; LS: lower stratosphere; for further information see Bange et al. (2013).

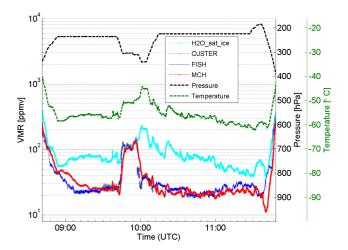


Figure 4. Time series of water vapour volume mixing ratio (VMR) from MCH (red), FISH (blue) and OJSTER (grey) during the CIRRUS-III flight on 28 November 2006. Ice saturation is shown in cyan, while pressure (black) and ambient air temperature (green) are plotted with dashed lines.

Prior to the CIRRUS-III campaign the MCH were (pre-flight) calibrated in the simulation chamber at Forschungszentrum Jülich following the procedures briefly described in Sect. 2. Unfortunately a post-flight calibration was not possible due to sensor failure after deinstallation of the MCH from the Learjet aircraft at the end of the campaign. From long-term experiences of MOZAIC preand post-flight calibrations it is well known that over the 3-month period between the pre-flight calibration and the end of the campaign the offset a(T) can change significantly by about 5 % RH while the slope b(T) changes by less than 2% on the relative scale (see Eq. 3 and Smit et al., 2014). In order to determine the potential change of the offset a(T)between pre-flight calibration and the end of the campaign, the so-called in-flight calibration method (Smit et al., 2008) was applied.

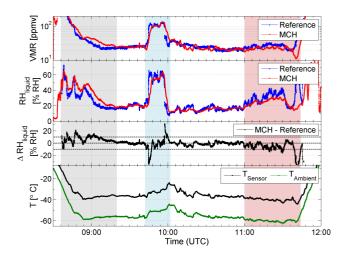


Figure 5. From top to bottom: VMR measured by the MCH (red) and the reference (blue), i.e. FISH (clear sky) and OJSTER (incirrus); RH $_{\rm liquid}$ and Δ RH $_{\rm liquid}$ (MCH and reference), as a function of flight time during flight 2 on 28 November 2006; and sensor temperature $T_{\rm sensor}$ (black) as well as ambient temperature $T_{\rm ambient}$ (green). The blue-shaded area represents air masses with high humidity and possible cirrus cloud. Air masses with sensor temperatures at and below the calibration limit are shaded in red. The grey-shaded sequence illustrates the effect of increasing response time as sensor temperatures decrease.

Thus, the sensor offset a(T) at lowest relative humidity was determined from the measurements themselves as obtained during periods of the aircraft flying in the lower stratosphere, where the water vapour mixing ratio reached well-defined minimum values. In our case, the minimum value in stratospherically influenced air masses was about 20 ± 1 ppmv as measured by the FISH instrument. Its resulting contribution to the RH_{liquid} signal of the MCH is minimal. Compared to the pre-flight calibration an offset change of (4.5 ± 1) % RH_{liquid} was found. The RH_{liquid} flight data of the MCH obtained during the CIRRUS-III campaign were corrected for this offset drift. The resulting overall uncertainty of the RH measurements by the MCH, including contributions from temperature uncertainties, is about ±5 %

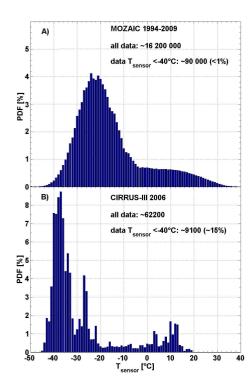


Figure 6. Frequency of occurrence for observations of T_{sensor} during ca. 15 years of MOZAIC (top panel) and CIRRUS-III (bottom panel).

 RH_{liquid} , which is in good agreement with the mean uncertainty range obtained from long-term MOZAIC measurements (Smit et al., 2014) .

4 Results – assessment of MCH performance

The instrumentation deployed in CIRRUS-III allows an inflight intercomparison of all water vapour instruments. Figure 4 illustrates an example of the kind of data collected from one research flight on 28 November 2006 (Flight 2). Data from the water vapour sensing instruments used for the intercomparison are shown as VMR. The $T_{\rm ambient}$ encountered during the flight ranged from -44.1 to $-62.4\,^{\circ}{\rm C}$ for relevant measurement altitudes. The respective water vapour VMR covered the range from 17 ppmv at the tropopause to ca. 150 ppmv in the free troposphere and even higher values during ascent from and descent into the airport.

For the instrument intercomparison we analysed the sensors with respect to RH_{liquid} since this is the parameter the MCH is calibrated against in the sensor temperature range (see Sect. 2). Further, data for water vapour VMR > 1000 ppmv were excluded from this study because the FISH instrument becomes optically opaque and thus insensitive to changes in VMR (Zöger et al., 1999).

In Fig. 5, we compare VMR data and RH_{liquid} data from the MCH and gas-phase reference, i.e. OJSTER data in cloud

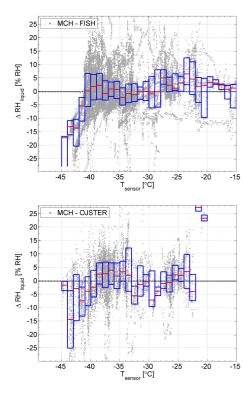


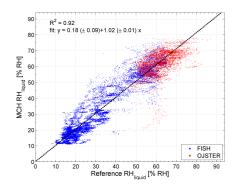
Figure 7. Differences in relative humidity RH_{liquid} of MCH and both reference instruments, i.e. FISH (top panel, clear sky) and OJSTER (bottom panel, in-cirrus), are scattered against the sensor temperature T_{sensor} . A drift towards too-dry MCH measurements below the calibration limit of $-40\,^{\circ}\text{C}$ is clearly seen. The median values (red lines in the box) of the $1\,^{\circ}\text{C}$ binned data as well as the 25th and 75th percentiles are within the calibration limits.

or otherwise FISH data, for a complete validation of the MCH for flight 2. Largest deviations of the MCH to the reference are found in clear-sky air masses for cold conditions with $T_{\rm sensor} < -40\,^{\circ}{\rm C}$ (this corresponds to ambient temperature below ca. $-60\,^{\circ}{\rm C}$ at M=0.70) and at transition sequences around the cirrus cloud. Except for these extreme conditions, the difference between the MCH and the reference is of the order of $10\,^{\circ}{\rm K}$ RH_{liquid} or less. Given the fact that during CIRRUS-III the MCH was operated at its lower limit of performance, the agreement with the research-grade reference instruments is remarkably good.

An analysis of MCH performance at the limit of its operation range is provided in the example of flight 2 in Sect. 4.2.

4.1 MCH performance against reference instruments

In order to prepare a data set for evaluation of the MCH performance, we introduced three filter operations to reduce the CIRRUS-III data set to MOZAIC typically operational conditions. First, it has to be noted that regular operation conditions of the MCH aboard long-haul passenger aircraft with a cruising speed of ca. M = 0.81 are characterised by $T_{\rm sensor} \ge -35\,^{\circ}{\rm C}$ (see Fig. 6a), which is within the



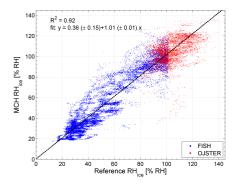


Figure 8. Comparison cross plot between reference, i.e. FISH (blue dots, clear sky) and OJSTER (red dots, in-cirrus), and MCH RH_{liquid} (left panel) and RH_{ice} (right panel) each displayed as a scatter plot with robust fitting curve (dashed line).

lower MCH calibration limit of -40 °C (see Sect. 2). However, during the operation aboard the slower-flying Learjet 35A (cruising speed < M = 0.70), $T_{\rm sensor}$ values significantly lower than -40 °C were reached (see Fig. 6b).

Consequently, data with $T_{\rm sensor} < -40\,^{\circ}{\rm C}$ were excluded from the analysis. This fact is illustrated in Fig. 7, which shows the difference in RH_{liquid} between MCH and FISH data for clear-sky conditions and OJSTER data for in-cirrus conditions, according to $T_{\rm sensor}$. Furthermore, the maximum $T_{\rm ambient}$ was set to the level of instantaneous freezing of $-40\,^{\circ}{\rm C}$ in order to minimise the perturbation of measurements by erroneously sampled liquid water droplets in warm clouds.

Finally, flight sequences of the Learjet 35A with steep ascents and descents were excluded, since these flight conditions are not comparable to conditions aboard long-haul passenger aircraft. To obtain information about the MCH performance relevant for the MOZAIC data set, i.e. for nearly constant flight levels with moderately slow changes in temperature and humidity, the flight altitude for CIRRUS-III was smoothed over 90 s time intervals, and when altitude changes exceeded $\Delta z > 6$ m in 5 s the respective data points were excluded from the intercomparison. These filtering operations lead to a data set with MOZAIC typically operational conditions with a remaining fraction of about 36 % of campaign data (see Table 3 for more details).

The correlation between MCH and reference RH_{liquid} data and RH_{ice} data from FISH (clear sky) and OJSTER (incirrus) is shown in Fig. 8. The scatter plots for the 1 Hz data sets reduced to MOZAIC-relevant conditions (hereafter referred to as "reduced data set") show similar scattering around the line of unity. Linear regression analysis confirms this with similar results for both cases: a correlation coefficient of $R^2=0.92$ with a slope of virtually unity. The offset for the RH_{liquid} regression is 0.18 ± 0.09 % RH_{liquid} , and for the RH_{ice} regression it is 0.36 ± 0.15 % RH_{ice} .

A more statistically based view on the data set is shown in Fig. 9, where the correlation between the sensors averaged for 5 % RH_{liquid} bins is shown. The MCH agrees very

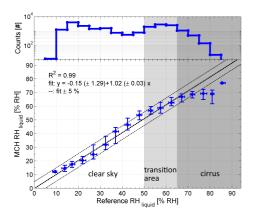


Figure 9. Correlation of RH_{liquid} data from MCH and the reference, i.e. FISH (clear sky) and OJSTER (in-cirrus), during CIRRUS-III; the straight line indicates the linear regression line, while the dashed lines illustrate the sensor uncertainty range $\pm 5\,\%$ RH_{liquid}. In the transition area both reference instruments can occur (see Fig. 8). The top panel shows the number of data points per $5\,\%$ RH_{liquid} bin.

well with the reference instruments over the entire range of values measured in the cloud-free atmosphere. Inside cirrus clouds, i.e. $RH_{liquid} > ca$. 70%, the sensors deviate as expected as a result of the increased response time of the MCH. Small-scale supersaturations are smoothed out, while OJSTER can detect these with response time of ca. 1 s. Linear regression analysis weighted with the number of occurrences provides a correlation coefficient of $R^2 = 0.99$ with an offset of -0.15 ± 1.29 % RH_{liquid} and a slope of 1.02 ± 0.03 . Median values and almost all of the 25th and 75th percentiles fall within the ± 5 % RH_{liquid} range around the linear regression line, which confirms the previously determined MCH uncertainty of 5% RH_{liquid} (see also Table 4).

For a better understanding of an uncertainty of 5% RH_{liquid}, Fig. 10 shows water vapour VMR as a function of temperature for 5% and 10% RH_{liquid} for pressure levels at typical passenger aircraft flight altitudes. As an example, at $T_{\rm ambient} = 215$ K and pressure = 220 hPa, a mea-

Table 3. Fraction of remaining data after filtering the data set of MOZAIC atypically operational conditions.

Method	Remaining data	Fraction of remaining data
No filter	62 207	100 %
$T_{\mathrm{ambient}} < -40^{\circ}\mathrm{C}$	35 650	57 %
$T_{\rm sensor} > -40^{\circ}{\rm C}$	31 331	50 %
W/o ascent/descent	26 234	42 %
All	22 184	36 %

sured RH_{liquid} = 5 % with an uncertainty of 5 % RH_{liquid} corresponds to a VMR of ca. 5 ± 5 ppmv.

The consistency of the MCH RH_{liquid} data is shown in Fig. 11. The probability distribution functions (PDFs) for RH_{liquid} derived from MCH data agree very well with those derived from the reference for the entire data set. Larger deviations at higher values of RH_{liquid} , e.g. at possible cirrus cloud edges, reflect the fact of the longer response time of the MCH. The sensor behaviour for those conditions at the limit of the sensor operation specifications is analysed in detail in the following section.

4.2 Limits of MCH operation

The comparison between the MCH RH_{liquid} data and the reference RH_{liquid} data, i.e. OJSTER data in cloud or otherwise FISH data, during the CIRRUS-III field study shows a remarkably good agreement for the reduced data set. However, the performance of the MCH sensor in conditions at its limits of operation, e.g. close to the lower calibration limit of $T_{\rm sensor} = -40\,^{\circ}{\rm C}$ or during strong humidity changes, has to be analysed in detail in order to assess the sensor's operation range. For this purpose, the time series of flight 2 is revisited in Fig. 5, where the individual RH_{liquid} time series, the difference of both RH_{liquid} time series and the $T_{\rm ambient}$ as well as the $T_{\rm sensor}$ time series are applied.

The following three sequences of interest have to be analysed:

Sequence 1 lasts from 08:40 to 09:10 UTC, when the MCH still shows a good response at higher sensor temperatures of about -20 °C and agrees within 5-10 % RH_{liquid} with the reference. However, at decreasing sensor temperature, the response time of the MCH increases significantly. This results in a delay causing higher humidity values and greater differences in the comparison with the reference. Because of the dominating van der Waals forces the adsorption of new water molecules by the dielectric membrane of the sensor occurs faster than desorption. For that, the response to positive humidity gradient is faster than to negative gradient, which can be seen in the behaviour of the RH_{liquid} differences in time.

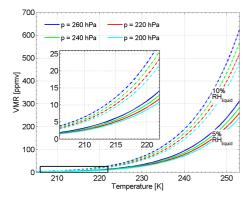


Figure 10. Water vapour volume mixing ratio (VMR) as a function of ambient temperature for 5 % (solid lines) and 10 % RH_{liquid} (dashed lines), respectively. The different pressure levels represent typical passenger aircraft flight altitudes. The inner box shows a zoom of the lower temperature and VMR values.

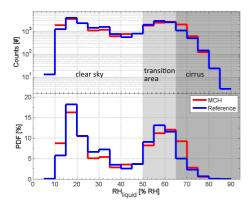


Figure 11. Number of data points (top panel) and frequency of occurrence (bottom panel) for observations of RH_{liquid} during CIRRUS-III; blue and red lines refer to data from reference, i.e. FISH (clear sky) and OJSTER (in-cirrus), and MCH, respectively. The number of counts of both data sets agrees in almost all 5 % RH_{liquid} bins. The exponential decline at higher values is in accordance with the result of Spichtinger et al. (2003). A bimodal distribution can be seen clearly in the probability density function (PDF) view of the data sets, where there is a clear-sky section at lower values and a cirrus section at higher values. The differences in the PDF can be mainly explained by the longer response time of the MCH into and out of the clouds.

- Sequence 2 illustrates a strong humidity change between 09:40 and 10:00 UTC, while flying through a cirrus cloud. Because of slower MCH sensor response at colder sensor temperatures, the MCH RH_{liquid} values can not follow the rapid changes in RH_{liquid} as observed by the reference.
- Sequence 3 refers to a section of the flight between 11:00 and 11:40 UTC, when $T_{\rm sensor}$ reaches values below the sensor calibration limit of $T_{\rm sensor} = -40 \,^{\circ}\text{C}$, i.e. ambient temperatures below $-70 \,^{\circ}\text{C}$ at commercial air-

RH bin	0-5 %	5-10 %	10-15 %	15-20 %	20–25 %	25-30 %	30–35 %	35–40 %	40–45 %
ΔRH _{liquid}	_	$3.0^{+0.2}_{-0.4}$	$1.0^{+1.6}_{-1.1}$	$0.4^{+2.2}_{-2.9}$	$-1.8^{+2.4}_{-2.7}$	$-2.3^{+5.5}_{-2.8}$	$-0.1^{+5.2}_{-4.4}$	$3.7^{+3.4}_{-7.3}$	$3.9^{+4.2}_{-2.9}$
Counts [#]	_	13	1276	4037	2335	1471	1606	776	569
RH bin	45–50 %	50-55 %	55-60 %	60–65 %	65–70 %	70–75 %	75–80 %	80–85 %	85–90 %
ΔRH _{liquid} [% RH]	$5.4^{+3.5}_{-3.1}$	$4.2^{+2.6}_{-2.9}$	$1.7^{+3.8}_{-4.2}$	$0.4^{+3.7}_{-2.8}$	$-0.8^{+2.7}_{-3.3}$	$-3.3^{+2.9}_{-2.8}$	$-7.7^{+3.8}_{-4.0}$	$-12.3^{+3.8}_{-7.1}$	$-8.9^{+0.8}_{-0.8}$
Counts [#]	813	2015	2910	2567	1109	512	148	24	3

Table 4. Median, 25th/75th percentile values and counts of ΔRH_{liquid} (MCH and reference). Data were classified into 5 % RH_{liquid} bins relating to the reference, i.e. OJSTER data in cloud or otherwise FISH data.

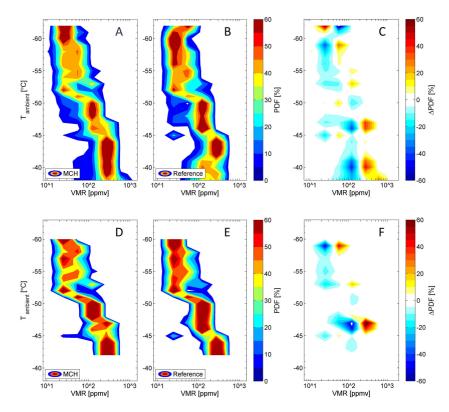


Figure 12. Probability density functions (PDFs) of the complete $(\mathbf{a}-\mathbf{c})$ and reduced $(\mathbf{d}-\mathbf{f})$ MCH (\mathbf{a},\mathbf{d}) and reference (\mathbf{b},\mathbf{e}) , i.e. FISH (clear sky) and OJSTER (in-cirrus), water vapour volume mixing ratio (VMR) data related to the ambient temperature T_{ambient} . Water vapour volume mixing ratio is binned in the logarithmic space between 0 and 8.8, with a bin size of 0.8 and temperature in 1 °C bins. (\mathbf{c}) and (\mathbf{f}) show the difference of the MCH and reference PDFs for the complete and reduced data set, respectively.

craft speed of M = 0.81. The MCH shows an increased response time and a loss of signal fine structure, and increasing deviations between the MCH and the reference instruments occur.

Despite delayed sensor response for conditions at the limit of its operation range, the MCH shows a very good overall performance during the CIRRUS-III field study. Figure 12 illustrates the PDFs of water vapour VMR data as a function of $T_{\rm ambient}$ (panels a to c for the complete data set and panels d to f for the reduced data set) according to Kunz et al.

(2008). The frequencies of occurrence are calculated in 1 °C bins for the MCH data set (panels a and d), the reference data set (panels b and e) and the deviation of the MCH and reference PDFs for the complete and reduced data set (panel c and f). The water vapour VMR is binned in the logarithmic space between 0.0 and 8.0 with a bin size of 0.8. The colour bars are binned in 5 % spaces for a better interpretation of the contour plots.

The MCH seems to remain at dryer values for the coldest temperatures of $T_{\text{ambient}} \cong -60 \,^{\circ}\text{C}$, which is again a result of

the delayed sensor response at sensor temperatures below the calibration limit. Further, small deviations at lower temperatures are also observed. In summary, data sets for both cases show a similar behaviour in the water vapour VMR distribution with only small deviations; these deviations have no statistically significant relevance.

5 Conclusions and recommendations

The CIRRUS-III (2006) aircraft campaign provided a data set for the evaluation of the MOZAIC Capacitive Hygrometer in a blind intercomparison with high-performance water vapour instruments based on tunable diode laser absorption spectrometry (OJSTER, in-cloud reference) and Lyman- α fluorescence detection (FISH, clear-sky reference).

Except for conditions at its operation limit (e.g. $T_{\rm sensor} < -40\,^{\circ}{\rm C}$ and during rapid changes in RH_{liquid}), the MCH performs with a difference of 10 % RH_{liquid} or less to the references.

In order to obtain a representative result for the MCH's uncertainty for its regular deployment aboard passenger aircraft, the data set was restricted to conditions corresponding to regular sensor operation aboard MOZAIC aircraft: data with sensor temperatures below $-40\,^{\circ}\text{C}$ were excluded due to the calibration limit. In MOZAIC less than 1% of RH observations are made at sensor temperatures colder than $-40\,^{\circ}\text{C}$. Strong ascent and descent sequences of the aircraft were removed, and the maximum T_{ambient} was set to $-40\,^{\circ}\text{C}$ to exclude effects of warm clouds.

The 1 Hz correlation yielded a robust linear fit with a slope of unity, with no statistically significant offset and a correlation coefficient of $R^2 = 0.92$, which was confirmed by the correlation of the binned RH_{liquid} data. The RH_{liquid} data grouped in 5 % RH_{liquid} bins agree very well for the MCH and reference instruments over the entire cloud-free range and for most of the cirrus cloud sequences, and they yield a MCH uncertainty of 5 % RH_{liquid}.

Comparing the MCH's and references' PDFs for RH_{liquid} shows no statistically significant effect of delayed sensor response at conditions beyond the operation range. Neither strong humidity changes nor operation at the lower calibration limits causes considerable sensor failures. The main limitation for the use of MCH RH_{liquid} data is related to sensor temperatures below the calibration limit of $T_{\rm sensor} = -40\,^{\circ}{\rm C}$. However, these temperatures are encountered only rarely in the MOZAIC programme as long as the flight routes do not reach polar air masses with ambient temperatures below $-70\,^{\circ}{\rm C}$. In summary, the MCH is highly suitable for climatology analyses in the MOZAIC programme even if the sensor is not applicable to high-time-resolution measurements.

A value for the limit of detection is not appropriate for the MCH, but the variable to describe its performance is the here determined uncertainty of the RH_{liquid} measurements. RH_{liquid} measurements below 5 %, which are common in the

lowermost stratosphere, have to be used carefully because these data are close to the sensor uncertainty range, which, as shown before in Sect. 4.1, results in a relative deviation of 100 %.

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