

# Insights into the dielectric response of ferroelectric relaxors from statistical modeling

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Ferroelectric relaxors are complex materials with distinct properties. The understanding of their dielectric susceptibility, which strongly depends on both temperature and probing frequency, has been a challenge for researchers for many years. Here we report a macroscopic and phenomenological approach based on statistical modeling to investigate how the dielectric response of a relaxor depends on temperature. Employing the Maxwell-Boltzmann distribution and considering temperature-dependent dipolar orientational polarizability, we propose a minimum statistical model and specific equations to understand and fit numerical and experimental dielectric responses versus temperature. We show that the proposed formula can successfully fit the dielectric response of typical relaxors, including  $\text{Ba}(\text{Zr,Ti})\text{O}_3$ ,  $0.87\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - $0.13\text{PbTiO}_3$ ,  $0.95\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - $0.05\text{Pb}(\text{Zr}_{0.53}\text{Ti}_{0.47})\text{O}_3$ , and Bi-based compounds, which demonstrates the general applicability of this approach.

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## I. INTRODUCTION

Relaxor ferroelectrics are materials that exhibit interesting dielectric responses different from normal ferroelectrics. For instance, they often possess relaxation modes at low frequencies ( $< 1$  GHz). Relaxor ferroelectrics have been exploited in many applications, such as actuators due to their giant electromechanical couplings [1,2], and their properties have extensively been investigated, including structural properties [e.g., polar nanoregions (PNRs)] using neutron scattering [3], dielectric responses [4–9], the crossover from ferroelectrics to relaxors [9]. To understand such systems, many theories have been proposed [3,10–16]. Relaxors are complex systems, to some extent similar to spin glasses [13,14,17], in that their compositions are, without exception, made of complex oxides containing different ions and inevitably inhomogeneous. For instance, the B-site ions of typical relaxors  $\text{Ba}(\text{Zr,Ti})\text{O}_3$  (BZT) and  $\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$  (PMN) are distributed randomly.

The dielectric response of ferroelectric relaxors is the defining feature that differentiates them from normal ferroelectrics: (i) large susceptibilities at low frequencies (gigahertz or lower); (ii) even more unusual, the characteristic temperature  $T_m$  at which the susceptibility peaks strongly depends on the frequency of the probing ac electric field. In other words, the susceptibility  $\chi$  depends on both temperature  $T$  and probing frequency  $\nu$ . Although such phenomena are well

known experimentally [11,18–23], numerical generation of the relaxor's dielectric response from model-based simulations has been challenging work. For instance, the shift of  $T_m$  of the lead-free relaxor BZT was only numerically simulated recently [6]. Since numerous ferroelectric relaxors exist, numerically treating each of them remains a daunting task. One way to mitigate this difficulty is to resort to statistical modeling [24]. For a complex system, a statistical approach can provide intuitive understanding by capturing dominant factors, derive equations to understand experimental results, and help extracting useful information. In the present paper, we adopt this approach to treat the dielectric response of relaxors and show that such a statistical model can indeed be applied to understand how the dielectric constants change with temperatures and probing frequencies.

Whereas the susceptibility of relaxors  $\chi(T, \nu)$  depends on both temperature and frequency, theoretical models often are proposed to treat  $\nu$  and  $T$  separately [7,10,11,25–27]. For instance, at a given temperature, two processes are employed in the fitting of  $\chi(\nu)$  of  $\text{Ba}(\text{Ti}_{0.675}\text{Zr}_{0.325})\text{O}_3$  [18,22]: The universal relaxor process and the conventional relaxor process, which have different relaxation characteristics employing the Curie–von Schweidler law at low frequencies and the Kohlrausch–Williams–Watts law at higher frequencies [18]. Other formulas, such as the Cole-Cole and the Havriliak-Negami equations, also are employed to model the dielectric response with respect to frequency at given temperatures. When phonon modes are close to or interacting with the relaxation modes, it becomes necessary to use coupled modes

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to model the dielectric response [5,6]. On the other hand, there are also many investigations on how the dielectric response  $\chi$  depends on the temperature  $T$  at given frequencies. In addition to the well-known Curie law for  $\chi(T)$  at high temperatures, the most useful equation for fitting around the dielectric peak appears to be the square law. In particular, the formula,

$$\frac{1}{\varepsilon(T)} = \frac{1}{\varepsilon_A} + \frac{(T - T_A)^\eta}{B} \quad (1)$$

was proposed to describe the permittivity at  $T > T_m$  [28,29]. Initially,  $\eta$  was found to be 2, but later was shown to be between 1 and 2 [4,11,30–32]. Here, we further the investigation in this direction and attempt to address some important questions regarding relaxor behaviors. We will explain why the dielectric constant has a peak value at  $T_m$  and what causes the asymmetry around the peak. Moreover, by constructing a statistical model that properly describes how dipoles behave in relaxors, we propose a formula to fit experimental results, which further illuminates the physics behind relaxation behavior.

This paper is organized as follows. In Sec. II, we introduce the statistical model. In Sec. III, we apply this model to both lead-free and lead-based relaxors. In Sec. IV, we discuss the implication and limitation of this approach. Finally, in Sec. V, we present a brief conclusion.

## II. STATISTICAL MODEL

The statistical model starts by considering a critical difference between ferroelectric relaxors and normal ferroelectrics. One crucial observation is that all relaxor ferroelectrics discovered so far are inevitably disordered and inhomogeneous systems. For instance, in BZT, Zr and Ti ions are distributed randomly, so are the Mg and Nb ions in PMN when the samples are treated macroscopically. In addition, PMN possesses an electric field arising from heterovalent  $\text{Mg}^{2+}$  and  $\text{Nb}^{5+}$  ions, which affects dipole distribution. It is important to further note that well-known relaxors can become nonrelaxors if their ions are ordered perfectly [33–35].

### A. Individual dipoles

The randomness of ions and the ensuing lack of long-range ordering has the important consequence that phonon modes may not be the best description for understanding relaxors. This fact is evidenced by the effective Hamiltonian that describes the BZT relaxor [12–14],

$$E = \sum_i (\kappa_i |u_i|^2 + \lambda_i |u_i|^4) + \dots, \quad (2)$$

where  $i$  labels the sites occupied randomly by Zr or Ti and  $\kappa_i$  ( $\lambda_i$ ) are the second- (fourth-) order coefficients in the Taylor expansion of energy with respect to  $\mathbf{u}_i$ , which is the local dipole on site  $i$ . For a homogeneous system, where  $\kappa_i$  and  $\lambda_i$  are constants, we can usually first consider the harmonic term and construct phonon modes, which are then used to describe the system, especially in low temperatures when the system condenses to particular phonon modes [36]. In contrast, with the loss of periodicity in relaxors, this approach is no longer profitable. One can insist on using averaged atoms (e.g., replacing Zr and Ti atoms with their average in BZT) to

retain the use of phonon modes. However, it is then necessary to consider defect-pinned intrinsic localized modes [37] and phonon localization [3].

The inhomogeneity also has important consequences on ferroelectric phase transitions. In the typical ferroelectric material  $\text{BaTiO}_3$ , we may ascribe the temperature-driven phase transition to the condensation of phonons to a particular phonon mode [36]. At high temperatures, many phonon modes are occupied; at low temperatures, due to mode softening, a certain mode (often corresponding to the well-known soft mode [38–40] in perovskites) has essentially zero energy, which dominates the system and induces phase transitions. Unlike  $\text{BaTiO}_3$ , there is no global phase transition due to the existence of PNRs and/or random electric fields, which eliminates the mode softening phenomenon and renders a global dipole order difficult to achieve [12,41]. In addition, relaxors exhibit strange phonon behavior, such as the “water-fall” effect [42–44] and the localization [3], further showing their differences from normal ferroelectrics. In this paper, we focus on individual dipoles and statistically model their dielectric responses. This change in view implies that phonon modes are less important in our analysis. We will show in the following that such consideration leads to fruitful results and better understanding of relaxors.

### B. Statistics of individual dipoles

Individual dipoles can be categorized into different groups based on their dynamics, and each group will have different contributions to susceptibility. We proceed by summarizing various interactions between dipoles and assuming such interactions effectively introduce a potential well of *average* depth  $E_b$ . We may relate  $E_b$  to the size of PNRs arising from the clustering of the same-type ions [12] and/or random electric field caused by heterovalent ions [41,42,45].

Since the kinetic energy of individual dipoles obeys the Maxwell-Boltzmann distribution, at temperature  $T$ , the number of dipoles with kinetic energy  $E_{\text{kin}}$  is given by

$$f(E_{\text{kin}}) = 2N \sqrt{\frac{E_{\text{kin}}}{\pi}} \left( \frac{1}{k_B T} \right)^{3/2} \exp\left(-\frac{E_{\text{kin}}}{k_B T}\right), \quad (3)$$

where  $k_B$  is the Boltzmann constant,  $N$  is the total number of dipoles, and  $f(E_{\text{kin}})dE_{\text{kin}}$  is the number of dipoles having a kinetic energy between  $E_{\text{kin}}$  and  $E_{\text{kin}} + dE_{\text{kin}}$ . With this distribution function, we can calculate the number of dipoles with kinetic energy that exceeds the potential well  $E_b$ , which is given by

$$\begin{aligned} N_1(E_b, T) &= \int_{E_b}^{\infty} dE_{\text{kin}} f(E_{\text{kin}}) \\ &= N \sqrt{\frac{4}{\pi}} \sqrt{\frac{E_b}{k_B T}} \exp\left(-\frac{E_b}{k_B T}\right) + N \operatorname{erfc}\left(\sqrt{\frac{E_b}{k_B T}}\right), \end{aligned} \quad (4)$$

here  $\operatorname{erfc}$  is the complementary error function. The number of dipoles confined to the potential well then is given by

$$N_2(E_b, T) = N - N_1(E_b, T). \quad (5)$$

The next step is to treat the two sets of dipoles ( $N_1$  versus  $N_2$ ) separately, assigning different susceptibilities to them. The total susceptibility then is given by

$$\chi(T, \nu) = \chi_1(T, \nu)P_1(E_b, T) + \chi_2(T, \nu)P_2(E_b, T), \quad (6)$$

where  $\chi_1(T, \nu)$  and  $\chi_2(T, \nu)$  describe the dielectric responses of each dipole group, whose form will be specified later. We also define

$$P_1(E_b, T) \equiv \frac{1}{N} N_1(E_b, T),$$

$$P_2(E_b, T) \equiv \frac{1}{N} N_2(E_b, T)$$

to normalize the dipoles to unit volume. Equation (6) is the centerpiece of this paper and will be demonstrated to be useful for the investigation of relaxors in general.

### III. RESULTS

We apply Eq. (6) to fit various  $\chi$ 's versus  $T$ 's obtained experimentally or numerically. The relaxors studied here include both lead-based (e.g., PMN) and lead-free relaxors (e.g., BZT).

#### A. Susceptibility of BZT

For the static susceptibility of the lead-free relaxor BZT [6,8,22,46], we assume: (i) dipoles with kinetic energy that overcomes the potential well can be treated as free dipoles, subject only to thermal excitation; (ii) dipoles inside the potential well only contribute a constant susceptibility  $\chi_2$ . The total susceptibility thus is given by

$$\chi(T) = \chi_1 \mathcal{L}\left(\frac{\theta}{T}\right) P_1(E_b, T) + \chi_2 P_2(E_b, T), \quad (7)$$

where  $\mathcal{L}(x) = \coth(x) - 1/x$  is the Langevin function, known for depicting orientational polarization under thermal fluctuations [47,48] and  $E_b$ ,  $\chi_1$ ,  $\chi_2$ , and  $\theta$  are constants which will be determined by fitting experimental or numerical data. It can be inferred from Eq. (7) that  $\chi_2$  is the susceptibility of the material at zero Kelvin,  $\chi_1 \mathcal{L}(\frac{\theta}{T})$  is essentially the Curie law at high temperatures, and  $\theta$  is proportional to the magnitude of the low-frequency electric field used in experimental measurements.

We first test Eq. (7) against the static susceptibility versus temperature obtained with the Monte Carlo (MC) simulation in a previous work [12]. Figure 1 shows that the overall fitting is good enough to reproduce results from MC simulations with the parameters shown in Table I. The closeness of  $E_b$  and  $T_m$  indicates the average depth of the potential wells plays a dominant role in determining  $T_m$ . Close examination of Fig. 1 also reveals that the fitting at the lowest temperature ( $\lesssim 25$  K) is not as good as the rest. To address this issue, we added a Gaussian distribution to  $E_b$  to remedy this minor problem. However, the resulting equation is quite complicated and deviates from our original goal of proposing a simple analytical formula to fit susceptibility. Therefore this additional step is not adopted here.

In order to have a good understanding of BZT's susceptibility, we show each component of Eq. (7) in Fig. 2. Figure 2(a)

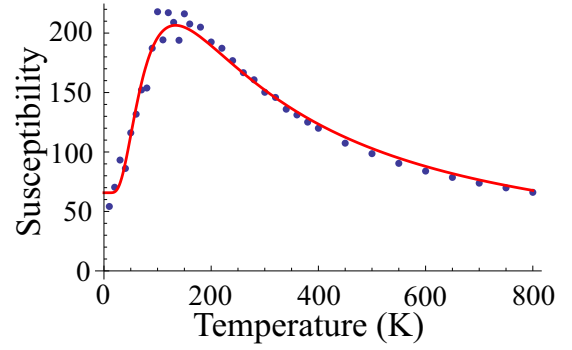


FIG. 1. Fitting the static susceptibility of  $\text{Ba}(\text{Zr}_{0.5}\text{Ti}_{0.5})\text{O}_3$  obtained from the Monte Carlo simulation using Eq. (7). The blue dots are from the Monte Carlo simulation [12], and the red solid line is the fitting curve using Eq. (7).

shows that  $P_1(E_b, T)$  and  $P_2(E_b, T)$  have opposite trends as the temperature increases. The number of dipoles that can overcome the potential confinement ( $P_1$ ) steadily increases with temperature, whereas the number of dipoles inside ( $P_2$ ) continuously becomes smaller. Figure 2(b) shows that the Langevin function is normalized at  $T = 0$  and decreases with temperature. Such a feature describes the ability of the free dipoles to respond to an external dc electric field. Moreover, Fig. 2(b) also shows the product of the Langevin function and  $P_1$ , which already exhibits some resemblance to the BZT's susceptibility [Fig. (1)].

Having examined the static susceptibility, we now move to the frequency-dependent dielectric response, which often is taken as a characteristic property of the relaxors [9,49]. We propose another equation to fit the susceptibility versus temperature,

$$\chi(T) = \frac{\chi_1}{1 + b \exp(-\theta/T)} P_1(E_b, T) + \chi_2 P_2(E_b, T), \quad (8)$$

where  $\chi_1$ ,  $\chi_2$ ,  $b$ , and  $\theta$  are constants at a given frequency (but may change when the frequency changes). The dielectric contribution from dipoles with kinetic energies higher than the potential well is given by

$$w_1(T) = \frac{1}{1 + b \exp(-\theta/T)}, \quad (9)$$

which, similar to the Langevin function, monotonically decreases with temperature  $T$ . The choice of this function reflects two considerations: (i) at very low temperatures ( $T$  close to 0), such dipoles will follow the probing ac electric field closely, leading  $w_1(T)$  to its maximum; and (ii) at higher temperatures, thermal motions of these dipoles hamper their ability to follow the ac electric field, leading to smaller  $w_1(T)$ . We will discuss this equation further in Sec. IV. With one more parameter ( $b$ ), this function may be taken as an extension to the Langevin function. We note that Eq. (7) can

TABLE I. Fitting parameters of various materials for Eq. (11)

	$\chi_1$	$\theta$ (K)	$\chi_2$	$E_b$ (K)
Values	741.6	220.5	64.7	159.1

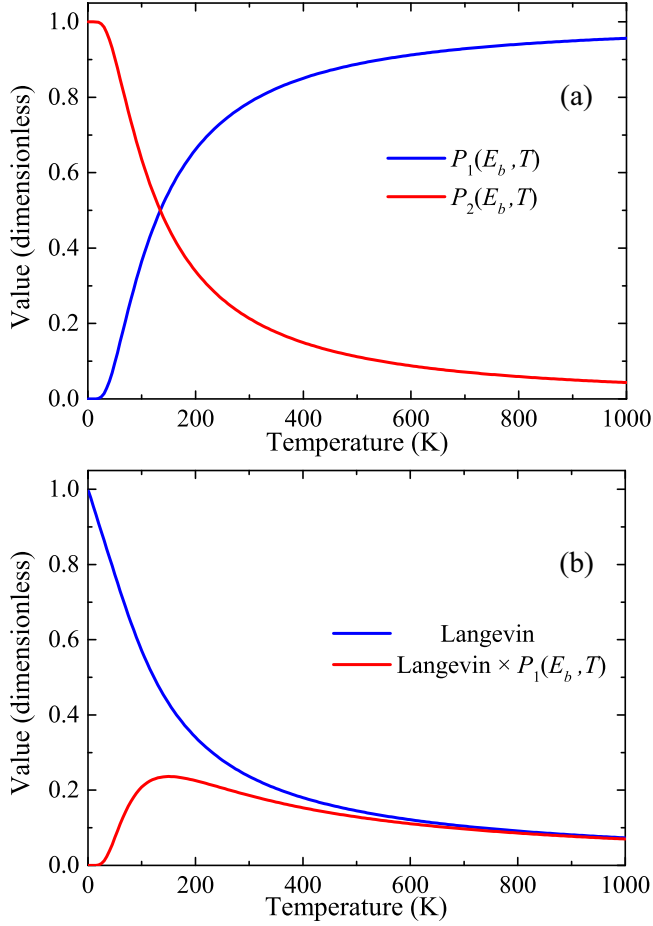


FIG. 2. The Maxwell-Boltzmann distribution [panel (a)] and the Langevin function  $\mathcal{L}$  [panel (b)] versus temperature. The parameters from Table I are used to plot each function.

no longer be used because the Langevin function is derived under the equilibrium condition of dipoles, whereas dipoles under ac electric fields are never in true equilibrium, therefore invalidating the use of the Langevin function.

We use Eq. (8) to fit BZT's susceptibility versus temperature at different frequencies and show the results in Fig. 3. Since  $E_b$  is a material parameter, we use the same value ( $E_b = 159.1$  K) obtained by fitting the static susceptibility (cf. Fig. 1). In Fig. 3, the numerical results are obtained from the MD simulations reported in Ref. [6]. As the figure shows, satisfactory fittings are achieved for frequencies between 1 and 1000 GHz. Table II shows all the parameters. Among them,  $\theta_1$  and  $\chi_1$  change substantially over the specified frequency range as shown in

TABLE II. Fitting parameters of numerically simulated  $\text{Ba}(\text{Zr}_{0.5}\text{Ti}_{0.5})\text{O}_3$  susceptibility at various frequencies [6] using Eq. (8).

	1 GHz	10 GHz	100 GHz	1000 GHz
$\theta$ (K)	579.6	762.6	1128.4	2158
$\chi_1$	406.5	312.6	209.3	99.9
$\chi_2$	73.1	63.5	56.2	57.9
$b$	10.2	9.9	9.5	7.7

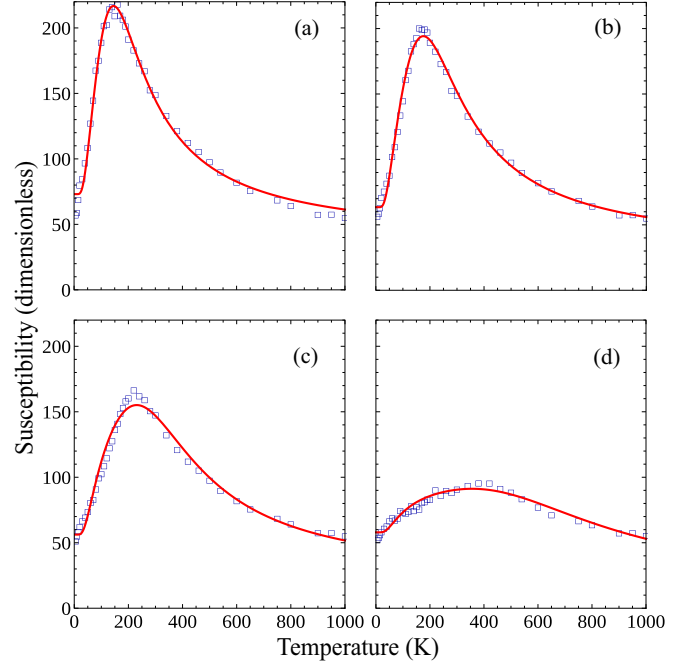


FIG. 3. Fitting of the susceptibility of  $\text{Ba}(\text{Zr}_{0.5}\text{Ti}_{0.5})\text{O}_3$  at  $f = 1, 10, 100, 1000$  GHz, obtained from molecular dynamics (MD) simulation using Eq. (8).

Fig. 4, where  $\theta$  depends on  $\ln(f)$  quadratically, whereas  $\chi_1$  linearly depends on it [50].

To further verify the suitability of this equation for experimental data, we also fit the result shown in Fig. 1 of Ref. [18] where  $\text{Ba}(\text{Ti}_{0.675}\text{Zr}_{0.325})\text{O}_3$  ceramics is measured at  $10^{-2}$  and  $10^5$  Hz. Figure 5 shows that satisfactory fittings are achieved.

### B. Pb-based relaxors

Unlike lead-free BZT, which possesses PNRs that are separated by Zr-rich regions, lead-based ferroelectrics

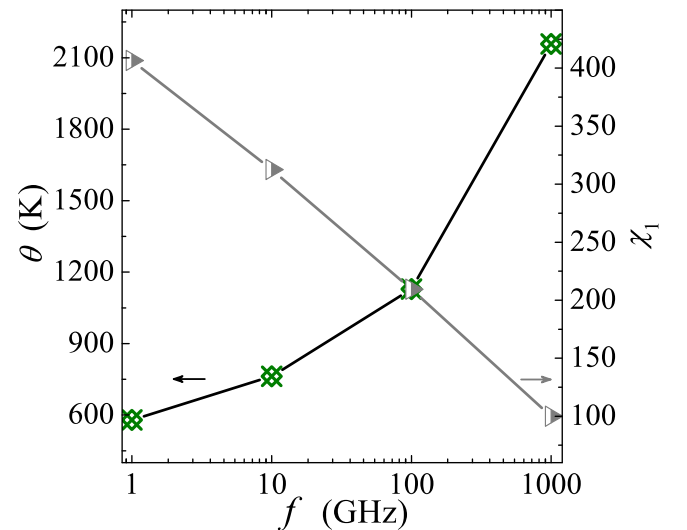


FIG. 4. Analysis of fitting parameters versus probing frequency.  $\theta$  versus  $\ln(f)$  and  $\chi_1$  versus  $\ln(f)$ .



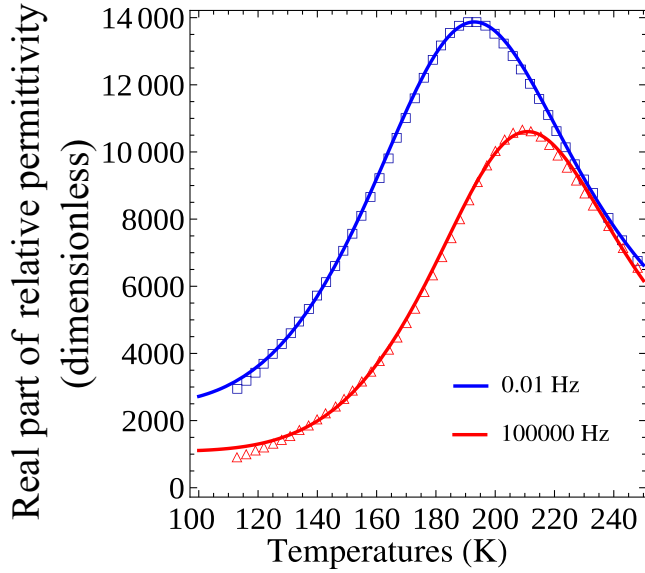


FIG. 5. Experimental susceptibility of  $\text{Ba}(\text{Ti}_{0.675}\text{Zr}_{0.325})\text{O}_3$  ceramics versus temperature fitted with Eq. (8).

[19,29,41,51] have the Pb-driven dipoles across the system [52], which cause phase transitions in systems, such as  $\text{PbTiO}_3$  and  $\text{Pb}(\text{Zr},\text{Ti})\text{O}_3$  [53–55]. Due to heterovalent ions inside, typical lead-based relaxors are subject to random electric fields, which distort the orientation of dipoles. Although the precise consequence of the random field is not all clear [14,15], such a distracting effect on dipoles appears to lead to a strongly modified phase transition with diffuse and smeared susceptibility peaks, in sharp contrast to that of normal ferroelectrics [41,56].

To model such a system and account for the moderate phase transition, we need a function that properly describes the dielectric constant versus temperature. Here, we propose to use the slightly modified well-known quadratic relation  $\frac{\epsilon_A}{\epsilon'} - 1 = \frac{(T-T_A)^2}{2\delta^2}$  proposed by Bokov and Ye [4] to relate the relaxor's permittivity to temperature [28,29] for dipoles above the average potential well [also see Eq. (1)]. This equation can be rearranged to give the following expression:

$$w_2(T) = \frac{1}{1 + \left| \frac{T-T_O}{\theta} \right|^\gamma}, \quad (10)$$

where  $\gamma$  is a critical exponent,  $T_O$  is associated with the peak position of the moderate phase transition, and  $\theta$  is a parameter describing the width of the peak. We note that, compared to  $\frac{\epsilon_A}{\epsilon'} - 1 = \frac{(T-T_A)^2}{2\delta^2}$ , we have used  $T_O$  instead of  $T_A$ ,  $\theta$  instead of  $\sqrt{2}\delta$ , and a general critical exponent  $\gamma$  instead of the fixed number 2. Appendix A provides a further discussion of this formula. We also note that such a choice of  $w_2(T)$  also agrees with the analysis recently given by Uchino [10], who provides a possible physical interpretation for this formula. Combining Eqs. (6) and (10), we obtain the following equation to fit lead-based relaxors:

$$\chi(T) = \frac{\chi_1}{1 + \left| \frac{T-T_O}{\theta} \right|^\gamma} P_1(E_b, T) + \chi_2 P_2(E_b, T), \quad (11)$$

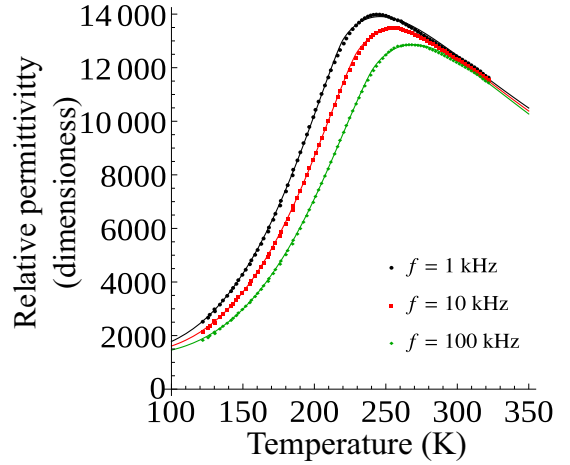


FIG. 6. Fitting the relative permittivity of PZN-0.13PT at  $f = 1, 10, 100$  kHz using Eq. (11).

where  $E_b$ ,  $\chi_1$ ,  $\chi_2$ ,  $T_O$ ,  $\theta$ , and  $\gamma$  are fitting parameters. The meaning of  $\chi_1$ ,  $\chi_2$ , and  $E_b$  are the same as discussed in Sec. III A.

Two considerations motivate the adoption of Eq. (11): (i) Pb-based relaxors usually have Pb-driven dipoles that exist across the system unlike BZT where dipole clusters (PNRs) are separated by Zr-rich regions; (ii) as a consequence of (i), despite strong random electric fields, there could be a global phase transition which exhibits temperature dependence following Eq. (10) [10].

To verify that Eq. (11) indeed works, we experimentally obtained the permittivity of  $0.87\text{Pb}(\text{Zn}_{1/3}\text{Nb}_{2/3})\text{O}_3$ -0.13 $\text{PbTiO}_3$  (PZN-0.13PT) [57,58] versus temperature at frequencies of  $f = 1, 10$  and  $100$  kHz [59]. As Fig. 6 shows, all three fittings are satisfactory. We note that in this fitting there is no need to have two  $\gamma$  values above and below  $T_O$  [10]. The asymmetric peak shown in Fig. 6 naturally is caused by the Maxwell-Boltzmann distribution function.

Table III summarizes the fitting parameters of the permittivity measured at various frequencies. Among all the parameters, the critical component  $\gamma$  changes the most (by 19.3% from 1 to 100 kHz) and decreases with increasing frequency; similarly,  $T_O$  also changes by 9.5%. On the other hand,  $\chi_1$ ,  $\chi_2$ , and  $\theta$  are relatively constant, which are independent of the frequency, and may be taken as material parameters. Such results hint towards the following formula that describes the dependence

TABLE III. Fitting parameters of PZN-0.13PT's permittivity measured at different frequencies. As the table demonstrates,  $\gamma$  and  $T_O$  are the most important variables that change a lot with frequency.

	1 kHz	10 kHz	100 kHz
$\gamma$	2.02	1.82	1.63
$T_O$ (K)	219.6	229.0	240.6
$E_b$ (K)	495.3	523.6	552.2
$\chi_1^a$	56601	55781	53529
$\chi_2$	1320.9	1284.2	1238.0
$\theta$ (K)	102.4	103.1	104.5

<sup>a</sup>Here,  $\chi_1$  and  $\chi_2$  are relative permittivity not susceptibility.

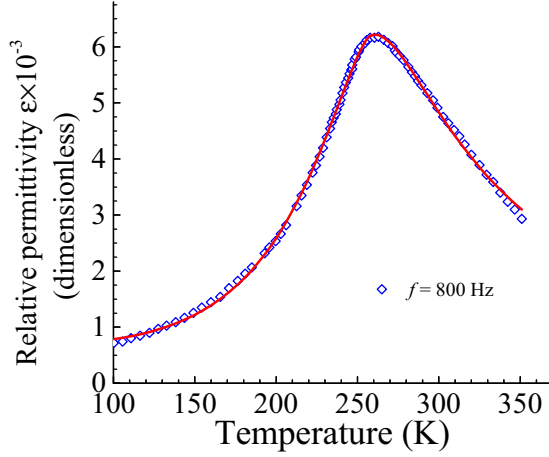


FIG. 7. Fitting of the relative permittivity of 0.95Pb(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub>-0.05Pb(Zr<sub>0.53</sub>Ti<sub>0.47</sub>)O<sub>3</sub> measured at 800 Hz using Eq. (11).

of PZN-0.13PT on both the temperature and the probing frequency:

$$\chi(T, \nu) = \frac{\chi_1}{1 + \left| \frac{T - T_O(\nu)}{\theta} \right|^{\gamma(\nu)}} P_1(E_b, T) + \chi_2 P_2(E_b, T), \quad (12)$$

where the two functions  $T_O(\nu)$  and  $\gamma(\nu)$  are frequency dependent whereas other parameters are constants for a given material. It is also worth noting that, for PZN-0.13PT  $\chi_2 \ll \chi_1$ , which indicates that the dipoles with kinetic energies above the potential well play a more important role, in contrast to the case of BZT (see Table II).

To further verify the proposed formula, we also fit the permittivity versus temperature of another lead-based relaxor 0.95Pb(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub>-0.05Pb(Zr<sub>0.53</sub>Ti<sub>0.47</sub>)O<sub>3</sub> [19]. It can be seen from Fig. 7 that the overall fitting is satisfactory with fitting parameters  $\gamma = 1.66$  and  $T_O = 256.7$  K. Similar to the PZN-0.13PT case, the results here also show  $\chi_2 \ll \chi_1$ .

#### IV. DISCUSSION

In the statistical model we divide the dipoles inside ferroelectrics relaxors into two groups, one group being confined in potential wells, whereas the other having overcome the potential confinement and exhibiting a more vibrant dynamics. It has been demonstrated that the Maxwell-Boltzmann distribution plays a significant role in determining the profile of  $\chi(T)$ . To address a particular type of relaxor, one only need to adjust the dielectric response function associated with each group of dipoles while keeping the rest unchanged. In this section, we discuss a few issues of this approach and its limitations.

##### A. Characteristic temperature $T_m$

The present analysis helps us to understand why the susceptibility of a relaxor reaches its peak value at some temperature  $T_m$ . For BZT, the function  $\chi_1 \mathcal{L}(\frac{\theta}{T})$  [see Eq. (7) and Fig. 2] or  $\chi_1/[1 + b \exp(-\theta/T)]$  [see Eq. (8)] describes the contribution to susceptibility from dipoles with kinetic

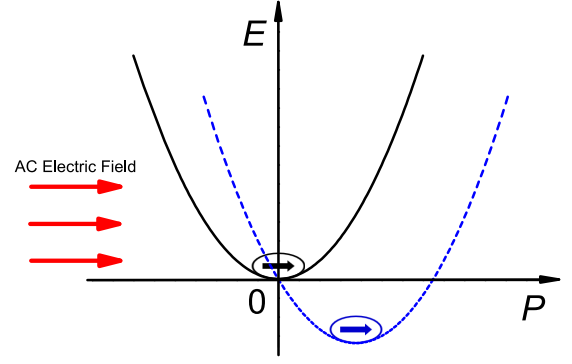


FIG. 8. The energy well for dipoles is shifted and lowered when an electric field is applied.

energies higher than  $E_b$ . These two functions are both monotonically decreasing with  $T$ , reflecting the fact that thermal motions prevent dipoles from aligning with the applied electric field. On the other hand, the number of dipoles above the potential wells increases with  $T$  as governed by the function  $P_1(E_b, T)$  (see Fig. 2). The combined effects of the two factors give rise to the susceptibility peak at  $T_m$ . However, the situation for lead-based relaxors is different. The function  $\chi_1/(1 + |\frac{T - T_O}{\theta}|^\gamma)$  [see Eq. (11)], which largely determines the value of  $T_m$ , manifests the vestige of a true phase transition in normal ferroelectrics, which is torn down by random electric fields and/or PNRs in the relaxors.

##### B. Rationale for Eq. (9)

For lead-free BZT, we propose Eq. (9) to describe the susceptibility of dipoles with kinetic energies higher than  $E_b$ . This choice follows the Debye relaxation, i.e.,  $\chi \sim 1/(1 + \omega^2 \tau^2)$  [47], where  $\omega$  is a constant (the probing frequency) and  $\tau$  is the temperature-dependent relaxation time. For a thermally activated process, the relation between  $\tau$  and  $T$  often is specified by the Arrhenius law, i.e.,  $1/\tau = A \exp(-E_a/T)$ , where  $E_a > 0$  is the activation energy [37, 56, 60]. In this case, the susceptibility will be  $\chi \sim 1/[1 + A^2 \omega^2 \exp(\frac{2E_a}{T})]$ , which is discussed by Jonscher [61]. However, the dynamic process considered here describes dipoles falling to a state of lower energy, which is created temporarily by the probing electric field (see. Fig. 8). Therefore the activation energy in this process will be *negative*, i.e.,  $\chi \sim 1/[1 + A^2 \omega^2 \exp(-\frac{2|E_a|}{T})]$ , which is the form adopted in Eq. (9).

We note that negative activation energy is known in some chemical reactions [60]. Negative activation energy appears here because when an ac electric field perturbs dipoles and tilts the relative energy of potential wells, the dipoles outside the potential wells will move towards the temporary potential minimum. However, the drifting to the potential minimum is hindered by thermal fluctuations of such dipoles. In fact, a higher temperature (corresponding to higher kinetic energy) results in a slower relaxation to the energy minimum (corresponding to larger  $\tau$ ), leading to negative activation energy. Furthermore, other interactions between dipoles (in particular short-range interaction) also may affect

this relaxation process and slow it down as temperature increases, giving rise to an apparent negative activation energy, whereas this is basically a zero-energy barrier process. We also note that, since the applied ac electric field is responsible for shifting the energy minimum and causing dipoles to drift, the change in its frequency may well alter the process, explaining why  $\theta$  in Eq. (8) is dependent on the probing frequency. Similar arguments explain why  $T_O$  also depends on the probing frequency.

In the above analysis, we focus on dipoles with kinetic energies higher than  $E_b$ . These dipoles are able to drift from one energy minimum to another when an ac electric field perturbs the system. It has been proposed that the drifting/hopping of dipoles from one potential well to another causes relaxations. However, without distinguishing dipoles inside and outside the potential well, such a proposal seems to have a tendency of confusing the wait time before hopping  $t$  (which reflects the distribution of dipoles at a given temperature) with the relaxation time  $\tau$  (which reflects how fast dipoles drift to the transient energy minimum and relates to the loss peak frequency in the Debye function), leading to some difficulties.

### C. Limitations

In previous studies [5,6,41], *ab initio* calculations are used, which prescribe all important interactions between dipoles and other degrees of freedom in the relaxors, and then MC or MD is used to numerically work out the consequences. In the present paper we do not start from an *ab initio* calculation, instead, employ statistical and phenomenological arguments. Having shown results and insights obtained with this approach, we now discuss possible limitations of the present approach with respect to the treatment of details, accuracy, and prediction power.

First, the proposed equations for lead-free [Eq. (8)] and lead-based relaxors [Eq. (12)] have five and six parameters, respectively. Ideally, one hopes to be able to use as few parameters as possible. However, it will be noted that, among these parameters, many are only material dependent (i.e., they do not depend on frequency or temperature). For instance, for a lead-free relaxor,  $E_b$  is a constant; for a lead-based relaxor,  $E_b$ ,  $\chi_1$ ,  $\chi_2$ , and  $\theta$  are close to constants (see Table III). For a given sample, these parameters may only need to be calibrated once. In this way, the number of parameters will significantly be reduced.

Second, in this paper we have focused on the temperature dependence of susceptibility. The dependence on frequency needs further investigation. For instance,  $T_O(\nu)$  and  $\gamma(\nu)$  in Eq. (12) need to be specified explicitly to address this issue. We note that the results shown in Table III will provide clues to the  $T_C$ 's and  $\gamma$ 's dependence on  $\nu$  and eventually help find analytical expressions for  $\chi(T, \nu)$ . In addition, we generally ignored possible long-range ordering of dipoles, which is another limitation to this approach. Although such possible long-range ordering makes relaxor physics rich, it will bring back Bose-Einstein statistics and make the current formulation more complicated. To what extent the Bose-Einstein and the Maxwell-Boltzmann distributions will be used for ferroelectric relaxors remains an open question.

Third, at high temperatures, the Curie law is observed in many ferroelectrics. For the static susceptibility of BZT [Fig. 1], this law can be recovered from the proposed equation, Eq. (7). On the other hand, for Eqs. (8) and (11), the Curie law cannot be recovered directly. For Eq. (11), we have the asymptotic relation  $\chi \sim [A/(T - T_O)^\nu + B/T^{3/2}]$  at very large  $T$ . It is unclear how well this relation can fit the Curie law. Therefore, in fitting experimental data at high temperatures, one needs to bear in mind that Eqs. (8) and (11) should be used with care.

Finally, with formulas, such as Eq. (12), we can in principle obtain the relation between  $T_m$  and  $\nu$  [assuming we know the analytical expressions of  $T_O(\nu)$  and  $\gamma(\nu)$ ], which can then be compared to the well-known Vogel-Fulcher law [6]. However, we have failed to obtain analytical expressions to relate  $T_m$  (note that  $T_m$  is not  $T_O$  whereas they may be close) to  $\nu$  and believe that a numerical calculation seems to be the only feasible way to establish the relation between  $T_m$  and  $\nu$ .

## V. CONCLUSIONS

Instead of working on the atomic level, the present paper employs a macroscopic statistical approach to describe the dielectric properties of the relaxors. The effects of disorder, PNRs, and random electric fields are considered statistically by introducing the average potential well, which can trap dipoles of low kinetic energies. An external ac electric field mostly will increase the magnitude of trapped dipoles but can rotate dipoles free from such trapping and align them with the field. These two groups of dipoles give rise to two different types of dielectric responses as shown in Eqs. (7), (8), and (11). The analytical equations resulting from this approach provide insight into the experimental and numerical results of the relaxors. Among other things, it is shown that the characteristic temperature  $T_m$  is determined by the Maxwell-Boltzmann distribution of the dipoles' kinetic energies as well as their ability to respond to the applied electric field. We can also conclude that lead-free relaxors (e.g., BZT) are different from lead-based relaxors (e.g., PZN-0.13PT) in that: (i) The mechanisms determining  $T_m$  are different. For lead-based relaxors, it appears  $T_O$  alone is able to determine  $T_m$ , whereas for BZT, both  $w_1(T)$  and  $P(E_b, T)$  are important; and (ii) for BZT,  $\chi_1$  and  $\chi_2$  are of the same order, whereas  $\chi_1 \gg \chi_2$  for the Pb-based relaxors, indicating that the dipoles outside the average potential well dominate the dielectric response of Pb-based relaxors. These results demonstrate that this statistical approach can provide a good understanding of important relaxor systems, and the proposed equations can be adopted in fitting experimental data of the relaxors in general (see Appendix C).

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#### APPENDIX A: EXTENDED FITTING RANGE

Unlike normal ferroelectrics, whose permittivity follows the well-known Curie-Weiss law  $1/\varepsilon = (T - T_{CW})/C$  above the Curie temperature, relaxors obey this law only for temperatures much higher (typically hundreds of degrees) than  $T_m$  where a broad and diffusive peak centers. Smolenskii [28] and Kirillov and Isupov [29] were the first ones proposing a quantitative description of such peaks. They suggested that the total number of relaxator contributing to the dielectric response in the vicinity of the permittivity peak is temperature dependent, governed by a Gaussian function with a mean value of  $T_O$  and a standard deviation  $\delta$ . With some additional

assumptions, they derived the following expression:

$$\frac{\varepsilon_0}{\varepsilon - \varepsilon_\infty} = \exp \left[ \frac{(T - T_o)^2}{2\delta^2} \right], \quad (\text{A1})$$

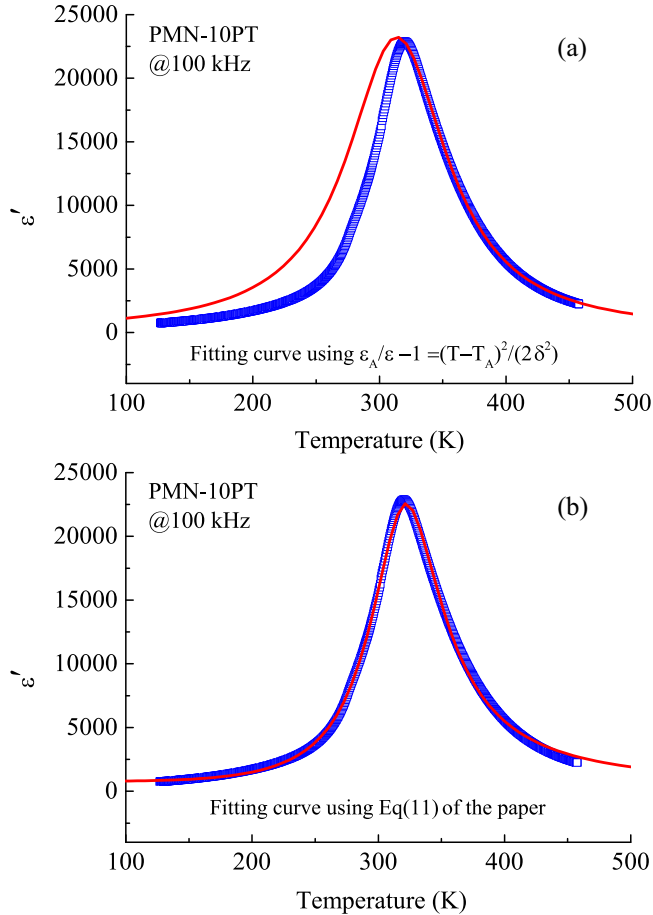


FIG. 9. The susceptibility of PMN-10PT obtained at 100 kHz are fitted with Eq. (A3) [panel (a)] and Eq. (11) [panel (b)].

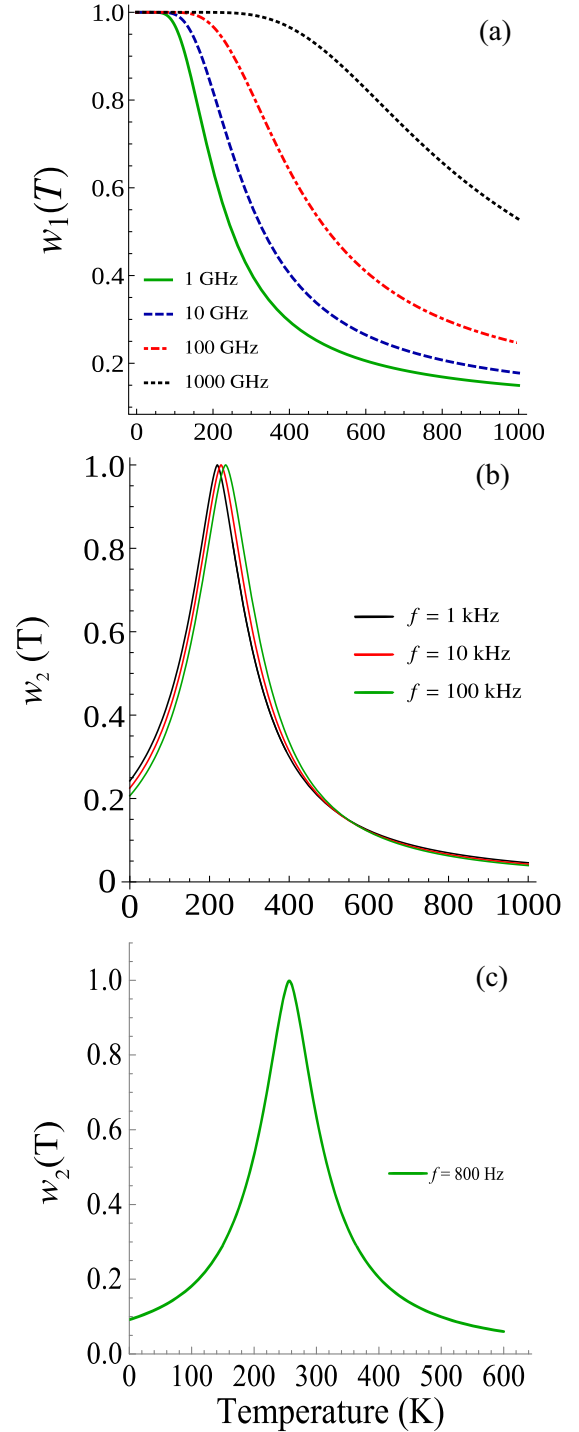


FIG. 10. The plotting for  $w_1(T)$  and  $w_2(T)$  with their parameters obtained by fitting BZT [panel (a), also see Fig. 3], PZN-0.13PT [panel (b), also see Fig. 6], and 0.95Pb(Mg<sub>1/3</sub>Nb<sub>2/3</sub>)O<sub>3</sub>-0.05Pb(Zr<sub>0.53</sub>Ti<sub>0.47</sub>)O<sub>3</sub> [panel (c), also see Fig. 7].



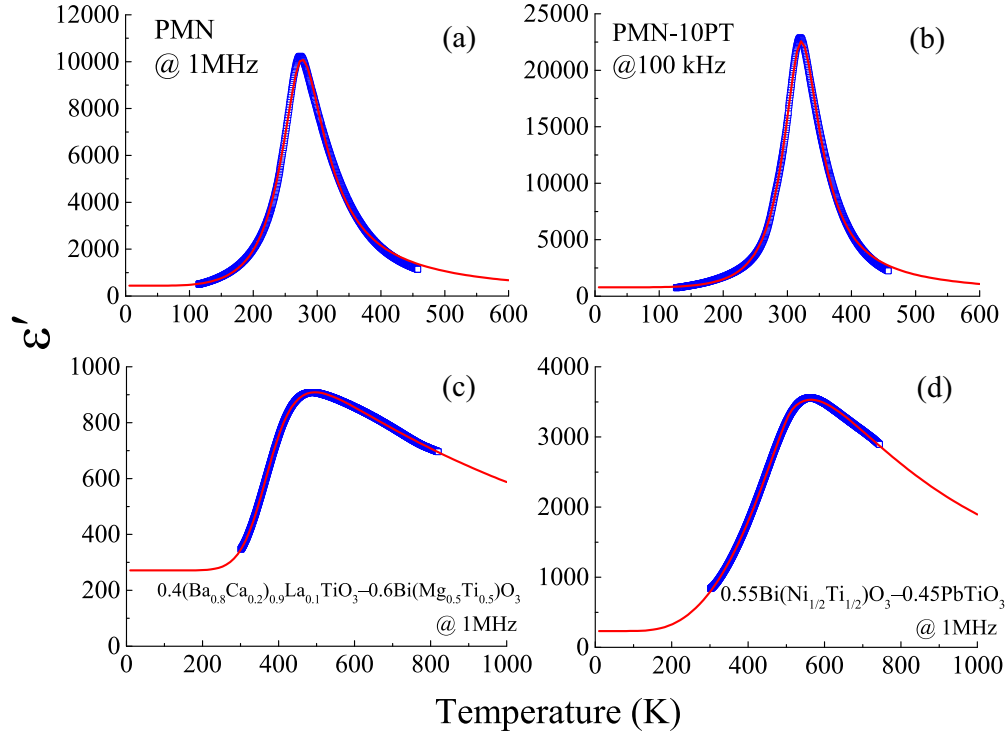


FIG. 11. Fitting the permittivity of various materials using Eq. (11). The blue circles are experimental data, and the red solid line is the fitting curve.

where  $\varepsilon_\infty$  is the high-frequency contribution and  $\varepsilon_0$  is a temperature and frequency-dependent parameter.

Neglecting  $\varepsilon_\infty$  and assuming that  $T_o$  is equal to the temperature where permittivity peaks ( $T_m$ ), one can expand Eq. (A1) and obtain a truncated power series [11],

$$\frac{\varepsilon_m}{\varepsilon} = 1 + \frac{(T - T_m)^2}{2\delta_m^2}. \quad (\text{A2})$$

The quadratic law [Eq. (A2)] was found to approximately be valid for  $T > T_m$  for many materials. However, the deviations of some experimental data from the quadratic law incited many authors to search for new formulas. A power law was proposed [30,31]

$$\frac{\varepsilon_m}{\varepsilon} = 1 + \frac{|T - T_m|^\gamma}{2\delta_\gamma^2}, \quad (\text{A3})$$

with  $1 \leq \gamma \leq 2$ , which differs from Eq. (A2) in that an empirical exponent  $\gamma$  is used instead of 2. This expression can be rearranged to give

$$\frac{\varepsilon}{\varepsilon_m} = \frac{1}{1 + \frac{(T - T_m)^\gamma}{2\delta_\gamma^2}} = \frac{1}{1 + \left| \frac{T - T_m}{(2\delta_\gamma^2)^{1/\gamma}} \right|^\gamma}, \quad (\text{A4})$$

where the right-hand side is just the  $w_2(T)$  we propose in Eq. (10).

Although Eq. (A2) or (A3) can successfully fit the temperature range of  $T > T_m$ , it is hard to fit the whole temperature range that is experimentally reachable [see Fig. 9(a)] with the main obstacle being the asymmetrical line shape around  $T_m$ . This obstacle is now resolved in this paper by introducing Eq. (11) where the asymmetry is accounted for by considering the Maxwell-Boltzmann distribution of dipoles. We illustrate

this point in Fig. 9 where fittings of PMN-10PT using Eqs. (A3) and (11) are compared.

## APPENDIX B: $w_1(T)$ AND $w_2(T)$

Figure 10 plots  $w_1(T)$  [Eq. (9)] and  $w_2(T)$  [Eq. (10)] with their parameters obtained by fitting BZT (Fig. 3), PZN-0.13PT (Fig. 6), and  $0.95\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$ - $0.05\text{Pb}(\text{Zr}_{0.53}\text{Ti}_{0.47})\text{O}_3$  (Fig. 7).

Figure 10(a) shows that, at low frequencies ( $\lesssim 10$  GHz),  $w_1(T)$  resembles the Fermi-Dirac function, that is, below  $\sim 250$  K, its value is close to one but becomes close to zero for  $T$  above  $\sim 250$  K. At a higher frequencies (e.g., 1000 GHz), however, this function strongly deviates from the Fermi-Dirac function with a long tail extending to high temperatures. Figures 10(b) and 10(c) show that  $w_2(T)$  is a symmetric peak, likely related to a phase transition in a lead-based relaxor. For Fig. 10(b), the peak position (around 220 K) slightly shifts toward higher temperatures with increasing frequency.

TABLE IV. Fitting parameters of various materials for Eq. (11).

	PMN	PMN-10PT	0.4BCLT-0.6BMT	0.55BNT-0.45PT
$\chi_1$	32201.07	67955.26	45373.38	11510.60
$E_b$ (K)	497.99	556.61	2204.65	985.24
$\chi_2$	442.07	792.65	271.47	232.94
$T_o$ (K)	272.73	319.51	364.84	508.84
$\theta$	44.10	35.71	121.38	255.20
$\gamma$	1.83	1.92	1.96	1.52

## APPENDIX C: APPLICABILITY TO OTHER SYSTEMS

In previous sections, we have focused on BZT and lead-based relaxor ferroelectrics and shown their fitting results. As a matter of fact, we have tested the proposed formula with various relaxor systems and obtained useful results. Figure 11 shows the results of four relaxor systems and the fitting

of the real part of their permittivity: (i) PMN; (ii) PMN-10PT; (iii)  $0.4(\text{Ba}_{0.8}, \text{Ca}_{0.2})\text{La}_{0.3}\text{TiO}_3$ - $0.6\text{Bi}(\text{Mg}_{0.5}, \text{Ti}_{0.5})\text{O}_3$ ; (iv)  $0.55\text{Bi}(\text{Ni}_{1/2}, \text{Ti}_{1/2})\text{O}_3$ - $0.45\text{PbTiO}_3$ . For these fittings, we have used Eq. (11) and obtained satisfactory results with the fitting parameters shown in Table IV, which further demonstrates the applicability of our approach.

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